

CONNECTICUT RIVER FLOOD CONTROL

REPORT

ON

REVIEW OF SURVEY

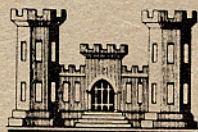
FOR

FLOOD CONTROL

PARK RIVER BASIN

CONNECTICUT

IN TWO VOLUMES
VOLUME II
(APPENDICES)



DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS.

JULY 1966

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DIGEST OF PUBLIC HEARING

APPENDIX A

DIGEST OF PUBLIC HEARING

A public hearing was held in Hartford, Connecticut, on 15 December 1964, to ascertain the views and opinions of local interests on the need and desirability of any modification to the existing flood control project at Hartford, with specific reference to the Park River. The attendance at the hearing numbered 81, of which 43 spoke, including representatives of Federal, State and local governments, industrial establishments, civic organizations, and interested individuals.

With few exceptions, prepared statements were read and submitted as exhibits. A statement prepared by Mr. Charles W. Cooke, Director of the Greater Hartford Flood Commission and presented by Mr. Harold F. Keith, Chairman of the Commission, outlined the desires of the Commission for modification to the existing Park River Conduit. Other speakers presented information substantiating the need for further flood control and generally endorsing the desires of the Commission. No opposition was expressed.

A digest of the public hearing is included in this Appendix. The hearing was conducted by Colonel E. J. Ribbs, Deputy Division Engineer.

DIGEST OF PUBLIC HEARING
HARTFORD, CONNECTICUT
14 December 1964

Speaker	Interest Represented	Comment
Abraham Ribicoff, U. S. Senator	State of Connecticut	Stated that review of existing flood control project is certainly necessary. Area has grown tremendously since 1942 and has great potential for growth. Urged Corps of Engineers to carefully study proposals to be presented with a view toward improving the existing flood control project. Urged and will support Corps in seeking authority to reimburse City of Hartford for local expenditures for conduit construction, which will qualify for Federal assistance, once Corps has authority to complete the work.
Harold W. Keith, Chairman	Greater Hartford Flood Commission	Statement prepared by Charles W. Cooke, Director of Commission: Described existing Park River Conduit, damage survey by the Commission following the August 1955 Flood, present conduit extension work by the Commission, the existing flood problem, and the various solutions which were studied. Presented desired plan of improvement which would consist of: (1) construction of conduit in the gaps left between conduit segments being built by the Commission; (2) 1,000 feet of conduit and 1,200 feet of improved

Speaker	Interest Represented	Comment
Harold W. Keith, Chairman (continued)	Greater Hartford Flood Commission	channel on the North Branch upstream of section proposed for construction by the Commission; (3) a pumping station in the vicinity of Riverside Street to discharge low-level drainage; (4) an auxiliary conduit to supplement the existing conduit and pass flows in excess of 18,000 cubic feet per second. In addition, reimbursement for cost of conduit construction by the Commission was requested.
Mayor William E. Glynn	1. City of Hartford 2. Thomas J. Dodd, U. S. Senator	1. Read a resolution by the Court of Common Council of the City of Hartford passed Dec. 14, 1964 requesting the Corps of Engineers to (a) reimburse the Greater Hartford Flood Commission 14 million dollars expended or to be expended on conduit construction; (b) assume the cost of constructing remaining portion of the Park River Conduit Extension. 2. Read a statement by U. S. Senator Thomas J. Dodd urging completion of the conduit work and reimbursement of the Greater Hartford Flood Commission's expenditures for conduit construction.

Speaker	Interest Represented	Comment
Alexander A. Goldfarb, Counsel, Greater Hartford Flood Commission	Emilio Q. Daddario, Member of Congress from Conn.	Read prepared statement which covered the history of flooding in Connecticut and the economic importance of Hartford to the Nation and which endorsed the request of the Greater Hartford Flood Commission for flood control improvements in the Park River Basin and reimbursement of money expended.
John O'Fallon	Federal Bureau of Public Roads	Had no statement at this time.
Col. E. J. Ribbs, Presiding Officer	Dept. of Interior, Fish and Wildlife Service	Read letter from U. S. Fish and Wildlife Service into the record which stated that modification of existing flood control project within the city limits will have no significant effect on limited fish and wildlife resources.
William S. Wise, Director, Conn. Water Resources Comm.	John E. Dempsey, Governor of Conn.	Read statement by Governor. In accord with Greater Hartford Flood Commission. Flood control in the Park River Basin is most important to the economic future of the region. Is concerned with Connecticut's industrial development. The potential of the Park River Basin for industrial, commercial, financial and residential development, together with public health and safety, are considerations which recommend review of the existing flood control project to determine need of further improvements. Favors

Speaker	Interest Represented	Comment
William S. Wise, Director, Conn. Water Resources Comm. (continued)	John E. Dempsey, Governor of Conn.	all flood protection that is feasible and practical to protect lives and property.
Joseph N. Gill, Commissioner	Conn. Dept. of Agriculture and Natural Resources	Comprehensive flood damage reduction program in Park River Basin will require additional participation by Corps of Engineers. Project formulation for Small Watershed plans for the North and South Branches, Park River, were predicated on provision of an auxiliary conduit as a part of conduit extension. The North Branch Park River Work Plan provides for four flood retarding structures. The South Branch Park River Work Plan, beginning at Hamilton St. in Hartford, provides for four floodwater retarding structures, preservation of a natural flood water retention swamp and over nine miles of stream channel improvement. Work plans were developed recognizing that continued development of flood plain areas results in loss of floodwater storage. Structural works of improvement would need to be augmented by regulatory measures between outlet of structure and proposed conduit extension. Channel encroachment lines are currently being established by the State Water Resources Commission. Upstream flood retarding structures coupled with the implementation of regulatory measures will supplement and complement downstream conduit extension projects.

Speaker	Interest Represented	Comment
Wm. J. Mislock	Commissioner, Conn. Public Works Dept.	Stated that the State is in favor of enclosing the entire Park River. Immediate construction of gap to Broad Street appears to be an immediate necessity so that State can complete its plans for development of parking garage in the area.
George S. Koch	Howard S. Ives, Commissioner, Conn. State Highway Dept.	Referred to 1944 Federal legislation establishing interstate Highway concept and 1956 Highway Act establishing highway network and methods of financing and setting 1970 as the completion date for the entire system. Interstate Route 84 through Hartford was designed to take advantage of airspace over the Park River and railroad tracks wherever possible. Preparation of contract plans started in 1959. It became apparent that construction of highway without provisions for future flood control in areas of restricted right of way might preclude necessary flood protection for Hartford. State and Greater Hartford Flood Commission entered into an agreement whereby two facilities could be designed and constructed concurrently where a conflict existed. The cost of conduit work already underway or soon to be put under construction should be considered as a part of the cost of flood control by the Corps of Engineers.

Speaker	Interest Represented	Comment
Lt. Col. Wm. J. St. John, Military Property Office, State of Conn.	Adjutant General, State of Conn.	Endorsed Greater Hartford Flood Commission proposal and recommended early construction of gaps. In addition to flood control, completion of conduit would provide additional parking and eliminate rodent population and hazard of open river.
E. Wells Eddy, Vice-Chairman, Greater Hartford Flood Comm.	Self	A resident of Newington, said he appreciates work of Corps and favors its continuation.
John W. Jessup, Principal Planner	Planning Commission, City of Hartford	Pointed out that flood control work by Corps in coordination with City has produced great benefits - permitted development of previously unusable land. Immediate construction of three sections of conduit by the Greater Hartford Flood Commission was necessary in order that future benefits could be realized and highway schedule met. If Corps completes work, reimbursement for work already done should be made. Commission supports proposal that Corps assume flood responsibilities to safeguard health, safety and general welfare.
Raymond J. Kelly, President, Hartford Board of Education	Board of Education	Supported proposal to have Corps complete conduit which would not only provide flood control but also needed parking and playing field area in the vicinity of Hartford High School.

Speaker	Interest Represented	Comment
George J. Ritter Former Corporation Counsel, City of Hartford	Self	Said 1955 legislation which created Greater Hartford Flood Commission provided that all funds which are spent for flood control would come from bond issues by City of Hartford. It was anticipated at that time that all or part of the funds so spent could at some future date be returned by the Federal Government.
Elisha Freeman, City Manager	City of Hartford	Introduced 9 Department heads who commented as follows:
John Walsh, Director of Finance	City of Hartford	Greater Hartford Flood Commission authorized to spend \$20 million. \$14 million spent or committed for conduit essential for construction of Highway I-84. \$6 million spent or committed on other flood control work. \$14 million is 29% of City's indebtedness. Requests Corps to complete the conduit work.
L. C. Lovell, Director of Public Works	City of Hartford	The 1955 flood divided city into two parts. Conduit will eliminate 8 bridges, with replacement cost of \$3,200,000, most of which are in need of replacement. Saving in replacement could be considered a benefit.
Robert J. Bliss, Exec. Director, Hartford Redevelopment Agency	City of Hartford	Agency in favor of any proposal particularly in vicinity of 33 acre city urban renewal project between Capitol Avenue and Park Street which will cost Federal, State and City governments a total of \$2,000,000.

Speaker	Interest Represented	Comment
Robert J. Bliss, Exec. Director, Hartford Redevelopment Agency (continued)	City of Hartford	Much of area, adjacent to the Park River, will have its use limited to parking unless flood protection is provided. Conduit plus renewal will change a flood prone area to a modern industrial park.
Charles E. Hughes, Traffic Engineer	City of Hartford	In 1955, all east-west roads to and from Hartford were blocked by overflowing North and South Branches Park River. A repetition today would be a catastrophe. When completed, interstate highway I-84 will supplement the local streets but it is essential that they never be again flooded.
A-9 Everett J. Pyle, Director of Parks and Recreation	City of Hartford	Enclosing the Park River in a conduit would make more park land available for development. Area would be used by factory workers and nearby residents. Addition of open space land would be consistent with Federal, State and local open space programs.
Dr. Norton C. Chaucer, Director of Health	City of Hartford	Proposed conduit extension will aid in pollution abatement, reduce odor nuisances, aid in rodent control, eliminate hazard to children, and eliminate the use of river bed and banks for illegal waste and rubbish disposal.

Speaker	Interest Represented	Comment
Daniel G. Lyons, Exec. Director, Hartford Housing Authority	City of Hartford	The 1955 flood necessitated evacuation of 178 families. Conduit construction would prevent a repetition and would eliminate hazard to children.
George E. Heppner, Asst. City Engineer	Porter H. Barrows, Hartford City Engr.	Supports proposal of Hartford Flood Commission. During 1955 flood all bridges in Hartford and for some distance up the North and South Branches Park River were inundated. Major fire apparatus and police control was limited to center of Hartford. Major hospitals were isolated to all but those in downtown area. A reduction in the possibility of future flooding is essential to prevent a recurrence.
Robert M. Kelley, Asst. Supt. of Schools	Hartford School Dept.	New high school is hampered by lack of space for athletics and for parking, both day and evening. Extension of the conduit would provide added space needed for full utilization of school facilities.
Betty Knox, Councilwoman	Hartford City Council	Expressed desire for adequate flood control financed on a fair share basis with help from Federal Government.
Ann Uccello, Councilwoman	Hartford City Council	Pointed out that Hartford is only community to undertake its own program. A program of this scope and magnitude deserves financial assistance.

Speaker	Interest Represented	Comment
Theodore J. DeLorenzo, Councilman	Hartford City Council	Said Hartford is burdened by bonded indebtedness and because central area is on a diminished tax basis. 50% of area is non-taxable governmental and charitable properties, hospitals and schools. Corps should encourage community initiative such as Hartford's by assuming responsibility for conduit completion.
Thomas J. Corrigan, Councilman	Hartford City Council	Importance of flood control to Hartford is indicated by the fact that 29% of city's bond indebtedness is tied up in it, as a result, other programs have had to be put off; he stated City should not be penalized for its initiative.
Christopher Percy	Capitol Region Planning Agency	He believes extensive flood control projects completed to date make sound beginning of an overall flood control program. CRPA questions the need for enclosing the North Branch Park River in a conduit above Farmington Avenue. Every effort should be made to keep the river system as a permanent open space with necessary flood control achieved by flood plain zoning.

Speaker	Interest Represented	Comment
George B. Kinsella, Councilman	Hartford City Council	Corps participated in flood control after 1936 flood on Connecticut River. A problem now exists along the Park River. Stated that we ask now for assistance before flood conditions again occur.
Arthur W. Sweeton, Deputy Manager and Chief Engineer, Bureau of Public Works, Metropolitan District	Chairman McDonough	Urged further flood control in Greater Hartford. Auxiliary conduit along Park Street should provide an economical outlet for some of the storm drains to be built as part of the District's comprehensive plan to separate old combined sewers. Use of auxiliary conduit for this purpose should result in savings of many hundred thousands of dollars.
A-12 Robert K. Killian, Attorney, Chairman, Hartford Democratic Town Committee	Democractic Town Committee, Individual	Felt that if favorable recommendation reflecting unanimous support of those present is submitted to Washington, funds will be made available.
James E. Bent, President, Greater Hartford Chamber of Commerce	(1) Individual (2) Greater Hartford Chamber of Commerce	(1) Said he was President, in 1955, of Rotary Club of Hartford which joined with others to form United Service Clubs of Conn. to raise money for flood relief work. Claims, otherwise unreported, amounted to \$40 million. Taxes alone on a loss of this size would probably be enough to pay for project being considered now.

Speaker	Interest Represented	Comment
James E. Bent, President, Greater Hartford Chamber of Commerce (continued)	(2) Greater Hartford Chamber of Commerce	(2) Chamber of Commerce believes that flood control on Park River is important to the economic future of the area. City's initiative in attempting to solve flood problem warrants assistance of Corps of Engineers.
John H. Fairbrother	Royal McBee Corp.	Stated that existing flood control project at Hartford is usually taken for granted. Company is vitally interested in Kane Brook. During flood, water covered parking area and threatened plant. East-West highway construction has aggravated the conditions as large areas have been filled, eliminating natural storage. Requested attention be given this problem to prevent future damages.
Robert K. Mooney, Treasurer, Mooney Co.	Mooney Co.	Company is in the storage business and owns property on Capitol Avenue abutting the Park River. Buildings were wet in 1936 and 1955. Clients do not like flood-prone buildings for storage of machinery and stock.
Wm. M. Baker, President, Morrow Machine Co.	Morrow Machine Co.	Gave data: plant on Laurel and Riverside Streets at confluence of north and south branches of Park River, three feet of water over floor in 1955. Heavy equipment cannot be moved. Some flood produced damages do not become apparent until months after the floods. Employ 250-275 people.

Speaker	Interest Represented	Comment
William R. Peele	Arrow-Hart & Hegeman Electric Co.	Said that they employ approximately 2,000 in 5 Hartford plants with 900,000 sq. ft. of space. Have already had land and one building taken by Hartford Flood Commission between Broad and Flower Streets. Hopes Corps will assist in completing the project.
Herbert E. Johnson, Vice-President, Hartford Gas Co.	Chairman, Wm. T. Webb	Stated that existing flood control project made it possible for the Company to construct a steam and chilled water plant adjacent to the Park River. Prior to flood control, gas service was interrupted and property damaged. Further flood control as proposed by Mr. Cooke would provide added protection and increase Hartford's tax base.
George A. Washburn, Civil Engineer	Hartford Electric Light Co.	Adequate flood control is vital to future commercial and industrial development and public health and safety. Urged conduit completion.
Wm. H. Kuehnel, Secretary, Greater Hartford Labor Council, AFL-CIO	AFL-CIO	Interested in flood control as thousands of members have suffered from past floods. Without flood control, manufacturing plants might move and jobs be lost. Endorsed proposal by Greater Hartford Flood Commission.

Speaker	Interest Represented	Comment
T. R. Harlow, Director, Conn. Historical Society	Conn. Historical Society	Reported Society is privately endowed institution with 900 members in Connecticut; 600 in other states. 70,000 books and pamphlets, and thousands of museum pieces, valued at \$10 million. 1955 flood damaged and destroyed rare books. Repairs to building and cost of dike for protection was \$42,000. In favor of flood control. Endorse proposal of Flood Commission.
Henry R. Olsen	Kilian Steel Ball Corp.	Reported that two 1955 floods caused flooding in plant. First - 8 feet of water; second - 4 feet. In favor of Commission's proposal.
A-15 Alexander Goldfarb, Counsel for Greater Hartford Flood Commission	Greater Hartford Flood Comm.	Stated \$20 million statutory authority for flood control exhausted or committed. No further authority likely except from the Federal Government.
Theodore Brindamour, Engineer	Greater Hartford Flood Commission	Said that Park River above existing conduit is subject to flood damage not only from runoff from the Park River Basin but from backup through the conduit when the Connecticut River is at a high stage.

APPENDIX B

HYDROLOGY AND HYDRAULICS

APPENDIX B
HYDROLOGY AND HYDRAULICS

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APPENDIX B

HYDROLOGY AND HYDRAULICS

1. INTRODUCTION

This appendix presents hydrological and climatological data for the Park River basin, derivation of the standard project flood, an analysis of the effect of various changes that have recently taken place in the basin, and effect of proposed plan of protection.

2. BASIN DESCRIPTION

a. General. The Park River basin, shown on plate B-1, is located in the central part of Connecticut where it drains a large portion of the metropolitan Hartford area. The watershed which drains 78.3 square miles is roughly rectangular in shape with an average width in an east-west direction of 5 miles and an average length in a north-south direction of 16 miles. Elevations range from about 20 feet msl along the lower reaches of the river to a maximum of about 900 feet along the western edge of the watershed. Most of the area, however, is below 200 feet msl in elevation and is comprised of rolling to hilly topography.

b. Park River. The Park River, located entirely within the confines of the city of Hartford, is formed by the junction of the North and South Branches. It flows in an easterly direction for a distance of 2.2 miles and discharges into the Connecticut River about a half mile upstream of the Charter Oak bridge. In 1944 the Corps of Engineers completed a twin-barreled concrete conduit that enclosed the Park River from Bushnell Park through the business center of Hartford to the Connecticut River (see plate B-2 for the general plan and profile).

c. South Branch Park River. The South Branch which flows in a generally northerly direction, drains an area of 46.8 square miles south and west of Hartford and is formed at the confluence of Trout and Piper Brooks. Trout Brook, with an area of 19.6 square miles, originates in the Talcott Mountain range in West Hartford and Farmington. Piper Brook, with a watershed of 22.2 square miles, develops in the hilly areas of New Britain. Its two main tributaries are Mill and Bass Brooks with respective areas of 5.6 and 10.3 square miles. There are numerous lakes and swampy areas in the tributary headwaters which have a

considerable reducing effect on floodflows. The Soil Conservation Service is constructing four floodwater retarding structures in the basin that control a total drainage area of about 5.2 square miles. These structures will have some modifying effect on future floods.

d. North Branch Park River. The North Branch which flows in a generally southerly direction drains an area of 27.4 square miles west and north of Hartford and is formed at the junction of Wash and Tumbledown Brooks. Wash Brook with 5.7 square miles drains the northern part of the basin and originates in the town of Bloomfield. Tumbledown Brook drains the western part of the basin and has an area about 8.7 square miles. Beamans Brook which also originates in Bloomfield has a watershed about 5.2 square miles.

There is one lake and several swampy areas in the basin but they do not have as much effect on floodflows in the North Branch. The Soil Conservation Service is constructing floodwater retarding structures in the basin that control about 8.1 square miles. These reservoirs have an appreciable reducing effect on floodflows.

3. CLIMATOLOGY

a. General. The Park River watershed has a variable climate characterized by frequent but usually short periods of precipitation. The basin lies in the path of the "prevailing westerlies" and is exposed to the cyclonic disturbances that cross the country from the west and south-west toward the northeast quadrant of the country. The area is also exposed to coastal storms, some of tropical origin, that travel up the Atlantic seaboard. In late summer and autumn months these storms occasionally attain hurricane intensity. Thunderstorms, either of a local origin or associated with a frontal system, occur generally during the summer months.

b. Temperature. Average monthly temperatures in the Park River basin vary considerably through the year with a mean annual temperature of about 50° F. The summer temperatures average in the upper 60's and low 70's with winter temperatures averaging in the upper 20's and low 30's. Freezing temperatures can be expected from about the middle of November until the end of March. The mean, maximum and minimum monthly temperatures for 60 years of record at the Hartford Weather Bureau station, located about 10 miles north of downtown Hartford are shown in table B-1.

c. Precipitation. The average annual precipitation over the Park River watershed is approximately 43 inches, which is evenly distributed throughout the year. The maximum and minimum annual precipitation at the Hartford Weather Bureau station (elevation 170

feet msl) for 60 years of record are 62.94 and 32.26 inches, respectively. Table B-2 summarizes the precipitation records for this station.

TABLE B-1

MONTHLY TEMPERATURES
(Degrees Fahrenheit)

<u>Month</u>	<u>Mean</u>	<u>Maximum</u>	<u>Minimum</u>
January	27.5	66	-26
February	27.8	68	-21
March	37.0	87	- 8
April	47.9	94	15
May	58.9	95	27
June	67.7	101	37
July	73.0	101	44
August	70.6	101	42
September	63.6	101	27
October	53.4	91	22
November	42.1	83	10
December	30.5	67	-11
ANNUAL	50.0	101	-26

TABLE B-2

MONTHLY PRECIPITATION
(Inches)

<u>Month</u>	<u>Mean</u>	<u>Maximum</u>	<u>Minimum</u>
January	3.61	7.77	0.91
February	3.21	5.72	1.54
March	3.69	9.21	0.29
April	3.68	7.66	0.65
May	3.43	7.04	0.73
June	3.46	8.08	0.66
July	3.67	11.24	0.54
August	3.98	21.87	0.93
September	3.52	14.59	0.20
October	3.03	11.61	0.18
November	3.71	7.36	0.87
December	3.55	6.88	0.78
ANNUAL	42.54	62.94	32.26

d. Snow. The average yearly snowfall over the watershed is about 40 inches. The water content of the snow cover over the entire basin reaches a maximum in the late winter or early spring with an average depth of 2 to 3 inches. Table B-3 summarizes the monthly and annual average snowfall at the Hartford Weather Bureau for 59 years of record.

e. Storm types. The Park River watershed experiences storms of four general types, namely:

(1) Extratropical continental storms which move across the basin under the influence of the "prevailing westerlies."

(2) Extratropical maritime storms which move northward along the eastern coast of the United States.

TABLE B-3

MONTHLY SNOWFALL
(Depth in Inches)

<u>Month</u>	<u>Snowfall</u>
January	10.9
February	12.1
March	7.5
April	1.4
May	-
June	-
July	-
August	-
September	-
October	-
November	1.9
December	8.1
ANNUAL	41.9

(3) Coastal storms of tropical origin, some of which attain hurricane magnitude. Hurricane storms generally occur in late summer or fall months and have caused the most devastating floods in the basin.

(4) Thunderstorms produced by local convective activity or by more general frontal action.

f. Notable storms. The storms associated with the 5 major floods of record in the basin are briefly described as follows:

(1) March 1936. A succession of several continental disturbances of the cold frontal type moved across the northeastern part of the United States during the early part of March. The disturbances were accompanied by warm temperatures and heavy rains. The severest storm produced 3 inches of rain in a 24-hour period.

(2) January 1938. On 24-25 January, another continental frontal type storm system passed over the basin depositing about 3 inches of rainfall. Warm temperatures in the 50's during this period

produced considerable runoff from snowmelt.

(3) September 1938. A stationary cold front associated with unsettled weather along the Atlantic coast was overrun by a rapidly moving tropical hurricane producing record breaking rainfall over large areas of Connecticut. Between 17 and 21 September, light rain fell almost continuously and culminated in a heavy downpour. During this 4-day period, between 11 and 12 inches of precipitation fell over the basin.

(4) August 1955. The northwesterly progress of hurricane "Diane" through the Middle Atlantic States was blocked by a stagnant high pressure system over the northeastern United States forcing the storm to veer off in an easterly direction, south of Long Island, on a course parallel to the southern New England coast. As the system moved slowly out to sea south of New England, it became recharged with moisture which was literally dumped over southern New England. This storm deposited 12 to 13 inches of rain over the basin.

(5) October 1955. The storm of 14-17 October originated as an extratropical low pressure area off the Florida coast. The forward northward movement of the system stalled off the New Jersey coast. Warm moist air circulating about the low overran the cooler air of the blocking high over southern New England producing heavy rainfall from 6 to 7 inches over the basin.

4. STREAMFLOW DATA

The U. S. Geological Survey has published records of streamflow for three locations since 1936 and four others since 1958 in the Park River watershed. A summary of pertinent data at each gaging station is given in table B-4.

5. HISTORY OF FLOODS

a. General. Outstanding floods on the Park River have occurred during all seasons of the year. Heavy rains with melting snow resulted in the floods of March 1936 and January 1938. Heavy rains during the summer and fall months caused the major floods of September 1938, August and October 1955. In addition, local thunderstorms have caused flash flooding on the smaller streams.

b. Historic floods. Records of historic floods occurring on the Park River are meager. However, the flood of October 1869, resulting from 12 inches of rain falling in 2 to 3 days, was severe and caused considerable damage.

c. Floods of record. The Park River has experienced five major

TABLE B-1.

STREAMFLOW RECORD - PARK RIVER BASIN

<u>Location</u>	<u>Drainage Area (sq.mi.)</u>	<u>Period of Record</u>	<u>Discharge (cfs)</u>		
			<u>Mean</u>	<u>Maximum</u>	<u>Minimum</u>
Park River at Hartford, Connecticut	74.0	Oct 1936 - Sept 1961	124	14,000 ⁽¹⁾	11 (2)
South Branch at Hartford, Connecticut	40.6	Oct 1936 -	73.1	5,000 ⁽¹⁾	7 (2)
North Branch at Hartford, Connecticut	25.3	Oct 1936 -	38.1	10,000 ⁽¹⁾	0.4(2)
Trout Brook at West Hartford, Connecticut	14.7	May 1958 -	28.3	1,020	1.4(2)
Piper Brook at Newington, Connecticut	14.4	May 1958 -	24.3	935	-1
Wash Brook at Bloomfield, Connecticut	5.66	Apr 1958 -	8.01	465	-1
Mill Brook at Newington, Connecticut	2.56	Apr 1958 -	4.23	460	-1

(1) August 1955

(2) Minimum Daily Flows

floods since 1900. They occurred in March 1936, January and September 1938, and August and October 1955. The flood of August 1955 is by far the largest flood of record in the basin. According to USGS records, the peak discharge at the Park River gaging station was 14,000 cfs or about 190 csm. Total volume of runoff approximated 8.5 inches. The October 1955 flood was the second largest and the volume of runoff was about 4.5 inches. Comparative flood magnitudes for these 5 floods at 3 USGS gaging stations in the basin are given in table B-5.

TABLE B-5

FLOODS OF RECORD*
(Peak Flow in CFS)

<u>Date</u>	<u>Park River Gage</u> (DA=74.0 sq.mi.)	<u>South Branch Gage</u> (DA=40.6 sq.mi.)	<u>North Branch Gage</u> (DA=25.3 sq.mi.)
19 Aug 1955	14,000	5,000	10,000
16 Oct 1955	6,420	2,800	3,680
25 Jan 1938	5,650	2,860	3,000
12 Mar 1936	5,400	-	2,800
21 Sept 1938	5,320	3,600	1,350

* USGS published records

d. Park River discharge frequency relationship. Peak discharge frequency relationships were developed at the Riverside Street gaging station from published records of the U. S. Geological Survey and stage records maintained since 1912 by the Engineering Department of Hartford. The frequency analysis was made in accordance with procedures described in ER 1110-2-1150, "Hydrologic Frequency Estimates," dated 10 October 1962. The method assumes that logarithmic values of annual peak flows are normally distributed, thereby permitting the application of standard statistical procedures. This enables the discharge frequency curve to be defined by its mean value and standard deviation. A skew factor of 1.0 was adopted and was based on a regional frequency analysis for the Connecticut River basin. A natural (1955 conditions) discharge frequency curve was developed based on the available records and is shown on plate B-3.

6. ANALYSIS OF FLOODS

a. General. Past floods were analyzed to determine the hydrologic flood characteristics of the Park River watershed. Both tributaries

were divided into subtributary areas and routing reaches for hydraulic analysis. The limits of the reaches were taken at hydraulic control points such as gaging stations, reservoir locations, and mouths of tributaries. Floods analyzed included those of March 1936, November 1937, January and September 1938, and August and October 1955. The winter and spring floods contained considerable snow melt which affected rainfall runoff relationships.

On the South Branch, floodflows were greatly modified by both the water supply reservoirs in the headwaters and the extensive valley storage throughout the watershed especially along the lower reaches. In addition considerable amounts of floodflows were diverted over low natural divides into other watersheds.

Floodflows on the North Branch were also affected by extensive valley storage in the tributary headwaters and also along the main stem upstream of the Albany Street gaging station.

b. Recent local flood control measures. Since the record floods of 1955, local interests developed plans for flood control works of improvements in both branches of the Park River which have been constructed or in the final design stages. The improvements which have substantially affected the runoff characteristics of the watershed, some beneficially and others adversely, are as follows:

- (1) Construction of 8 flood retarding structures by SCS.
- (2) About 9 miles of improvements along the South Branch consisting of the realignment, widening and deepening of the existing channel. The improved channels will have discharge capacities ranging from 11,000 cfs near the mouth of the South Branch to 6,000 cfs on Trout Brook and 4,500 cfs on Piper Brook. Some sections of the completed and proposed channels are concrete lined.
- (3) Major highway construction in the flood plain of the South Branch.
- (4) Extension of the existing Park River conduit up the North Branch to near Farmington Avenue and up the South Branch to Pope Park.

Table B-6 presents pertinent data on the 8 reservoirs and the South Branch channel improvements. General locations of the improvements are shown on plate B-1.

c. Effect of local works on flood discharges. Flood retarding structures, constructed and proposed by the Soil Conservation Service store runoff from 8.11 square miles, or 29 percent of the North Branch and 5.21 square miles, or 11 percent of the South Branch watershed.

TABLE B-6

PERTINENT DATAA. SOIL CONSERVATION FLOOD RETARDING STRUCTURES*

<u>Reservoir</u>	<u>Drainage Area (sq.mi.)</u>	<u>Storage</u>		<u>Outlet Discharge with Pool at Spillway Crest</u>		<u>Conduit Size</u>
		<u>Acre- Feet</u>	<u>Inches of Runoff</u>	<u>CFS</u>	<u>CSM</u>	
<u>North Branch</u>						
Wintonbury	1.62	725	8.57	95	67	30" Dia.
Blue Hills	1.70	1,057	11.66	66	39	30" Dia.
Blcomfield	3.05	1,588	9.76	165	54	36" Dia.
Cold Spring	1.94	1,038	10.03	107	55	36" Dia.
	8.11					
<u>South Branch</u>						
Talcott	1.57	890	10.63	114	73	2-30" Dia.
Bugbee	1.96	760	7.27	280	143	48" Dia.
South Reservoir	1.30	650	9.40	114	88	30" Dia.
Burnt Hill	0.38	170	8.39	53	140	30" Dia.
	5.21					

* All reservoirs have been completed except Cold Spring, Burnt Hill and Bugbee which are scheduled for completion in 1966 or early 1967.

B. SOUTH BRANCH CHANNEL IMPROVEMENTS
BY SCS AND LOCAL INTERESTS

<u>Stream</u>	<u>Location</u>	<u>Channel Capacity (cfs)</u>	<u>Scheduled Completion Date</u>
South Branch	Hartford W. Hartford	10,400 to 11,100	1968
Piper Brook	W. Hartford Newington	3,600 to 4,550	1966
Mill Brook	Newington	1,000	1967
Trout Brook	W. Hartford	3,300 to 6,000	1968
Rockledge Brook (S. Branch Trout Brook)	W. Hartford	750 to 1,000	Completed

These reservoirs will have some modifying effect on future floods in the basin. Because of the large outlet capacities of the reservoirs, there is only a small modifying effect on minor to moderate size floods. More appreciable reduction will be realized during major floods. Other works such as channel improvements, highways and conduit extensions will have a tendency of increasing peak flows because of the loss of valley storage, lowering of the gradient and improved channel alignment. On the South Branch the net overall effect of improvements will be higher peak flows but occurring at corresponding lower elevations. The effect of the improvements on the North Branch will be lower peak flows and lower elevations. Channel work on the South Branch with lower gradients and less effective use of the valley storage, will cause higher peak flows to occur on the Park River which will result in more frequent flooding. On the Park River the conduit extensions constructed for highway crossings will have no modifying effect on discharge relationships at the open river sections. A discharge-frequency curve for the Park River depicting the effects of local works is shown on Plate B-3. The higher peak flows also will reduce the degree of protection provided lower Hartford by the existing Park River conduit. It is conceivable that, with the numerous changes that have taken place since 1955, a storm of the magnitude of hurricane "Diane" could now cause a flood that would overtax the capacity of the existing Corps of Engineers conduit and flood the protected portion of the city of Hartford.

d. Effect of local works on the August 1955 flood. The August 1955 storm produced greater rainfall amounts over the North Branch than the South Branch. Over the North Branch the average precipitation was about 12.5 inches, while the South Branch experienced an average of about 10.5 inches. An isohyetal map of the storm is shown on plate B-5. Although the North Branch drains 25.3 square miles compared to the 42 square miles of the South Branch, the estimated peak of 10,000 cfs (U. S. Geological Survey) on the North Branch was twice as great as the estimated peak of 5,000 cfs (USGS) on the South Branch. Several factors tended to produce this smaller peak flow on the South Branch. The four headwater water supply reservoirs controlling 4.1 square miles were drawn down at the beginning of the flood and therefore stored a considerable amount of runoff. It is estimated that approximately 2,000 acre-feet of floodflows were diverted into the Mattabesset and Quinnipiac River basins from the Piper and Mill Brook watersheds. These diversions took place at low natural divides and were caused by high backwater gradients in the brooks and the South Branch. The floodflow on the South Branch also was affected by about 3,600 acre-feet of valley storage.

The North and South Branches component flows for the 1955 flood were routed to the Park River and a synthesized hydrograph

was added for the local drainage area of 7.2 square miles. The total compared favorably with the USGS Park River hydrograph except for volume. Analysis of the North Branch hydrograph indicated that the runoff exceeded the average rainfall. The runoff hydrograph was adjusted and rerouted to the Park River. Plate B-4 shows the August 1955 flood hydrographs at the USGS gaging stations and the adopted North and South Branch components routed to Riverside Street on the Park River. Had there been no diversion of floodflows out of the basin, it is estimated the peak flow of the South Branch at Newfield Avenue would have increased from 5,000 to 7,200 cfs resulting in a peak of 15,700 cfs on the Park River at Riverside Street. Current channel and highway works would further increase the Newfield Avenue peak to about 9,000 cfs. The four SCS flood retarding reservoirs would reduce the peak flow to about 8,200 cfs which is still considerably higher than the estimated 5,000 cfs experienced in 1955.

On the North Branch, channel improvements and highway work would have only a minor effect on a recurring August 1955 flood. The four SCS flood retarding structures would reduce the peak flow of 10,000 cfs at Albany Avenue to about 7,500 cfs. At the USGS gaging station on the Park River, the effect of highway and channel works would increase the peak flow of 15,700 cfs (with no diversion) to 18,750 cfs and the SCS reservoirs would reduce the peak to 16,100 cfs. The net overall effect of all these improvements would be to increase the peak of the August 1955 flood by about 400 cfs as shown on plate B-4.

e. Effect of local works on Park River elevations in Hartford.

(1) General. Two open lengths in the Park River conduit extension still remain, the first being section 2 in the Flower Street-Broad Street area and the other being sections 4 and 7 upstream of Capitol Avenue to about Willow Street (see plate B-2). Channel conditions in these open gaps have remained the same, that is, the cross sectional areas, alignment and riverbed profiles have not been changed. As previously mentioned, the effect of the overall local works has been to increase the Park River discharges for all frequencies. The resultant effect has been an increase in water surface elevations for all frequencies along the Park River upstream of the conduit entrances near the State Armory.

(2) Overtopping of Bushnell Park dike. The original conduit, completed in 1944, has a headwall and dike at the conduit entrance near Bushnell Park constructed to elevation 51 feet msl (including 3 feet of freeboard). This gave added protection to the downtown area of Hartford from all but rare floods when the dike might either be overtopped or fail, resulting in large volumes of water flowing into downtown Hartford. Although it takes a large flood to overtop this dike, the frequency of such an occurrence has been appreciably

increased due to local work improvements. The original conduit and headwall dike were designed for a discharge of 18,000 cfs. With a greater design storm than previously used and recent developments in the basin, the standard project flood would produce a flow of 30,300 cfs at Riverside Street. This would result in overtopping the entrance headwall and cause serious flooding in downtown Hartford.

7. STANDARD PROJECT FLOOD

a. General. In 1940 the engineering firm of Metcalf & Eddy recommended a design discharge of 18,000 cfs for the Park River conduit that extends from the Connecticut River to Bushnell Park. Following the flood of August 1955 Metcalf & Eddy were retained by the Greater Hartford Flood Commission to evaluate the effect of this record flood on design floodflows in the Park River basin. Using additional rainfall and runoff data, the engineering firm computed a new design flood which had a peak discharge of 24,900 cfs. A report prepared by Metcalf & Eddy for the Commission, dated February 1958, outlined the procedures used in developing the flood. In general, the procedures were in accordance with those outlined in EM 1110-2-11405 and CEB 52-8. The storm producing this flood has been adopted as the standard project storm for the Park River. Recently local interests proposed a work plan which would significantly change the runoff characteristics of the basin. NED retained Metcalf & Eddy to evaluate the effects of these proposed improvements in the basin on the design storm. Results of this study indicated that the SPF would increase from 24,900 to 30,300 cfs.

b. Standard project storm rainfall. The adopted standard project storm rainfall was based upon depth-duration curves of the experienced August 1955 "Diane" rainfall which was centered over the nearby Westfield River basin in Massachusetts. Approximately 18.3 inches of rain fell over 75 square miles in a 48-hour period and 12.5 inches in a 12-hour period. The maximum 6-hour value was 7.9 inches. These amounts are comparable with values from CEB 52-8 for the 6 and 12-hour periods but are considerably higher for the 48-hour duration. A comparison of the adopted SPS rainfall and values from CEB 52-8 and the experienced August 1955 rainfall at Hartford are shown on plate B-6. Since the main branches of the Park River contain a considerable amount of valley storage, the amount of rainfall is an important factor. Hence, the larger volume storm was adopted as the SPS. A tabulation of 6-hour rainfall values from this storm is given in table B-7.

TABLE B-7

ADOPTED STANDARD PROJECT STORM RAINFALL
PARK RIVER BASIN

<u>Time</u>	<u>6-Hour Rainfall (inches)</u>	<u>Losses (inches)</u>	<u>Rainfall Excess (inches)</u>	<u>Rainfall Pattern (inches)</u>
0	-	-	-	-
6	7.9	0.3	7.6	-
12	4.6	0.3	4.3	0.5
18	1.8	0.3	1.5	1.5
24	1.8	0.3	1.5	4.3
30	0.8	0.3	0.5	7.6
36	0.8	0.3	0.5	1.5
42	0.3	0.3	-	0.5
48	0.3	0.3	-	-
TOTAL	18.3	2.4	15.9	15.9

c. Unit hydrographs. Unit hydrographs were derived from analyzing floods recorded at the gaging stations on the North Branch Park River and the Park River. A comparison of the unit hydrographs derived by NED and Metcalf & Eddy are shown on plate B-7. The close agreement in unit hydrographs led to the adoption of the Metcalf & Eddy unit graphs for determining the standard project flood. Because of the large amount of valley storage on the South Branch Park River, the recorded flood hydrographs did not lend themselves to unit hydrograph analysis.

d. Standard project flood. The adopted standard project flood at the Park River gage was derived by applying the selected storm rainfall excess shown in table B-7 to the adopted 6-hour unit hydrograph. At the Park River gage the peak discharge from this flood was 24,900 cfs and referred to by Metcalf & Eddy in their reports as the flood from project storm A. This flood was based on runoff conditions as they existed immediately following the August 1955 flood.

e. Effect of local improvement on standard project flood. The consulting firm of Metcalf & Eddy were retained by NED to evaluate the effect of the present improvements as well as possible future improvements on the adopted standard project storm (see paragraph 6b). Assuming 1955 river conditions but no diversions out of the watershed, subtributary components were developed and routed to the Park River gaging station. The component routings resulted in a peak flow of 25,800 cfs which is only 4 percent greater than the

peak flow of 24,900 cfs obtained by applying storm rainfall to the unit hydrograph at the Park River gage. Plate B-8 shows the standard project flood based on 1955 conditions and also as modified by local improvements. The result of Metcalf & Eddy's investigations are contained in report titled: "Hydrological Investigations and Report on Design Flood, Park River Basin, Connecticut," dated October 1963. Table B-8 gives a summary of results of peak discharges for various improved conditions. The SPF peak of 25,800 cfs would be increased to about 35,000 cfs due to recent channel improvements and highway construction. This peak would be reduced to 30,300 cfs by the eight flood retarding structures in the basin. The net effect of all local improvements since 1955 would be an increase of 4,500 cfs on the peak of the SPF.

The SPF was routed through the valley storage on the North and South Branches assuming a maximum conduit capacity of 18,000 cfs. At Bushnell Park, the headwall of the conduit would be overtopped resulting in the release of about 10,000 acre-feet of water into the downtown section of Hartford. Assuming that floodflows in excess of 18,000 cfs would be contained upstream of the conduit entrance then ponding would occur to about elevation 59 feet msl.

8. SELECTED PLAN OF IMPROVEMENTS

a. General. After careful consideration of the various methods of providing flood protection for the city of Hartford, it was determined to provide local protective works consisting of Park River conduit extensions, a 22-foot diameter auxiliary conduit and pumping station. The protective works are designed to provide protection for the standard project flood. In formulating the plan, it was necessary to consider the following:

- (1) Concurrent elevation of Connecticut River and peak outflow from Park River.
- (2) Effect of open sections in conduit extension.
- (3) Maximum permissible ponding upstream of the existing conduit entrances.

b. Concurrent Connecticut River elevation. Since the improvements on the Park River will consist mainly of completing conduit extensions and constructing an auxiliary conduit, the coincident tailwater elevation is of prime importance in determining the size of an auxiliary conduit. Studies were made of past major floods on

TABLE B-8

SUMMARY OF RESULTS OF PEAK DISCHARGES
FROM ADOPTED SPF

<u>Location</u>	<u>Drainage Area (sq.mi.)</u>	<u>1955 Conditions (cfs*)</u>	<u>Modified by "A" (cfs*)</u>	<u>Modified by "B" (cfs*)</u>	<u>Modified by "C" (cfs*)</u>	<u>Modified by "D" (cfs*)</u>
North Branch Park River at Mouth	27.7	11,450	6,120	7,960	10,400	10,400
South Branch Park River at Mouth	47.0	14,750	14,100	14,900	20,400	23,300
B-16 Park River at River- side Street Gage	74.7	25,800	19,900	22,000	30,300	33,500

* Free unimpeded flows with conduits large enough to discharge these flows

"A" - 8 SCS flood retention reservoirs

"B" - 8 SCS flood retention reservoirs and extension of conduit to the entrances on both branches

"C" - Reservoirs, conduit extensions, South Branch watershed channel improvements

"D" - Reservoirs, conduit extensions, channel improvements and ultimate South Branch conduit to confluence of Piper and Trout Brooks

the Connecticut River and the relative timing of Park River flows. Although local improvements have tended to speed up peak inflows on the North and South Branches, the large volume associated with the SPF utilizes a considerable amount of valley storage causing the peak outflow to occur 6 to 8 hours after the peak inflow. Plate B-9 shows a plot of the elevation hydrographs for the Connecticut River at Hartford for the largest floods of record and the discharge hydrograph of the Park River for the August 1955 flood. It is noted that during the August 1955 flood the Connecticut River peaked only 12 hours after the peak flow on the Park River and at the time of the Park River peak discharge, the Connecticut River was at elevation 26 feet msl and rising about 0.7 feet per hour. High stages on the Connecticut River concurrent with a SPF on the Park River could result from a downstream flood similar to that of August 1955 rather than a general basin flood similar to that of March 1936. For design conditions it was assumed that the Connecticut River was at elevation 30 feet msl at the time of peak outflow from the Park River. Although the Connecticut River has experienced higher stages (37.6 feet in March 1936) it is considered that a high degree of protection will be provided using this design criterion.

c. Effect of open sections in conduit extension. The existing Park River conduit constructed by the Corps of Engineers in 1944, terminated at Bushnell Park about 1 mile downstream of the confluence of the North and South Branches. It is a twin-barrelled conduit, each section about 19.5 feet high and 30 feet wide and contains a total area of 1,160 square feet.

The Connecticut Highway Department has completed two separate sections of conduit extension on the Park River totaling 2,900 feet in length. One section of conduit extension enclosing 2,760 feet of the North Branch and one section enclosing 1,460 feet of the South Branch are now under construction and are shown on plate B-2.

Invert elevations of the conduit sections are approximately 5 to 10 feet lower than the existing riverbed. In order to gain any beneficial effect from the new sections, the remaining portion of the Park River would have to be improved by lowering and widening the river bottom. An improved 30-foot, concrete-lined channel with 1 on 2 side slopes would provide about the same discharge capacity as the conduit extension sections. The improved channel, however, would not provide protection for the SPF unless the banks were either walled or diked or the channel enclosed in a conduit. Because of physical site limitations it was not possible to construct dikes to contain the flood. Although construction cost studies indicated that it would cost about the same either to enclose the channel in a conduit or to provide floodwalls, added benefits

would be derived from enclosing the river in a conduit.

d. Maximum allowable ponding. Initial studies indicated that due to physical limitations it would not be possible to construct an auxiliary conduit large enough to carry the SPF by gravity flow. In order to reduce the size of the auxiliary conduit, the conduit system was surcharged and the peak inflow modified by the valley storage in the lower portions of the North and South Branches. The conduit entrance was structurally designed for 10 feet of surcharge, which is equivalent to elevation 54.5 feet at the South Branch conduit entrance. Using various size auxiliary conduits in conjunction with the main conduit, the SPF inflows on the two Branches were routed through the valley storage to compute the corresponding ponding elevations. For this analysis it was assumed that the existing Park River conduit was extended up both Branches to the conduit entrances. Standard Project flood ponding elevations for various sized auxiliary conduits, supplementing the main conduit discharges, are listed in the following table:

TABLE B-9

PONDING ELEVATIONS VS.
AUXILIARY CONDUIT SIZES

<u>Auxiliary Conduit</u> <u>(diameter in feet)</u>	<u>Ponding Elevation Upstream</u> <u>of North and South Branch</u> <u>Conduit Entrances</u> <u>(elevation, feet msl)</u>
0	59
20	53.5
22	52
25	50.5
30	48

As previously mentioned, the headwall at the South Branch conduit entrance has been constructed to elevation 54.5 feet msl by local interests. A minimum freeboard of 2.5 feet would result in a maximum ponding elevation of 52 feet. The above table shows that a 22-foot auxiliary conduit would result in ponding to 52 feet.

To be compatible with conditions on the South Branch it is proposed to construct a headwall at the North Branch conduit entrance to the same elevation.

9. HYDRAULIC ANALYSIS OF SELECTED PLAN

a. Park River conduit extensions. There are two open sections of conduit which remain and are shown on plate B-2. One length extends from Station 8+68 to Station 21+0, the other from Station 38+10 on the Park River to Station 12+30 on the North Branch. Completion of these conduit extensions will make the Park River conduit continuous from the Connecticut River to the entrances on the North and South Branches. The sections will conform in size and shape to be consistent with the existing conduits as follows:

Park River - each barrel 26.5 feet high by 34 feet wide
North Branch - each 25 feet by 22 feet wide
South Branch - each 27.5 feet by 36 feet wide

Typical conduit sections are shown on plates E-3 and E-4. Rating curves were also computed ($n=.013$) for normal flows and with various coincident Connecticut River elevations and are shown on plate B-11.

b. Auxiliary conduit. A 22-foot diameter conduit will be constructed to supplement the capacity of the main conduit during large floods. The conduit will extend from the junction structure eastward to the Connecticut River, a distance of approximately 9,500 feet and is shown on plates B-2 and E-5. Provisionally, the invert of the auxiliary at the junction structure (Station 99+0) is plus 16 feet msl. It slopes to minus 12 feet at Station 45+0 and then to minus 14 feet msl at exit portal (Station 8+50). The invert elevation in the lower portion of the conduit was governed by existing street and interstate highway grades. A discharge rating curve at station 98+0 is shown on plate B-11. With the Connecticut River at elevation 30 feet msl and the head pools at elevation 52 feet msl, the discharge capacity of the auxiliary conduit is about 5,500 cfs. Diversion of floodflows into this conduit would tentatively begin when Park River flows exceed 1,500 cfs (about 20 csm.).

10. INTERIOR DRAINAGE

a. General. The interior drainage analysis was performed in accordance with procedures outlined in EM 1110-2-1410 "Interior Drainage of Leveed Urban Areas: Hydrology."

b. Description. The area affected by the proposed plan of improvements extends upstream on the Park River from about Broad Street to the vicinity of Farmington Avenue on the North Branch and Hamilton Street on the South Branch. A portion of the area also has been affected by the construction of the route 84 interstate highway system. This area has been primarily developed for residential, commercial and industrial purposes with park land comprising a small portion.

The storm drainage system is separate from the sanitary sewer system, and includes drains from both high and low level areas. High level drains discharge directly to the Park River through the conduit wall and can be surcharged during high conduit stages without causing damage. The high level drainage systems were designed by the Greater Hartford Flood Commission to discharge runoff from a 25-year storm, and have been constructed in conjunction with completed sections of the conduit extensions.

The low level drainage area comprises 171 acres almost all of which are used for residential, commercial or industrial purposes. A class I category (concentrated commercial and industrial sections) has been selected as being indicative of the area. The topography is relatively flat. The GHFC has designed the low level drainage system to carry flows from a 50-year storm and portions of the collector systems have been constructed adjacent to the completed sections of the conduit extensions. This system is divided into four collector drains which will convey the flow into a pumping station. Gravity flow will occur when low or moderate river stages in the conduit occur, but pumping will be required during high conduit stages. Pertinent data on the four storm drains designed by GHFC are listed below:

<u>Storm Drain Size</u> (dia. in inches)	<u>Drainage Area</u> (acres)	<u>Gravity Discharge- Design Flow</u> (cfs)
84	102	250
72	54	137
36	10	33
15	<u>5</u>	<u>8</u>
TOTAL	171	428

The pumping station will be provisionally designed to discharge a flow of 428 cfs through the gravity outfall.

c. Coincident riverflows and interior runoff.

(1) General. Preliminary studies indicate that pumps will not be necessary to discharge interior runoff when river stages in the conduit are below 28 feet msl at the pumping station, equivalent to flows less than 5,000 cfs. This insures a satisfactory gradient in the drainage system during gravity flow. As previously noted: (a) the proposed conduit invert is considerably lower than the existing river bottom, see plate E-2, and (b) diversion of floodflows into the auxiliary conduit occurs when riverflows exceed 1,500 cfs.

(2) Experienced coincident rainfall. The five largest

floods of record on the Park River are shown in table B-5. A study of the Hartford rainfall records show the most intense rainfalls that occurred concurrently with the Park River flows above 4,000 cfs to be the following:

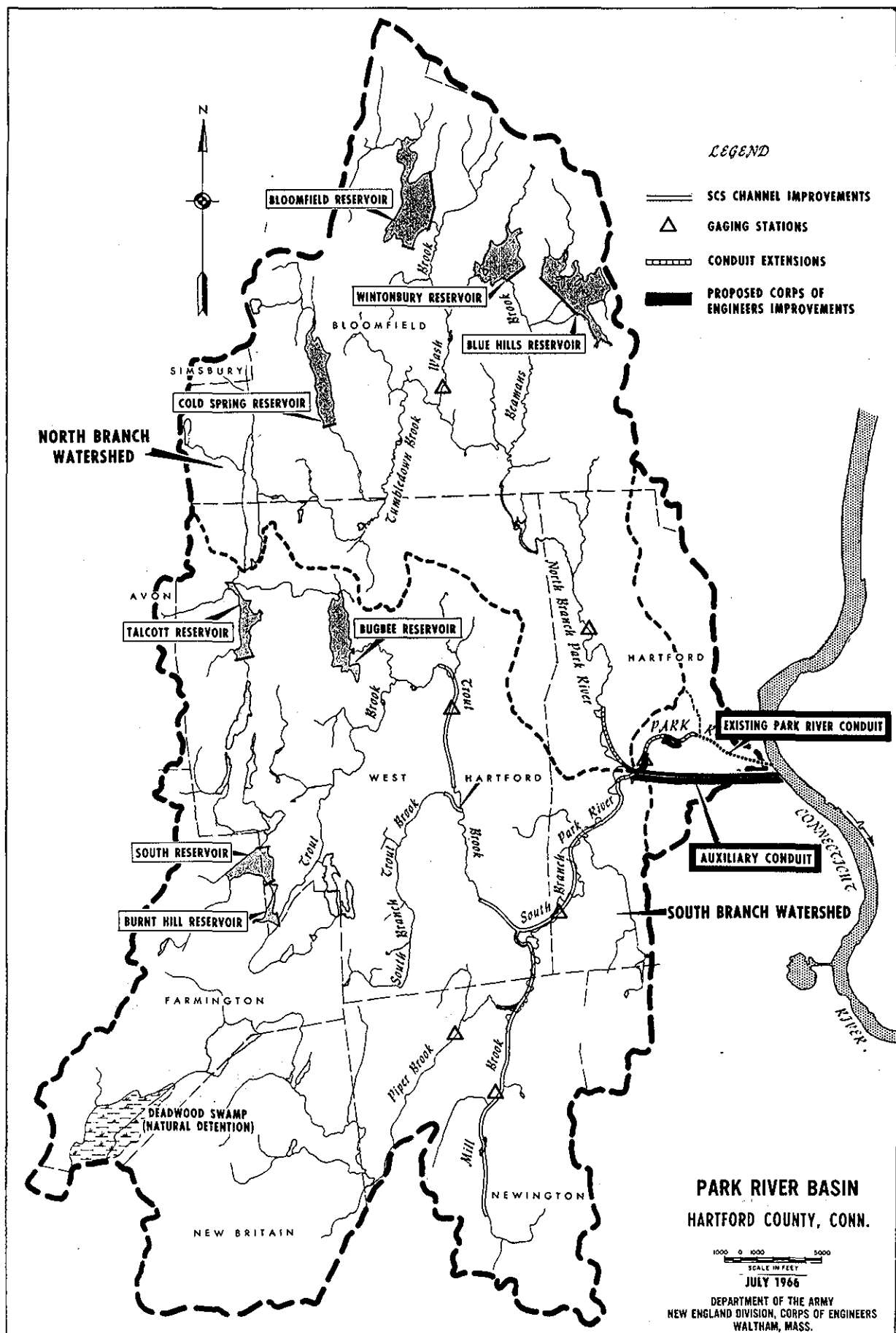
August	1955	Q =	4,500 cfs,	rainfall =	1.35 inch/hour
September	1938	Q =	5,100 cfs,	rainfall =	0.75 inch/hour

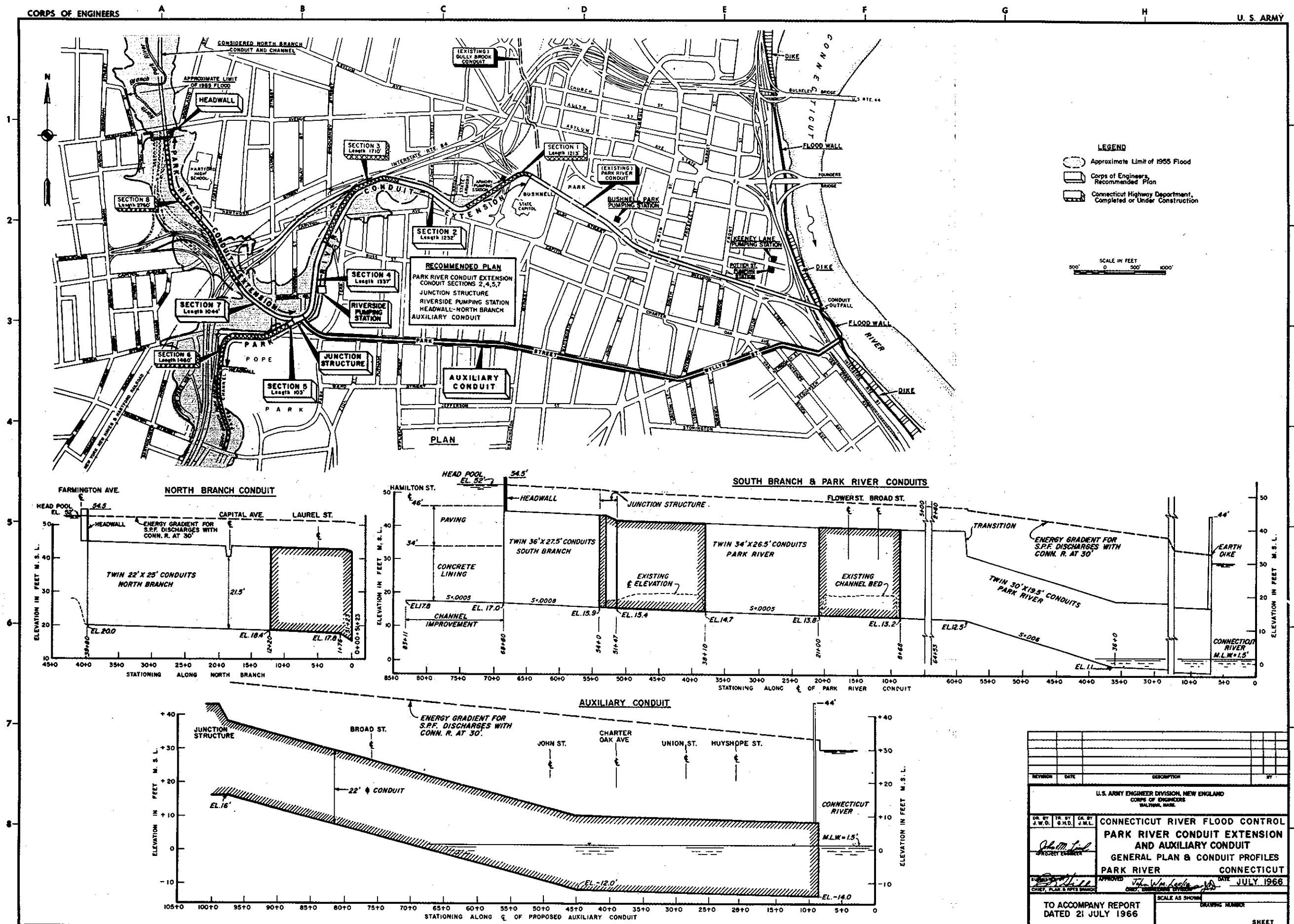
All other concurrent rainfall for flows above 4,000 cfs had intensities less than 0.25 inch/hour.

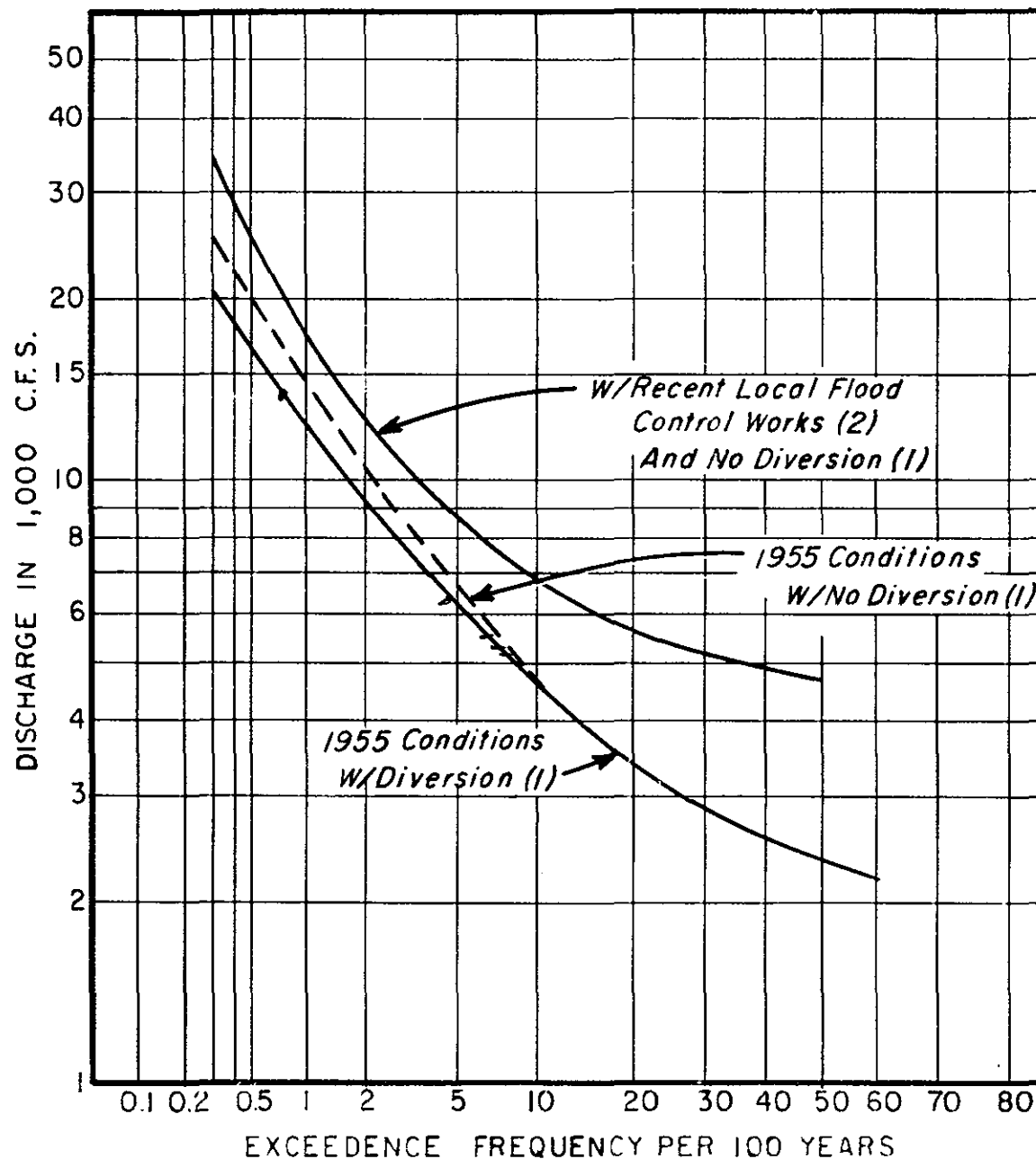
d. Design rainfall and runoff. A 5-year, 1-hour rainfall of 1.65 inches per hour has been selected as occurring during periods when the conduit stages are high enough to necessitate pumping. The furthest point from the pumping station in the low level drainage area is 5,500 feet which results in a concentration time of about 30 minutes. Using the rational formula, $Q = CIA$, to determine a peak flow, with $C = 0.65$, $i = 2.6"/hr.$, $A = 171$ acres, results in a discharge of 290 cfs.

e. Pumping station. The pumping station has been tentatively located on the right bank of the Park River in the vicinity of Riverside Street and will collect runoff from both sides of the river. The pumps will discharge a flow of 250 cfs, equivalent to 1.5 inches of runoff per hour, against a head differential of about 30 feet which would occur during a standard project flood.

f. Ponding. With the inclosure of the Park River in a conduit, the area adjacent to and over the river will increase in value due to economic development. For this reason, it is not considered feasible to reserve areas for temporary storage of interior floodflows during periods when pumping is required. It is possible to allow ponding in streets, parking areas, etc. for short periods of time, but the potential ponding and subsequent damages cannot be adequately determined at this time due to the considerable amount of conduit construction and urban redevelopment presently taking place. During the preparation of the design memorandum, further consideration will be given to the adequacy and design of the gravity outfall, pumping capacity, ponding and potential damage.

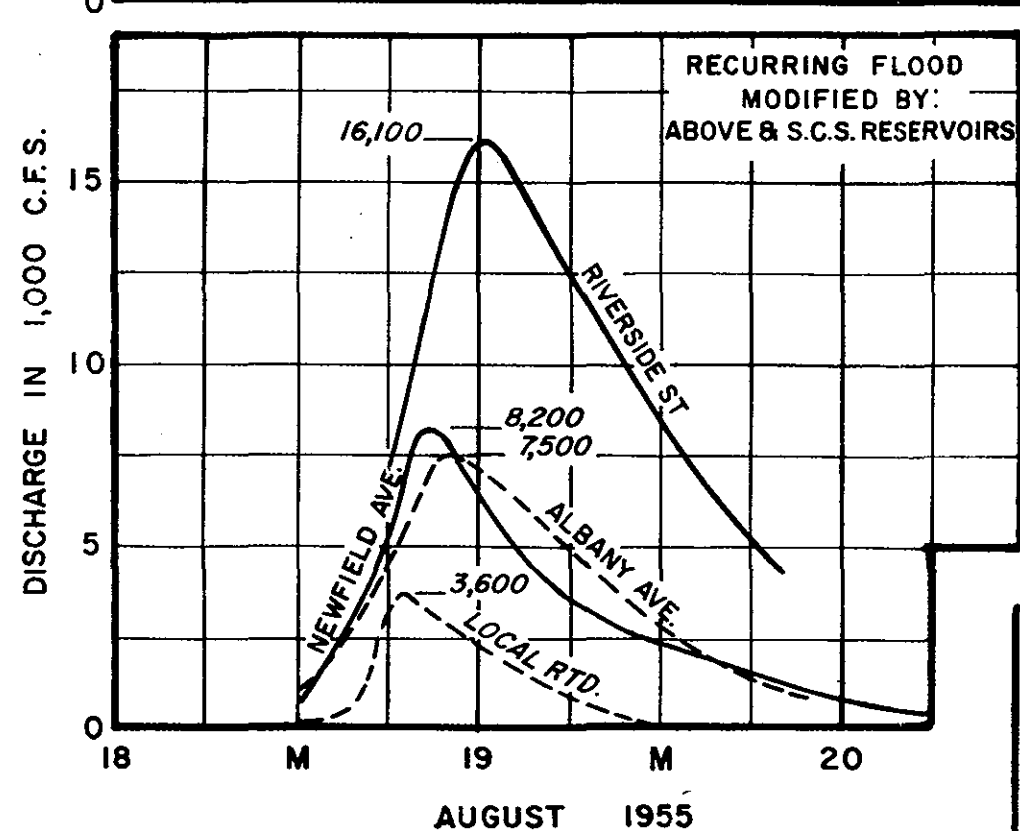
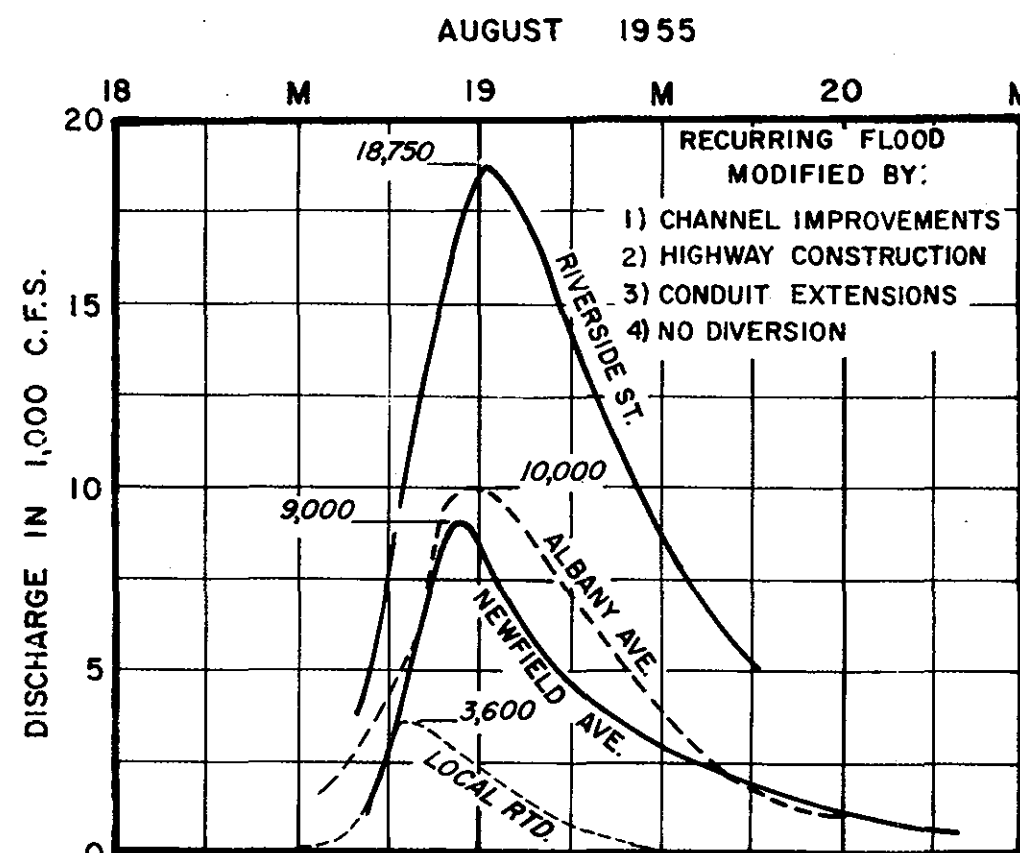
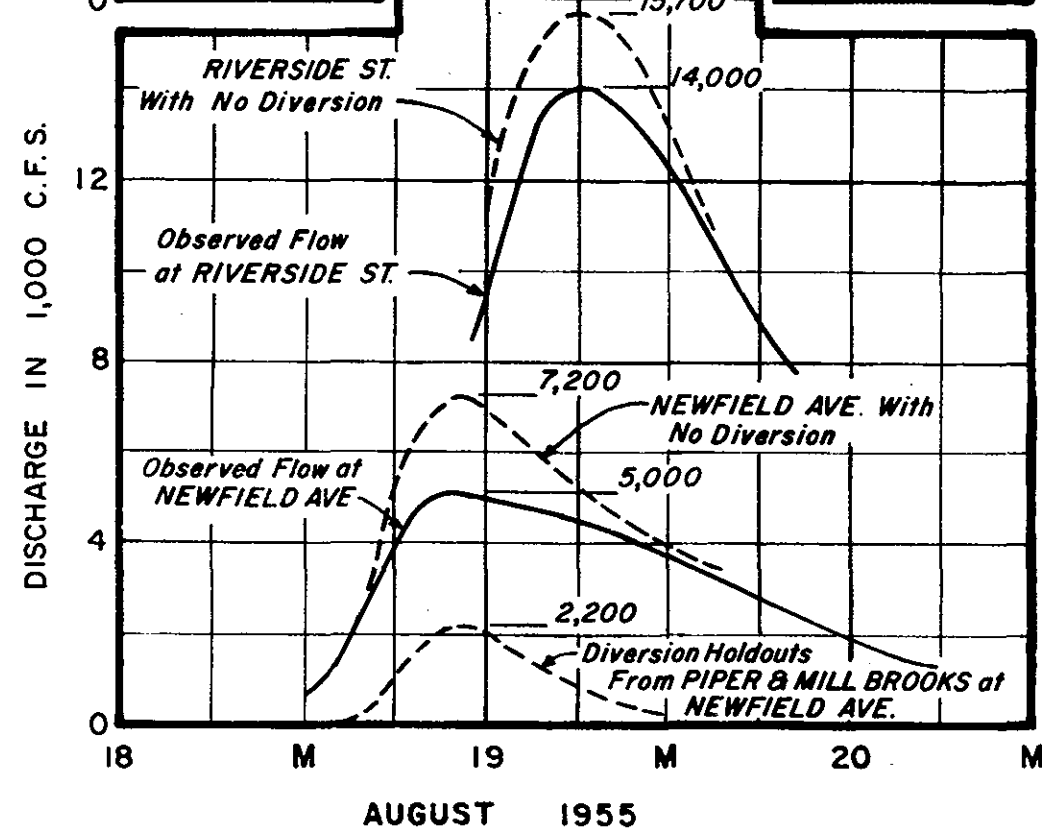
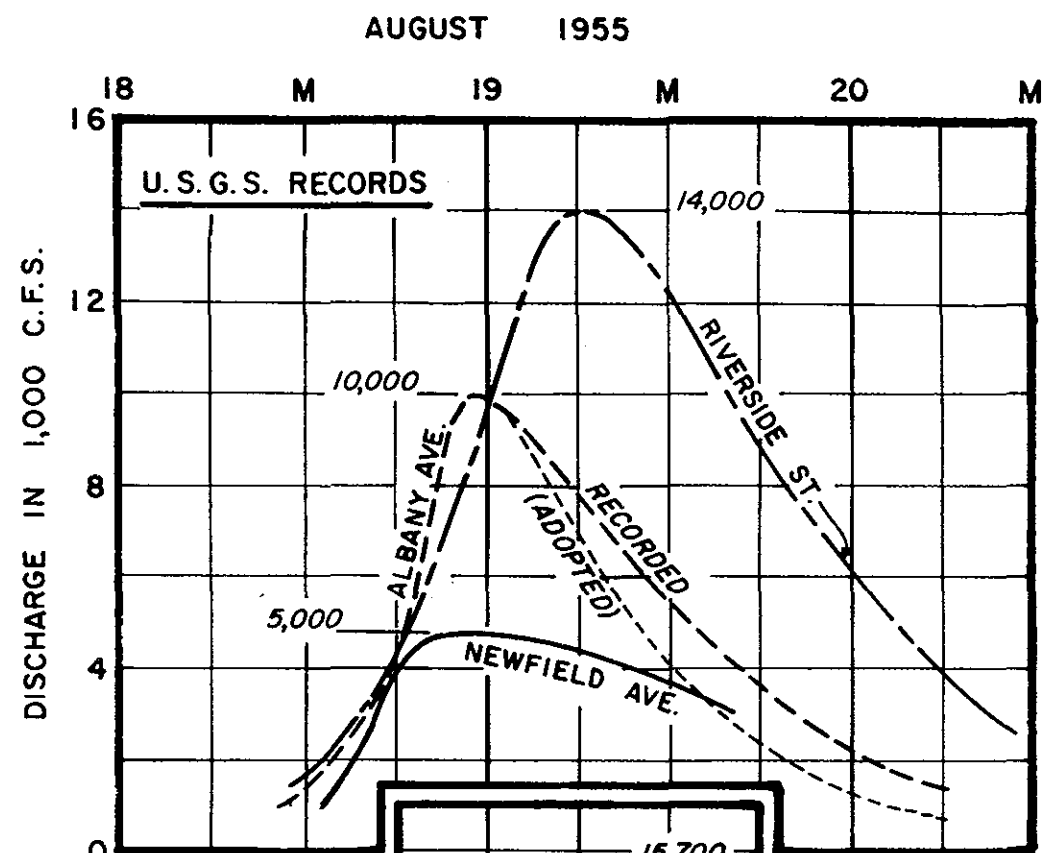






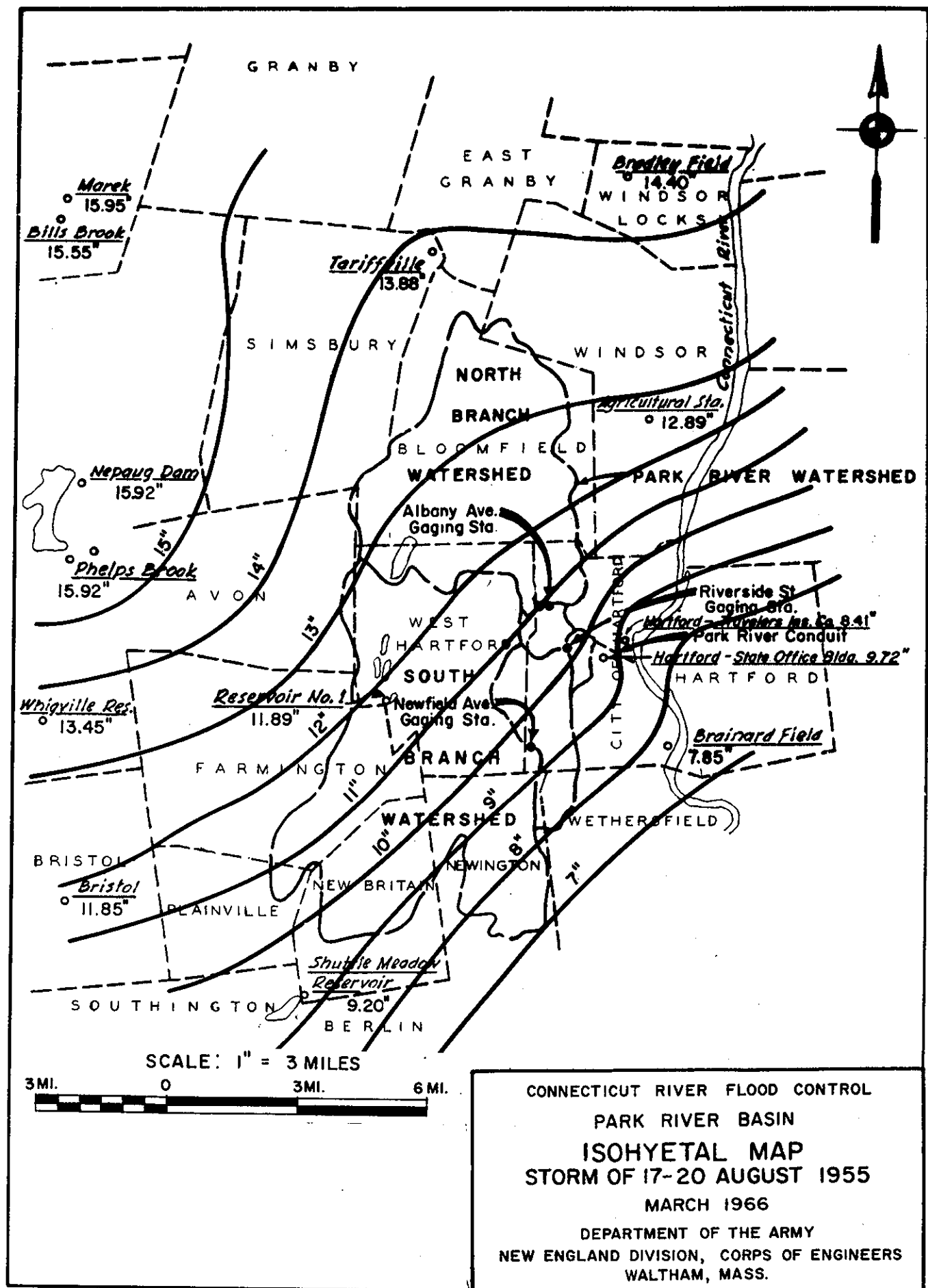
- (1) Diversions Out of Watershed Occur at Mill and Piper Brooks.
- (2) Flood Control Works Include:
8 S.C.S. Reservoirs.
Channel Improvements
Conduit Extensions
Highway Construction
- (3) Channel Capacity of Park River Assumed Adequate To Discharge All Flows.

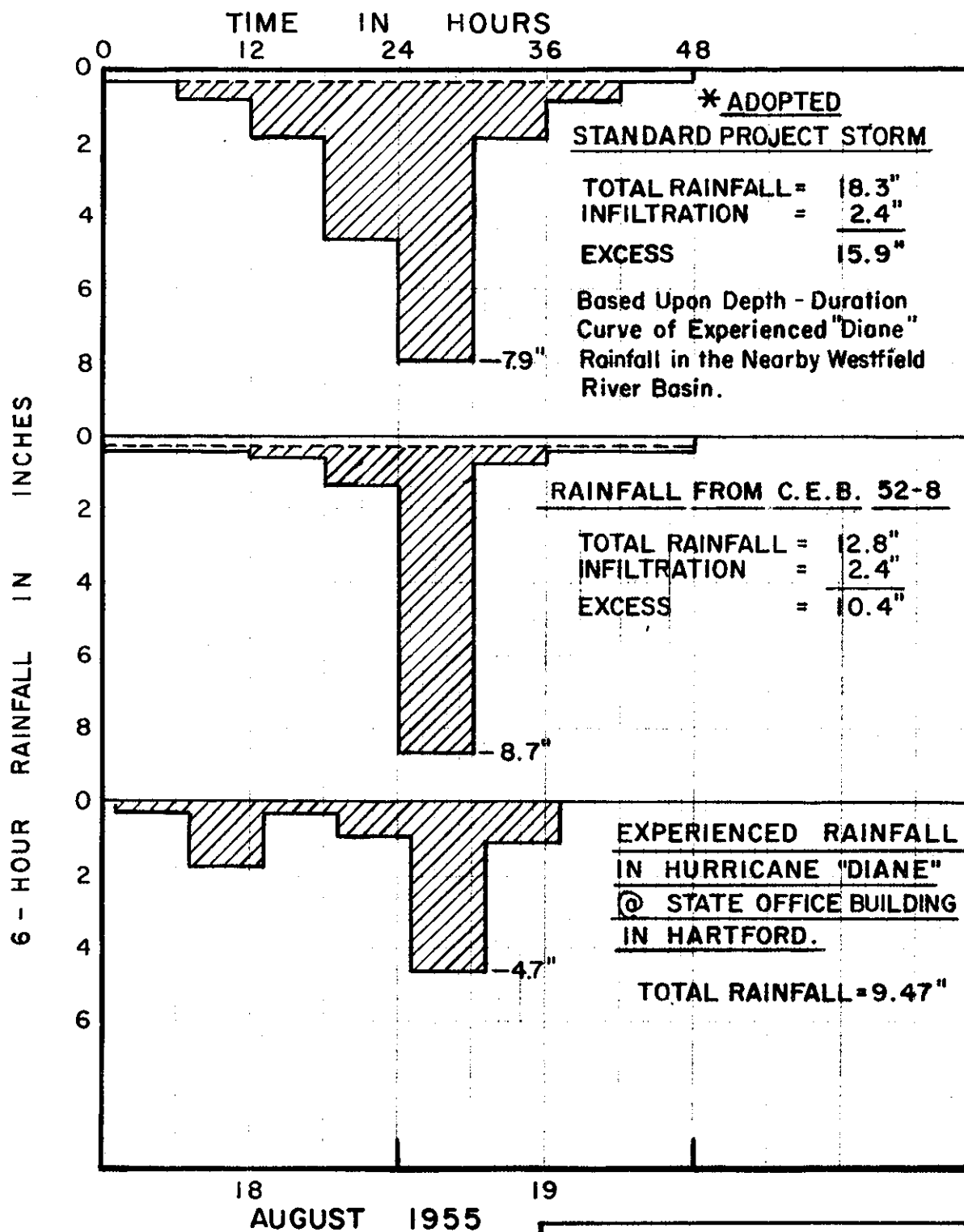
CONNECTICUT RIVER FLOOD CONTROL
PARK RIVER BASIN
 DISCHARGE FREQUENCY CURVES
 PARK RIVER @ RIVERSIDE ST.
 MARCH 1966
 DEPARTMENT OF THE ARMY
 NEW ENGLAND DIVISION, CORPS OF ENGINEERS
 WALTHAM, MASS.



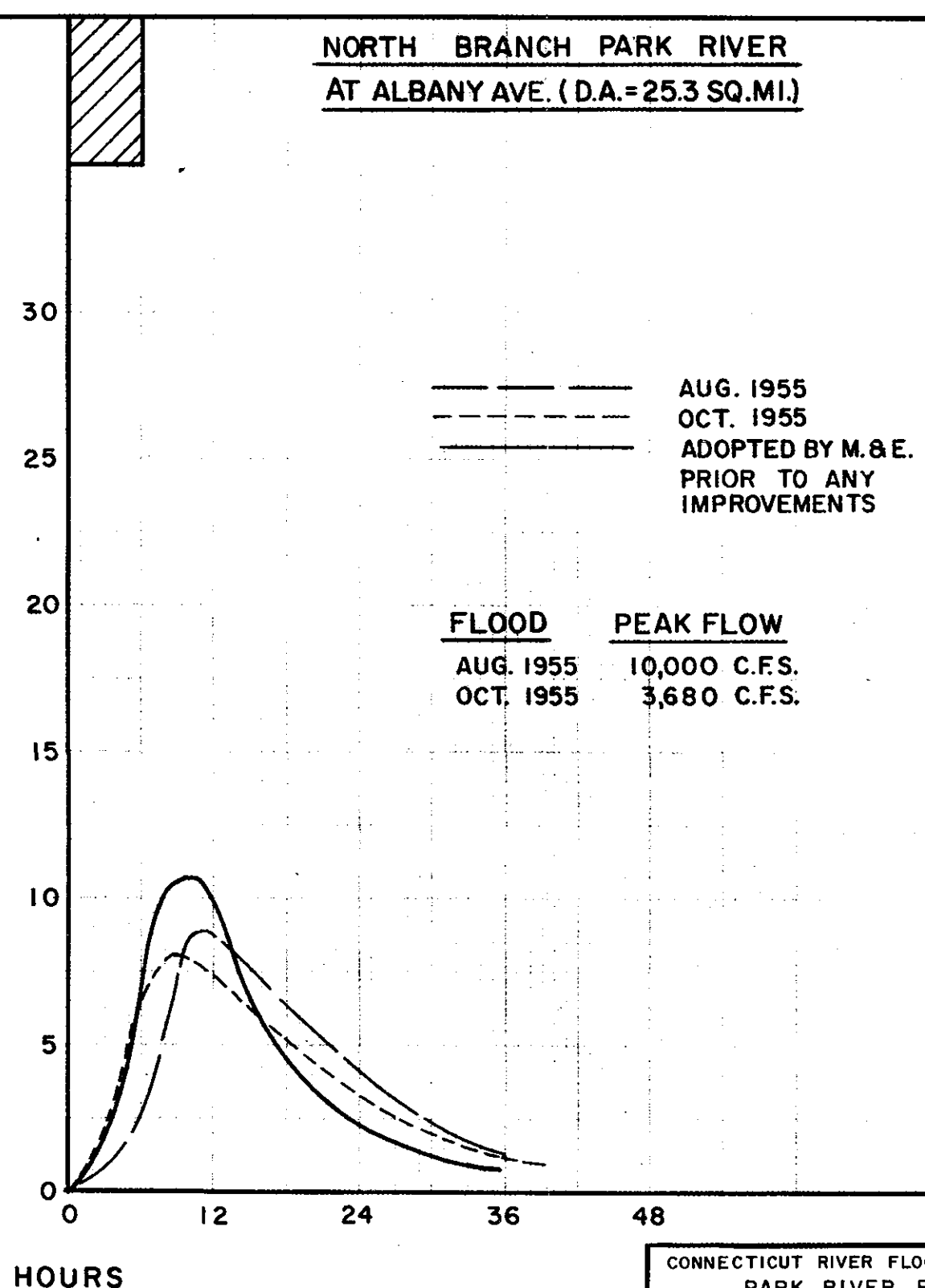
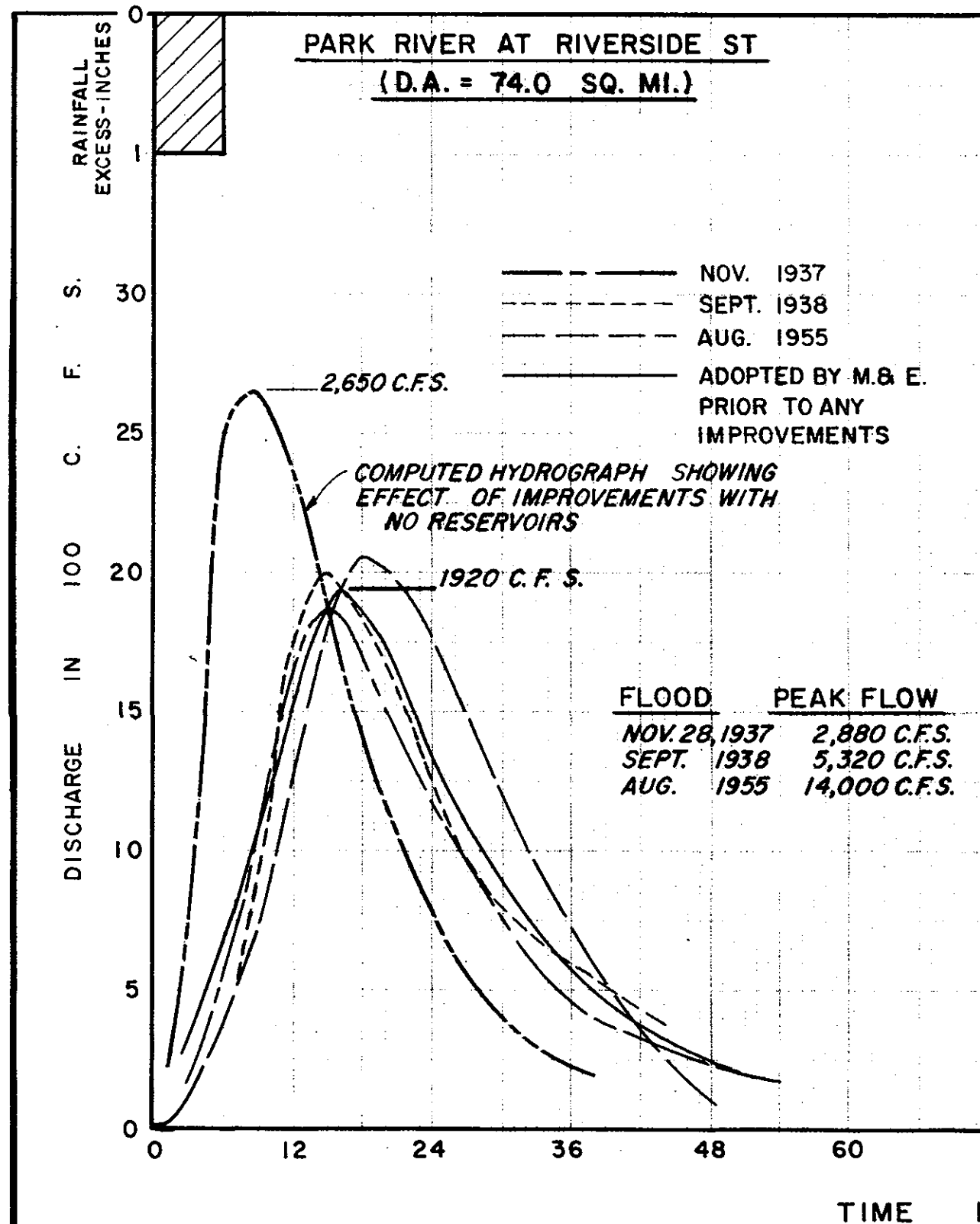
DRAINAGE AREAS	
PARK R. at RIVERSIDE ST.	74.0 Sq.Mi.
N. BRANCH at ALBANY AVE.	25.3 Sq.Mi.
S. BRANCH at NEWFIELD AVE.	40.6 Sq.Mi.
LOCAL on BOTH BRANCHES	8.1 Sq.Mi.

CONNECTICUT RIVER FLOOD CONTROL
 PARK RIVER BASIN
 AUGUST 1955
 FLOOD ANALYSIS
 MARCH 1966
 DEPARTMENT OF THE ARMY
 NEW ENGLAND DIVISION, CORPS OF ENGINEERS
 WALTHAM, MASS.





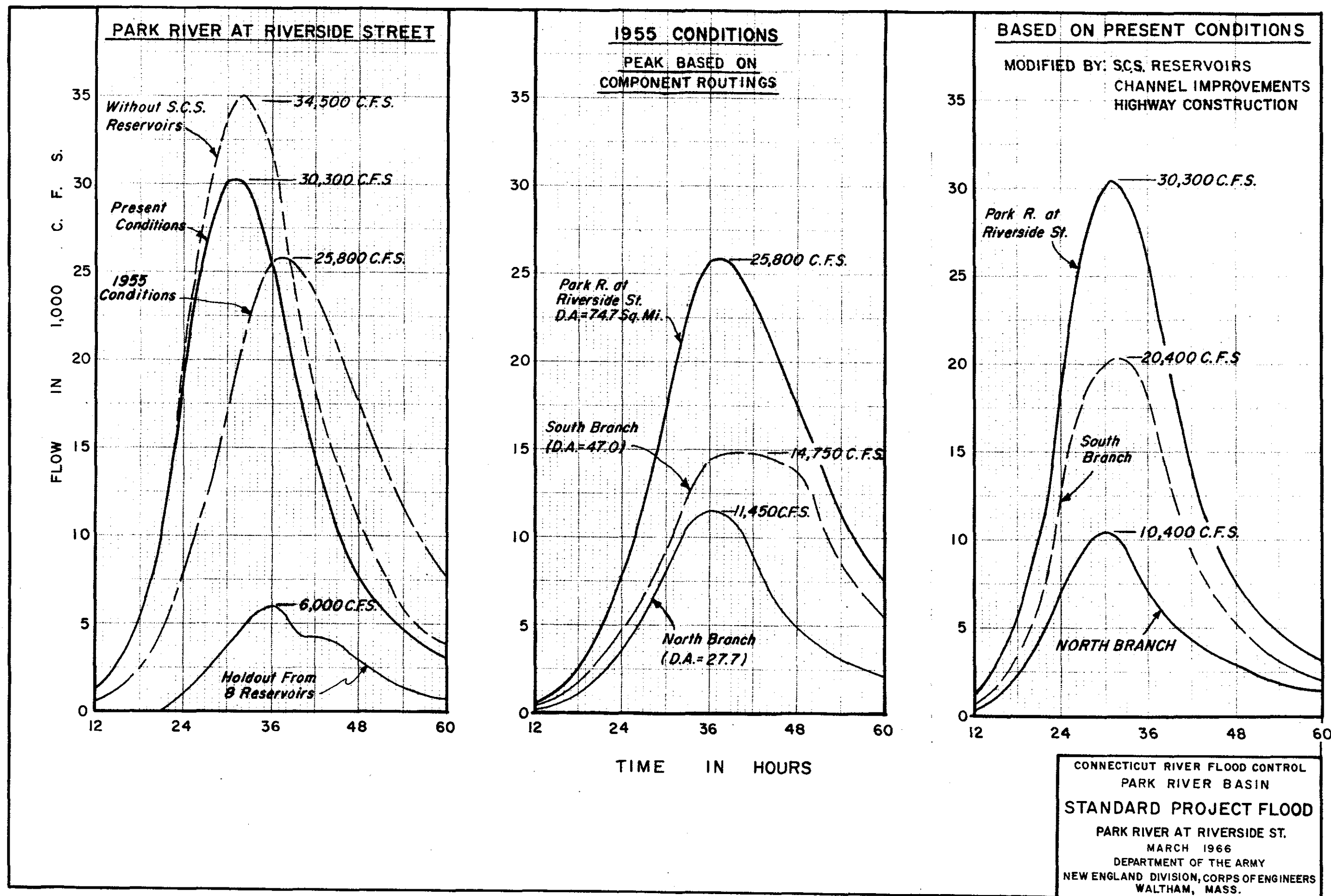
CONNECTICUT RIVER FLOOD CONTROL
PARK RIVER BASIN
COMPARISON OF
STORM RAINFALLS
MARCH 1966
DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS.

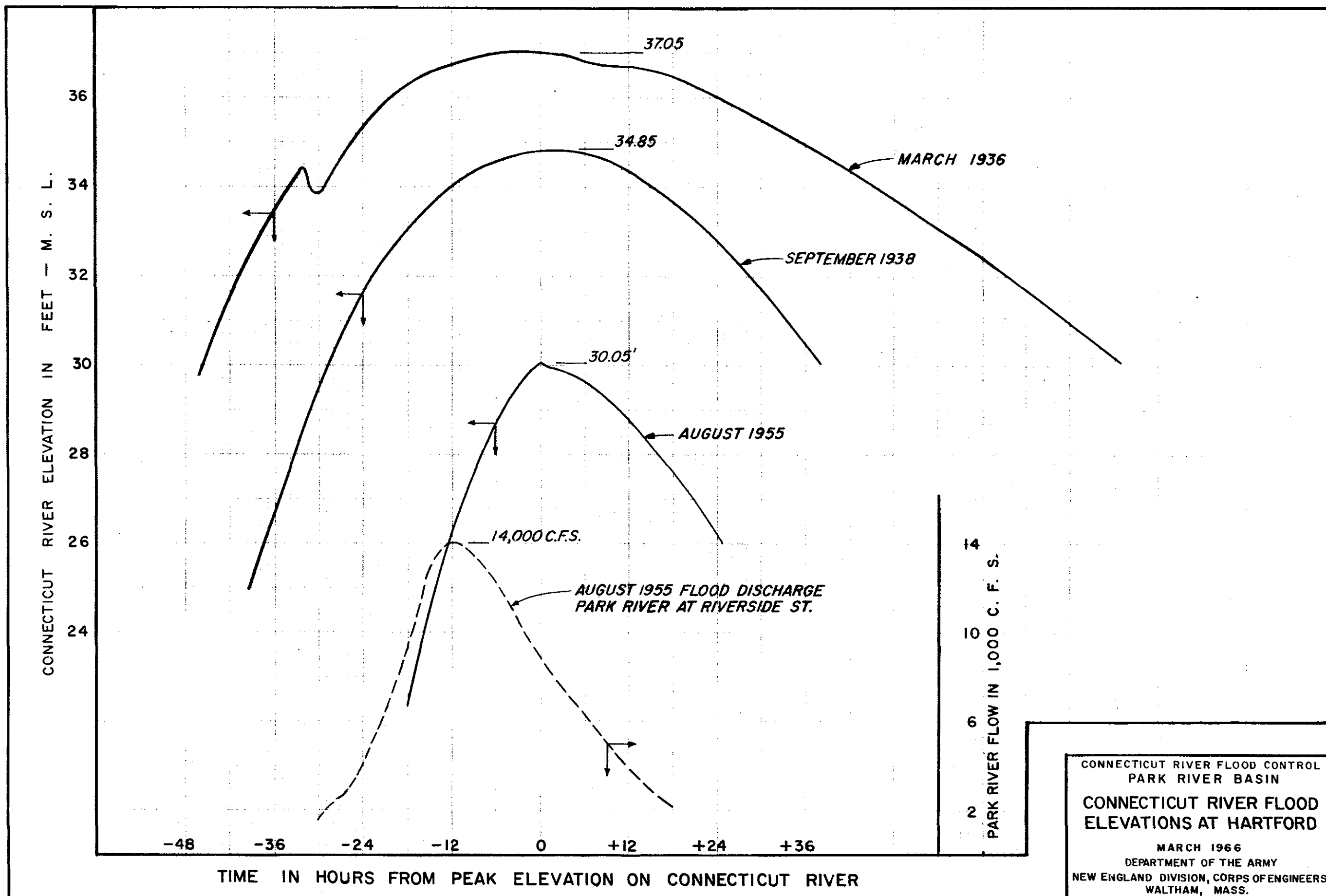


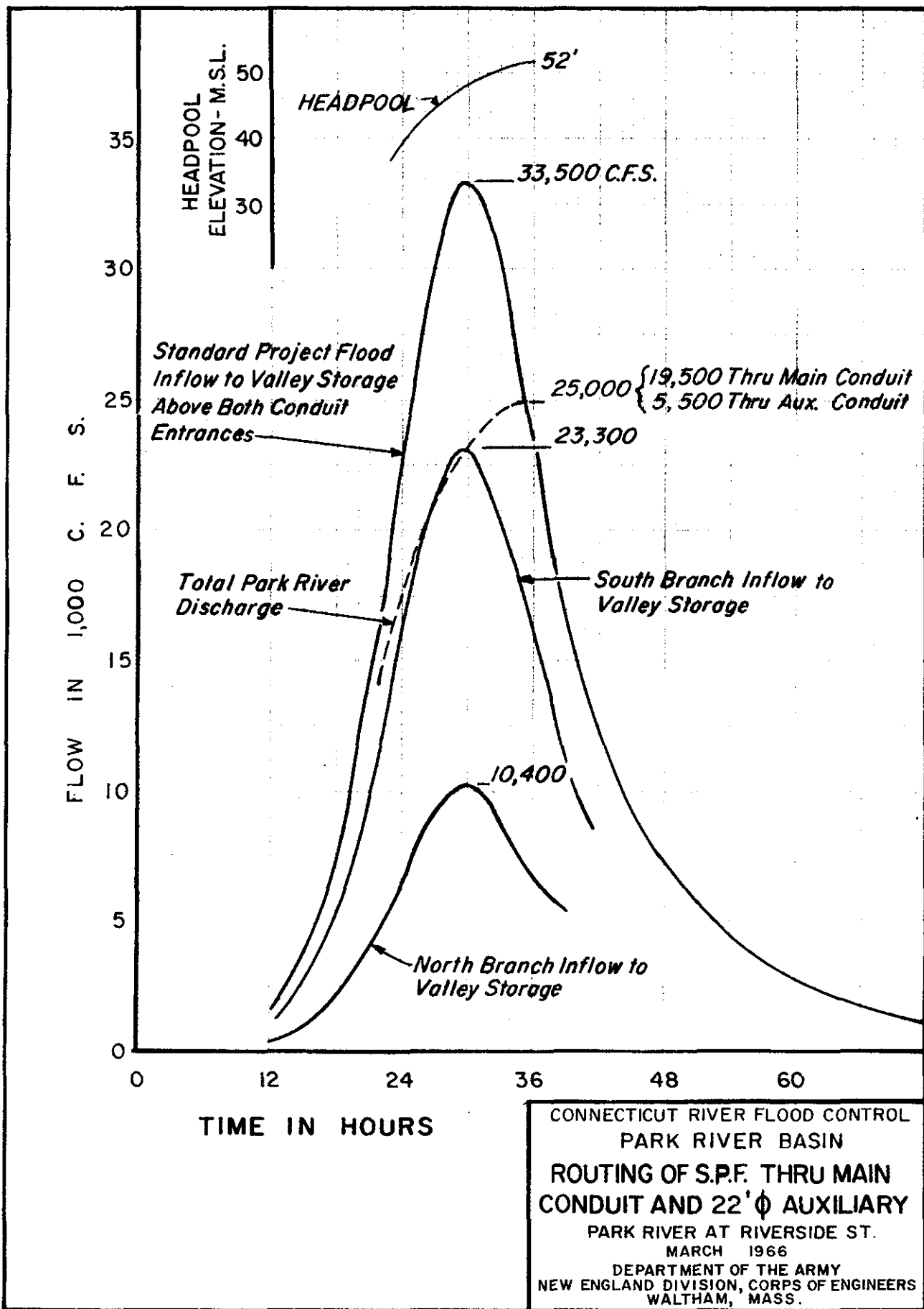
CONNECTICUT RIVER FLOOD CONTROL
PARK RIVER BASIN

UNIT HYDROGRAPHS

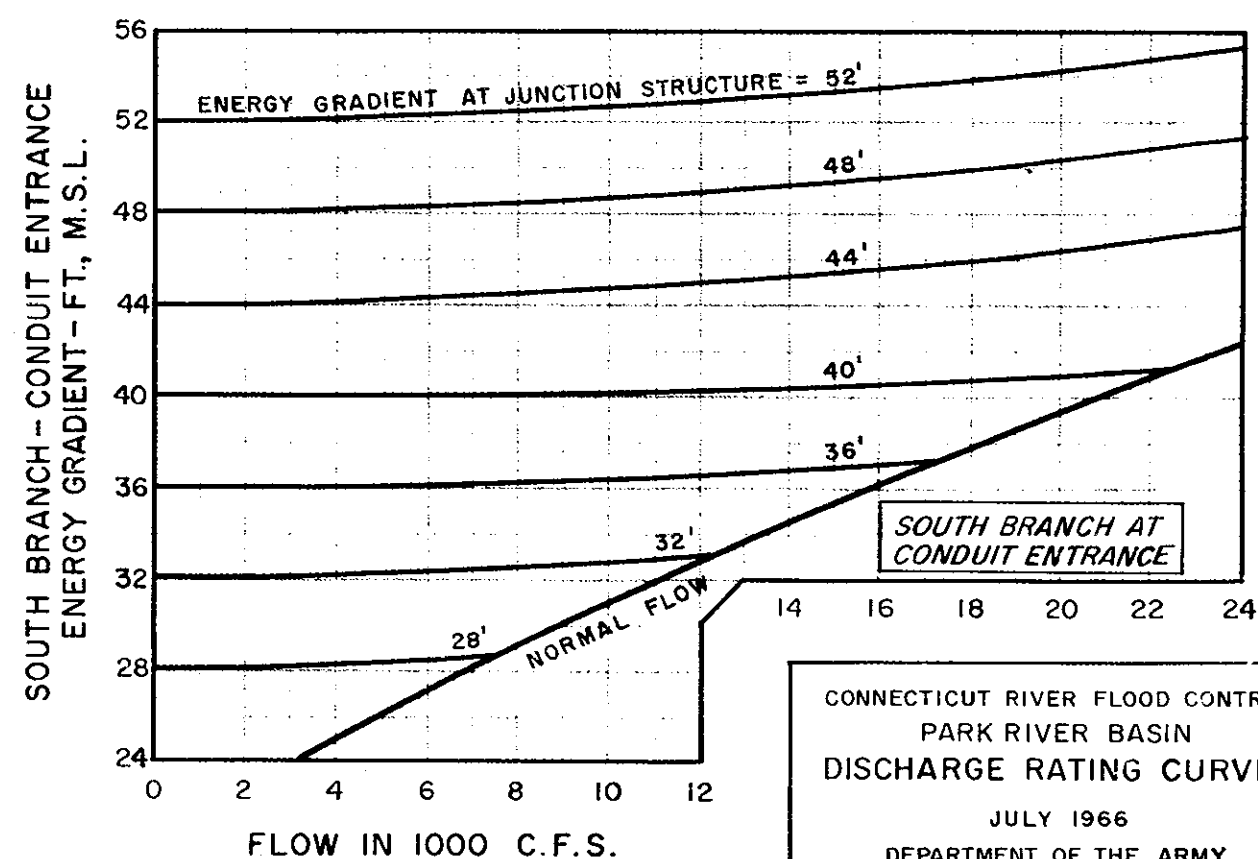
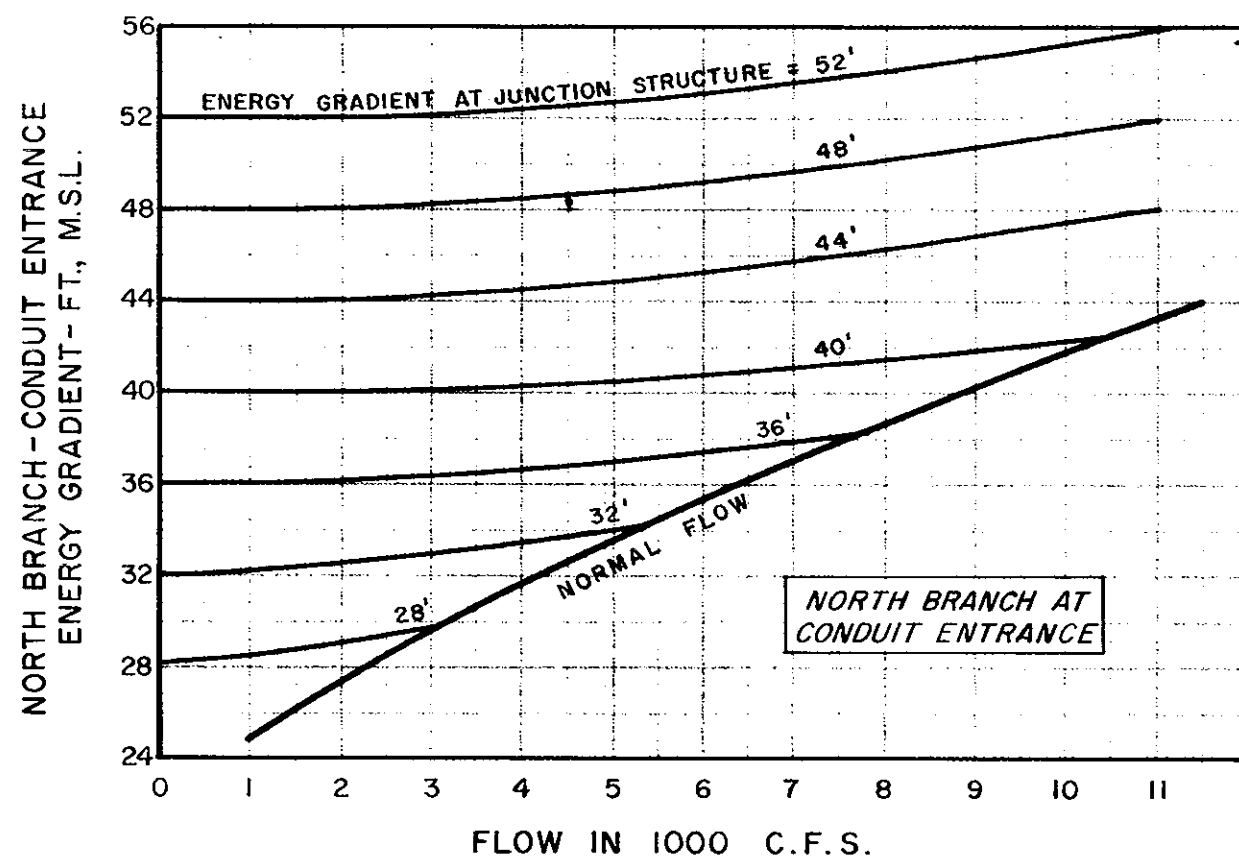
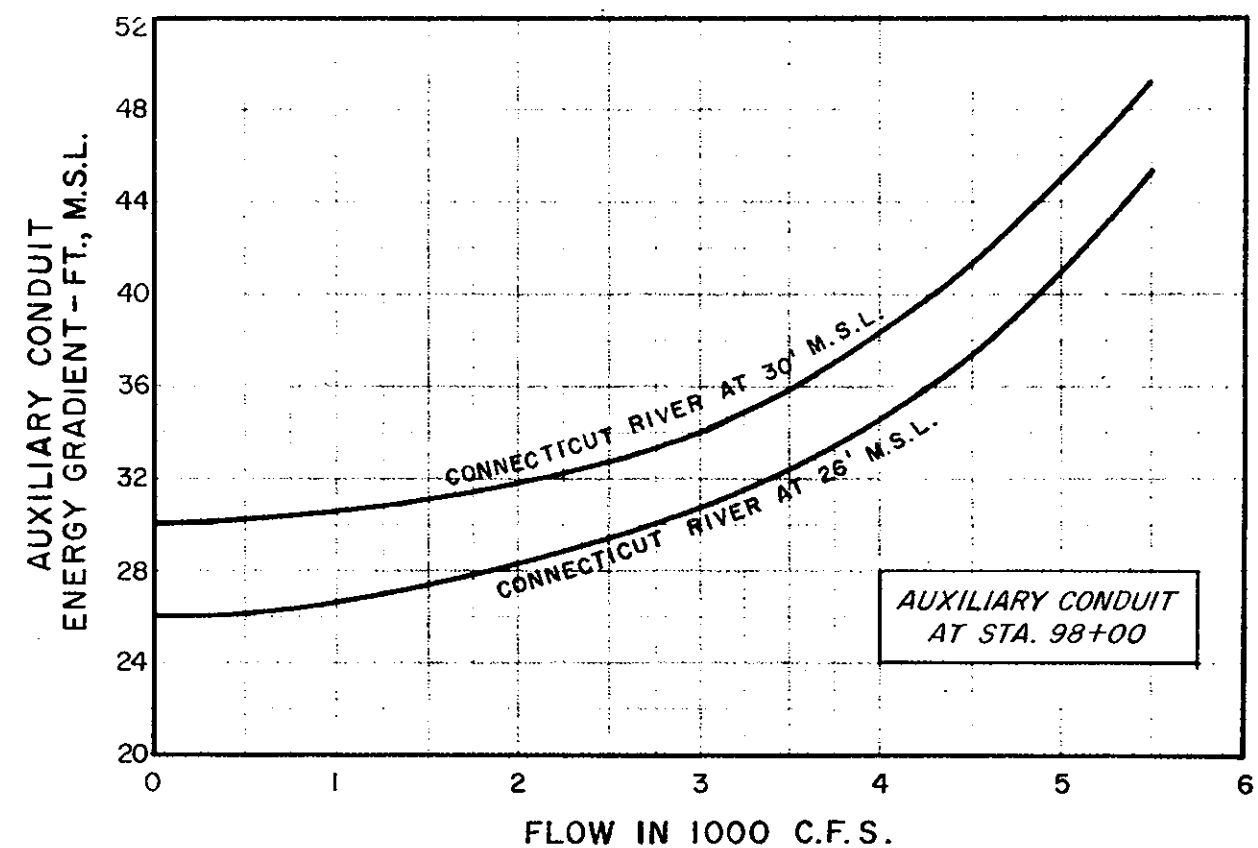
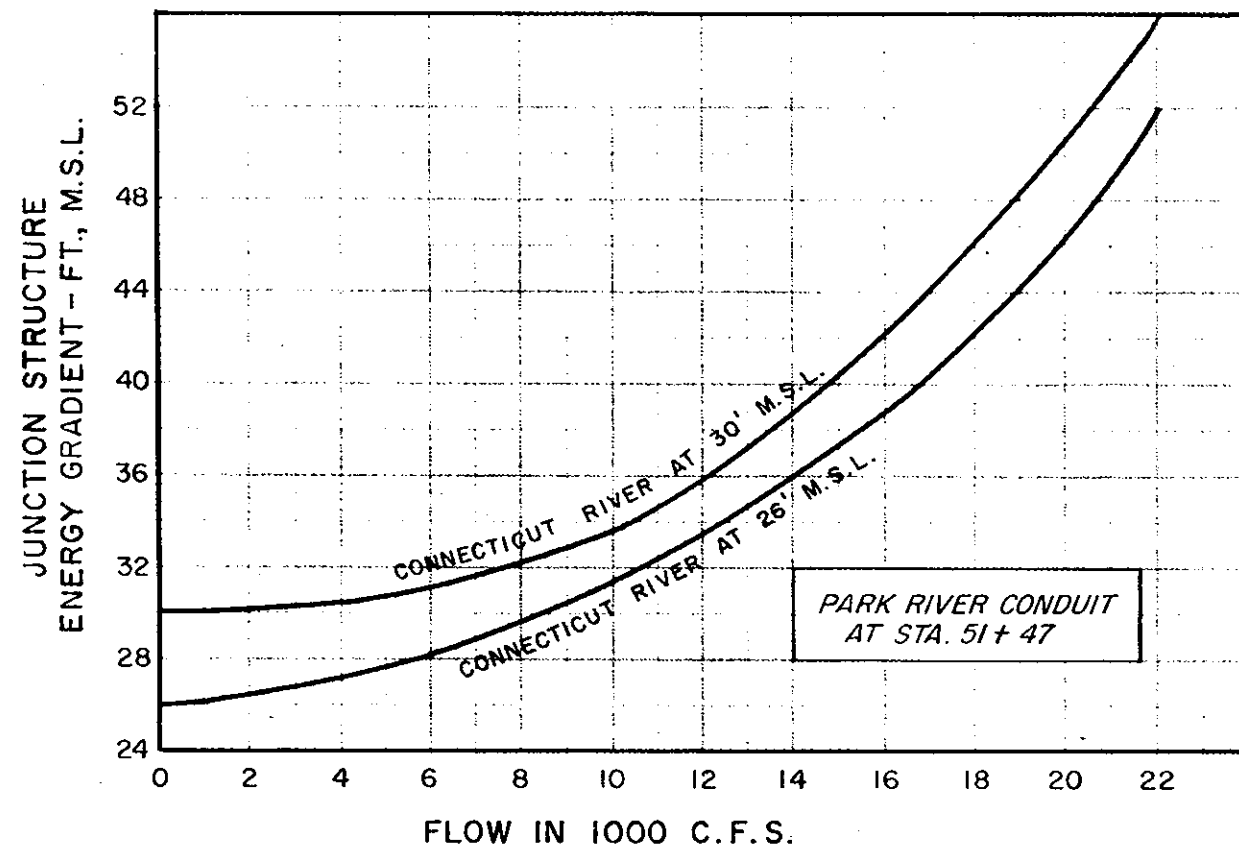
MARCH 1966
DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS.







CONNECTICUT RIVER FLOOD CONTROL
PARK RIVER BASIN
ROUTING OF S.P.F. THRU MAIN
CONDUIT AND 22' ϕ AUXILIARY
PARK RIVER AT RIVERSIDE ST.
MARCH 1966
DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS.



CONNECTICUT RIVER FLOOD CONTROL
 PARK RIVER BASIN
 DISCHARGE RATING CURVES
 JULY 1966
 DEPARTMENT OF THE ARMY
 NEW ENGLAND DIVISION, CORPS OF ENGINEERS
 WALTHAM, MASS.

APPENDIX C

ECONOMIC DEVELOPMENT

APPENDIX C
ECONOMIC DEVELOPMENT

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APPENDIX C

ECONOMIC DEVELOPMENT

PRESENT CONDITIONS

1. GENERAL

Hartford is the capital of Connecticut and its most populous city. Located at the head of navigation on the Connecticut River the city lies slightly to the north of the geographic center of the state and is less than an hour's drive from all parts of the state except for lower Fairfield County.

2. TRANSPORTATION

The Greater Hartford area is the nexus of the State's Highway system with two of its interstate Highways, I-91 and I-84, and eight state routes connecting the city to all parts of the state and to its adjoining neighbors, New York, Massachusetts and Rhode Island. Construction on I-91 to the south and I-84 to the southwest is in progress and completion is expected well before the 1972 deadline for the entire Interstate System. Both highways are in operation to the Massachusetts line to the north and northeast. To the south and west State Route 15, the Wilbur Cross Parkway, connects the city to Fairfield County and the New York City area. Other major State Routes radiating from the area are 2, 4, 5, 6, 9 and 44.

The New Haven Railroad serves Hartford, providing both freight and passenger service. Passenger trains connect the city to Springfield to the north and New Haven, Bridgeport and New York City to the south. Freight service is furnished with 200 industrial sidings serving 225 industries in the Greater Hartford Area, numerous team tracks for public use and full "piggy-back" service facilities for trailer transport.

Air freight and passenger service for Greater Hartford is supplied at Bradley Field in Windsor Locks, about 25 minutes drive from the center of Hartford. Seven passenger carrying airlines serve the airport; Alleghany, American, Eastern and Mohawk, Northeast, TWA and United.

The Connecticut River is navigable with a 15-foot improved channel from Long Island Sound to Hartford. In 1963, the last year for which complete data are available, tonnage of water borne products on the

river amounted to 3,000,000 tons. Over 95 percent of the tonnage was petroleum products, the balance being bituminous coal and some bulk chemical products.

3. POPULATION

Hartford is the core city of an SMSA with a 1960 population of 525,207. During the decade 1950-1960 the core city declined in population by 8.6 percent following the nation-wide trend of movement to the suburbs but the SMSA had a growth of 29.2 percent overall, exceeding the growth rate of the state (26.3 percent) and of Hartford County as a whole.

4. ECONOMY

The economy of Hartford is a vigorous one, with a diversified mix of manufacturing, wholesale and retail trade, insurance and finance. Government is also a larger than normal employer in Hartford with the state government centered there. The home offices of several of the country's largest insurance companies in their respective fields are located in Hartford. Total employment in the insurance industry amounts to approximately 10 percent of the work force in the Hartford Labor Market Area. Manufacturing, the largest single employer in the Hartford Labor Market Area, accounts for 32.4 percent of the labor force. Among its principal products, in Hartford, are typewriters, small arms, ball bearings and electrical equipment. The city is also the shopping center for central Connecticut and trade and services are important employers. The unemployment rate, 3.7 percent in March 1965, was 16 percent below the National average.

5. LAND USE

Based on 1960 Census data Hartford has a gross population density of 8719 per square mile. When the areas of the public parks and state owned facilities in the city are taken into account the density is in excess of 12,000 per square mile. Past practice in building was such that there is little vacant land available for new construction.

FUTURE CONDITIONS

6. GENERAL

All indicators point to a continuing growth in economic activity and population for the SMSA of which Hartford is the center. The

Capital Region Planning Agency, a State sponsored agency, in a report in 1961 projected a population growth of two and a half times in the next 50 years for the Hartford area. Data from a projective Economic Study of New England and parts thereof being prosecuted in connection with the Comprehensive Survey of the Connecticut River Basin confirms the Region Planning Agency's projection and indicates a continuing rise in the level of economic activity.

Such a growth in population with the increase in economic activity necessary to support it will place such a demand on land in Hartford that every usable plot and existing building will be put to its highest use. Because of its location in the heart of Hartford the flood plain of the Park River will feel the demand as soon as protection is provided.

APPENDIX D

FLOOD LOSSES AND BENEFITS

APPENDIX D
FLOOD LOSSES AND BENEFITS

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APPENDIX D

FLOOD LOSSES AND BENEFITS

1. DAMAGE SURVEYS

Following the flood of August 1955, the Greater Hartford Flood Control Commission engaged a private engineering company to make a survey of the damages. Physical losses and some non-physical losses were evaluated. Much of the data collected in the survey was rendered obsolete by changes in use and by land taking in connection with construction of Interstate Route I-84, which traverses the basin. In 1964 and early 1965, Corps of Engineers personnel made a damage survey of the basin. Data from the earlier survey were used to determine depths of flooding but a complete re-evaluation of losses was made in the light of current physical and economic conditions. The damage survey consisted of door-to-door interviews and inspections of residential, commercial, industrial and other properties within the flood plain. Recorded information included extent of the areas flooded, description of the properties, nature and amount of damages, depth of flooding, high water references and relationships to prior flood stages. Damage data were generally furnished by property owners or tenants. Engineers and analysts prepared estimates on the basis of these data and developed their own estimates when owner or tenant estimates were unavailable.

Sufficient data were obtained to derive losses for: (1) the 1955 flood crest, (2) a stage 5 feet higher, (3) the stage where damage begins referenced to the 1955 flood crest, and (4) intermediate stages where marked increases in damage occur.

2. LOSS CLASSIFICATION

Flood loss information was recorded by type of loss and by location. Primary losses evaluated include (1) physical losses, such as damage to structures, equipment and machinery, raw and finished stock, cost of cleanup and repairs, and (2) non-physical losses, such as unrecoverable loss of business and wages, cost of emergency services and increased cost of operation.

Primary losses resulting from physical damage and a large part of the related non-physical loss were determined by direct inspection of property and evaluation of losses by property owners and field investigators. Where non-physical portions of primary losses could not be directly determined with available data, estimates were based upon the relationship between physical and non-physical losses for similar properties in the area.

3. RECURRING LOSSES

A recurrence of the record flood levels of August 1955 under 1965 conditions in the Park River Basin would cause losses estimated at \$6,750,000 in the reaches of the river between the present end of the Park River Conduit and Flatbush Avenue on the South Branch and Albany Avenue on the North Branch.

Over 58 percent of the losses would be concentrated in the portion of the basin between Broad Street on the downstream end of the main stem and Hamilton Street on the South Branch and Farmington Avenue on the North Branch. Here, three industrial concerns with payrolls of more than 3,000 employees, thirty-six small manufacturing ventures and thirty-nine commercial establishments employing an added 2,000 people lie in the flood plain. Total losses in this zone would amount to \$3,930,000 under current conditions.

Upstream of Farmington Avenue, a loss of \$1,900,000 could be expected along the 2.1 mile stretch of the North Branch to Albany Avenue. While the largest single type of loss would be residential, industrial and public losses would also occur in the reach.

On the South Branch, from Hamilton Street upstream to Flatbush Avenue, losses would amount to \$950,000. Approximately 30 percent of the loss would be industrial in character with much of the remaining loss being suffered by residential property.

4. ANNUAL LOSSES

a. Present Conditions. Estimated recurring losses for various stages of flooding under present conditions in the studied area were combined with stage frequency data to derive damage-frequency relationships as a measure of annual losses. The stage frequency data reflected conditions to be expected after construction of all authorized Soil Conservation Service projects on the North and South Branches of the Park River. Annual losses amount to \$1,037,500 in the studied area, broken down as follows:

Main Stem Park River, North Branch to Farmington Avenue and South Branch to Hamilton Street	\$ 883,600
North Branch, Farmington Avenue to Albany Avenue	18,600
South Branch, Hamilton Street to Flatbush Avenue	16,100
Conn. River Dike Area in Hartford	119,200

b. Future Conditions. As discussed in Appendix C, Economic Development, the flood plain of the Park River in the studied area will have more intensive land use in the future than at present. Adjustments in annual losses were made to reflect the future conditions which could be positively identified. In addition, for those areas where definite forecasts could not be made, an increase in losses expressed as a percentage of the present loss and based on current trends in the areas was made. Derivation of annual losses and benefits for a typical reach of the Park River is shown on Plates D-1 and D-2.

For the properties along the Park River between the present conduit entrance and Capitol Avenue use and occupancy since the flood of 1955 has been about 40 percent of actual capacity based on highest and best use. Demand for space both for light industrial use and for wholesale commercial needs in Hartford are such that with the flood threat removed these properties would once more be put to their best use. The future losses under such conditions would increase in proportion to the increase in usage. Annual losses under current conditions in the area amount to \$41,400. Higher usage would increase these losses by \$62,100 annually. The increase in use and occupancy could be expected to start with project completion and be complete by the end of the third year. Discounted at 3-1/8 percent, the equivalent annual loss amounts to \$60,200.

For the Underwood Urban Renewal area, a square foot annual loss for the Underwood and Merrow properties under current conditions was derived. The square foot loss value was arrived at by dividing the total annual loss for the two properties by the total land area of the two properties. A square foot loss value of \$0.776 was derived in this manner. As the depth of flooding in the area planned for future industrial construction would be the same as for the two

existing plants and as both plants are modern in their equipment the value is a reasonable one to be used for future losses provided intensity of land use remains the same. However, land use regulations under the Redevelopment Plan preclude any such intensity of use so the value was reduced 50 percent to comply with land use practices proposed under the Plan. There are 473,000 square feet of land set aside for industrial development in the Renewal area. It is estimated that the development will start in the area with the start of conduit construction and take place uniformly over the next ten years. The additional annual loss in the area will be $(\$0.77 \times 473,000 \times .5 \times .86801) - (\$13,800)* = \$169,700$.

The 8-acre tract of land upstream of the Urban Renewal Area and bounded by Laurel Street, Park Street, Interstate Route I-84 and the river will be put to use with protection. The property was formerly occupied by a large foundry. Land taking in connection with Interstate Route I-84 took two acres of the original property and precluded access to the back of the foundry except for a railroad spur. The property has been sold to an investor and the buildings are being demolished. Future annual losses in this area were arrived at using the square foot loss value derived for the Urban Renewal Area adjusted to reflect the restrictive effect of the existing highway system on access and circulation. Development is projected to take place within 5 years of project completion and losses were discounted for that period using a 3-1/8 interest rate. Future annual losses so derived amount to \$93,600.

No attempt was made to project future conditions on the North Branch and the South Branch of the Park River above Farmington Avenue and Hamilton Street respectively. Total annual losses on the main stem of the Park River and its branches to Hamilton Street and Farmington Avenue amount to \$1,207,000 over the life of the project.

5. TANGIBLE FLOOD DAMAGE PREVENTION BENEFITS

Tangible flood damage prevention benefits to the various studied plans of protection were derived as the difference between annual losses expected over the project life without protection and the annual losses remaining after provision of the recommended plan of protection. Annual benefits so derived amount to \$1,160,000.

The existing flood control improvements at Hartford provide a high degree of protection from Connecticut River flooding. The

D-4

*Annual loss for present residential and commercial property to be removed.

recommended project will provide equivalent protection from Park River flood runoff.

As an index of the effects of floods exceeding the capacity of the existing conduit and flooding downtown Hartford, data was obtained from the Hartford Clearing House on the dollar volume of daily transactions. At the present time the daily clearings are in excess of \$20,000,000 and they are growing at a monthly rate of 1 1/2 percent.

A flood of a magnitude which exceeded the conduit capacity would take from 5 to 7 days to recede in the North and South Meadow areas of Hartford. Over and above the damages caused by the flood in the flood plain proper, there would be a large decrease in the business activity of Hartford because of the lack of access from the east of Hartford and the extreme congestion caused by the loss of use of the area's principal north-south route through the Meadows. This decrease would be directly measured by the clearing house receipts. While it is estimated that some 90 percent of the decreased activity would represent simply a deferral, the other 10 percent would be lost forever. Therefore, such a flood would cause business losses in Hartford of \$10,000,000 to \$14,000,000 over and above the losses in the flood plain. On an annual basis this amounts to \$140,000 annually. Construction of the auxiliary conduit would prevent these losses.

Construction of the conduit will obviate the need for four existing bridges over the Park River and its North Branch at Broad Street, Flower Street, and Laurel Street. None of the bridges are modern; all would have to be replaced over the life of the project. The estimated replacement costs of the bridges is \$275,000. Annual maintenance costs for the bridges amount to \$1,140. The annual savings to the City of Hartford at these four locations amount to the amortized costs plus maintenance.

		4370	
275,000 x 0.03276	\$ 9,009	4 5/8	
Annual Maintenance	<u>1,090</u>	12,860	
		<u>1,090</u>	
	\$10,099	13,950	
Called	\$10,000	14,000	
		(x 1.125 P.L.)	
		68 P.L. 15,700	

60,200
170
2,200,000
43,000
3,300,000

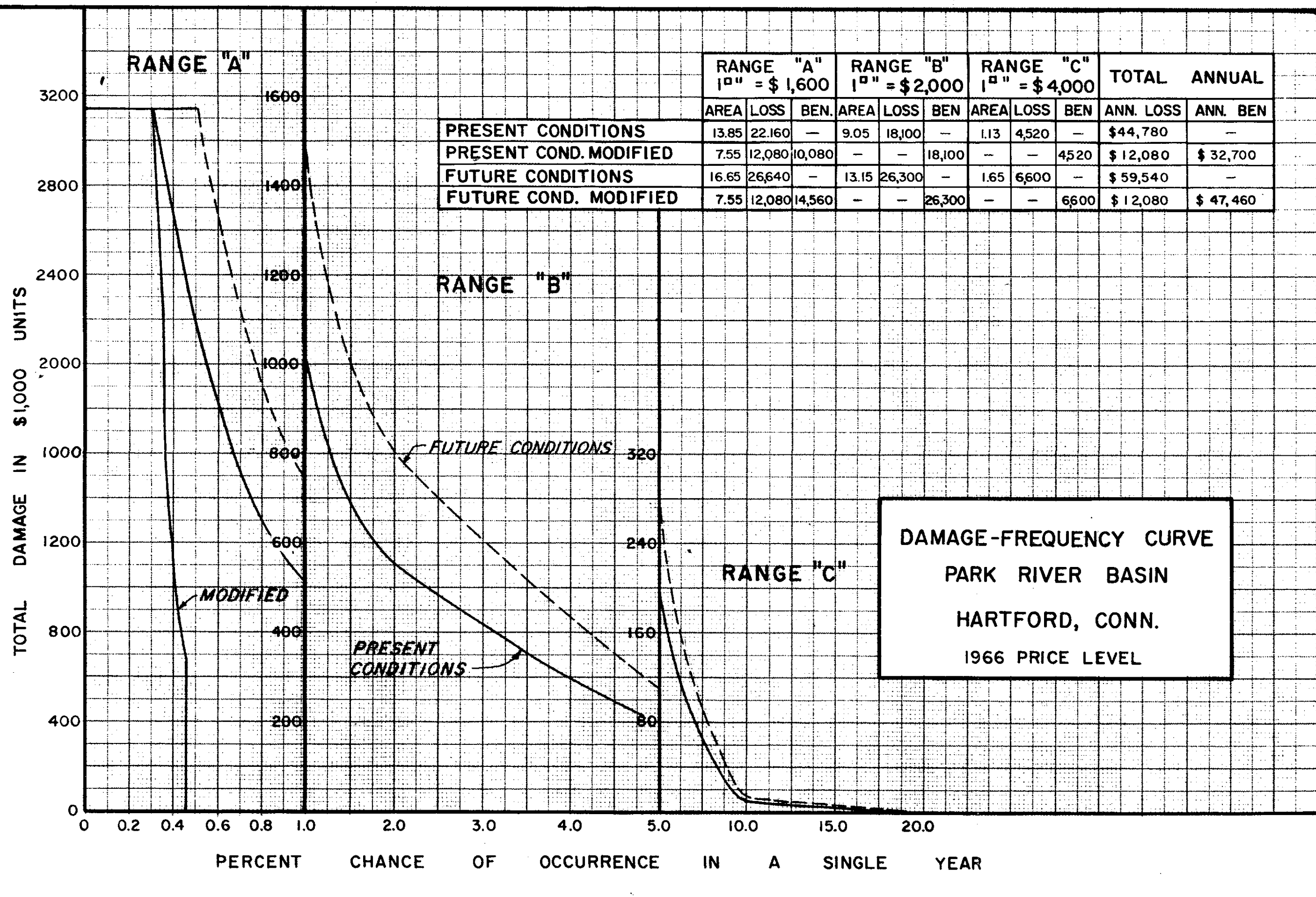
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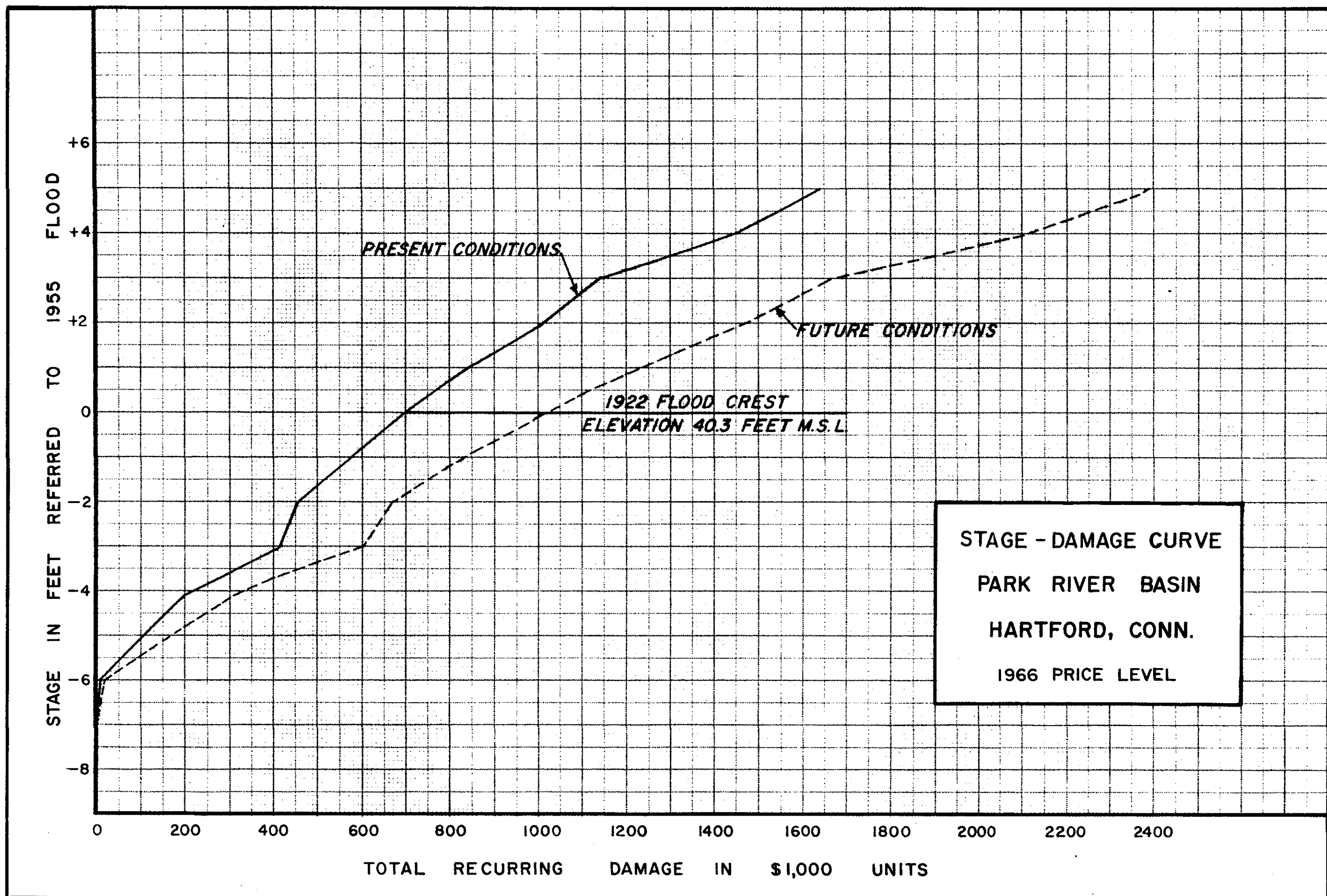
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In the reaches of the river between Broad Street and Capitol Avenue on the main stem and between Laurel Street and Interstate Route I-84 on the North Branch the area on top of the conduit can satisfy an urgent need for parking for employees of the industries and commercial ventures along the river. This use is incidental to normal conduit usage. The need for parking is so critical that one of the largest employers in the neighborhood has threatened to close his plant and move elsewhere unless some relief is afforded for the parking situation. Over 10 acres of space formerly used for parking in this area has been taken by the State for construction of Interstate Route I-84. The State Highway Department and the Hartford Traffic Commission have already entered into an agreement whereby space under the over-passes and interchanges on Route I-84 will be leased to the City on nominal terms and be adapted to parking by the city. This will do little to alleviate the parking problem because of the various configurations and limited amount of such space. Moreover, the locations, at interchanges and local street over-passes, will aggravate the traffic problem on the local ways because of access and egress from the parking areas into congested traffic.

An investigation was made into the rate of annual earnings for parking space for several New England cities, including Hartford, as a measure of the value of the parking space available on top of the conduit. Information was received from State and municipal authorities and private operators on rates of return from public metered lots, public lots leased to private operators and privately-owned and operated facilities. The annual rate varied from \$.30 a square foot for metered parking in a Boston suburb to \$2.00 per square foot for private lots in Boston. In Hartford, the rental rates for both public and private parking are the same and yield a net annual return of \$0.70 a square foot. While the projected increase in population and economic activity noted in Appendix C, Economic Development would indicate a higher rate of return in the future, the present value was adopted as being reasonably assured. There are 160,000 square feet of conduit surface on which parking will be available so the annual benefit to the provision of such parking amounts to \$112,000.

The total tangible annual benefits to the recommended project amount to \$1,420,000.





APPENDIX E

PROJECT DESCRIPTION AND COST ESTIMATES

APPENDIX E
PROJECT DESCRIPTION AND COST ESTIMATES
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APPENDIX E

PROJECT DESCRIPTION AND COST ESTIMATES

INTRODUCTION

1. PURPOSE

The design features and cost estimates of the recommended modification of the existing flood control project for Hartford, Connecticut, consisting of five sections of conduit, junction structure, a pumping station, an auxiliary conduit, and a headwall, are presented in this Appendix. The principal features are shown on Plates E-1 through E-5.

DESIGN CRITERIA

2. HYDRAULIC

a. Existing Park River conduit. The existing Park River conduit was designed to discharge 18,000 c.f.s. into the Connecticut River with the river stage at elevation 26.0 feet m.s.l. (mean sea level) and the conduit headwaters at elevation 44.0 feet, m.s.l. The conduit is two-barrelled in cross section with inside dimensions of each barrel 30 feet wide by 19 feet 6 inches high. Under design conditions which produce a maximum flow, the conduit will be totally submerged and no significant changes in velocity will occur except beyond the outlet where a rock apron prevents scour in the bed of the Connecticut River.

At moderate rates of flow and, under certain conditions, a hydraulic jump will occur within the conduit. The probability of conditions developing to produce a jump of troublesome magnitude is considered extremely remote. In the event that such conditions do develop, however, the jump could possibly undulate and cause vibrations in the structure if the water surface comes into contact with the roof. However, the structure was considered to be sufficiently massive and structurally sound so as not to be damaged by this infrequent occurrence.

b. Conduit extensions. The extensions to the existing Park River conduit which either have been completed or are presently under construction were designed by an engineering firm engaged by the Greater Hartford Flood Commission. Sections 1 and 3 on the Park River are sized to pass a flow of 18,000 c.f.s.; sections

6 and 8 are designed for flows of 22,000 c.f.s. and 10,000 c.f.s. respectively.

Proposed sections 2, 4, 5, and 7 are sized to flow full with the occurrence of a standard project flood.

c. Auxiliary conduit. The auxiliary conduit was designed to flow full throughout its length with the occurrence of a standard project flood.

3. STRUCTURAL

a. Existing Park River conduit. The existing Park River conduit, together with the inlet and outlet structures, was designed to withstand the most severe loadings and combinations of loadings. Provisions were made for tying into the conduit such appurtenances as the Bushnell Park pumping station and the Gully Brook conduit. The conduit was designed to withstand a pressure from a gradient of 48.0 feet, m.s.l. at the entrance in Bushnell Park with the Connecticut River at 26 feet, m.s.l.

b. Conduit extensions. The structural design criteria and computations, for those sections of the Park River conduit extension which were designed for construction in conjunction with segments of Interstate Route 84, were reviewed by the New England Division of the Corps of Engineers to insure conformity with the criteria contained in the pertinent Engineering Manuals, copies of which had previously been furnished the design engineers.

The two sections of conduit between the junction structure and the existing Park River conduit were designed to withstand internal pressures which would be produced by a pressure gradient 9 feet above its crown.

The South Branch conduit and the North Branch conduit, which are being built by the Connecticut Highway Department were designed to withstand internal pressures which would result from a pressure gradient of 10 feet above the crown.

Proposed sections 2, 4, 5, and 7 will be designed to be compatible with adjacent sections 1, 3, 6, and 8.

c. Auxiliary conduit. The rock tunnel section of the auxiliary conduit will have a minimum lining thickness of 2'-0". Quantities are based on a payment line 9" outside the line of minimum thickness. Provisions have been made for steel support and rock bolts in areas of inadequate rock. Tunneling in earth will require support steel and liner plate throughout. Sections constructed in open cut will be of reinforced concrete.

4. CONDUIT EXTENSION SECTIONS COMPLETED OR UNDER CONSTRUCTION

The Connecticut Highway Department has completed two sections of conduit extension on the Park River (designated as conduit extension sections 1 and 3 and shown on Plate E-1) totaling 2,923 feet in length. A section of conduit on the North Branch, 2,760 feet in length (conduit extension section 8), and a section of the South Branch (section 6), 1,460 feet in length, are now under construction. In addition, 1,451 feet of paved channel just upstream of conduit extension section 6 is also under construction. The sizes of conduit extension sections completed or under construction are shown on Plate E-2.

The sections of conduit extension completed or under construction and the South Branch approach channel were designed by an engineering firm engaged by the Greater Hartford Flood Commission and coordinated with I-84 highway plans. Construction contracts for the sections of conduit and the highway are being administered by the Connecticut Highway Department. These sections have been designed to be adequate for use as pressure conduits.

Based on an agreement between the Connecticut Highway Department and the Greater Hartford Flood Commission, the Commission will pay approximately \$12,740,000 for conduit construction with funds furnished by the city of Hartford.

SELECTED PLAN OF PROTECTION

5. DESCRIPTION OF PLAN

a. General. The selected plan of improvement consists of filling in the 'gaps' in the conduit extension by the construction of four sections of conduit (sections 2, 4, 5 and 7), a junction structure, an auxiliary conduit, a pumping station, drainage facilities, and a headwall at the entrance to the North Branch conduit extension.

Construction of the four sections of conduit will require the removal of three highway bridges and one foot bridge, and removal and relocation of existing sanitary sewers, water lines, and utilities.

b. Conduit sections 2 and 4. Conduit sections 2 and 4 will be two-barrelled reinforced concrete structures 1,232 feet and 1,337 feet in length, respectively. Each barrel will be 34 feet wide and 26.5 feet high. Design will be comparable to existing sections 1 and 3 with allowances for variations in foundation

conditions and anticipated loading.

Conduit section 2 will be founded on bedrock throughout its length. Construction will require removal of Broad Street and Flower Street bridges and factory buildings on the right bank of the river, relocation of sanitary sewerage facilities and utilities, and the construction of drainage pipes and facilities to dispose of high-level and low-level drainage which now discharges to the river.

Section 4 will be founded on earth throughout most of its length. Construction will include lateral drainage pipes and facilities to conduct low-level drainage to a pumping station to be constructed on the right bank of the Park River near Riverside Street. Lateral drainage pipes will be connected to existing pipes which parallel conduit section 3.

c. Conduit section 5. Conduit section 5 will be entirely on earth and will require bearing pile foundation. It will be a twin-barrelled reinforced concrete structure 103 feet in length. Each barrel will be 36 feet wide and 27.5 feet high. Design will be comparable with section 6.

d. Conduit section 7. Conduit section 7 will be entirely on earth and will require bearing pile foundation. It will be a twin-barrelled reinforced concrete structure, 1,044 feet in length. Each barrel will be 22 feet wide and 25 feet high. Design will be comparable with conduit section 8, now under construction, with allowances for differences in foundation conditions and anticipated loading.

Conduit section 7 includes drainage pipes and facilities to conduct low-level drainage to the proposed pumping station to be located on the right bank of the Park River. Construction will require the removal of the Laurel Street bridge.

e. Auxiliary conduit. The auxiliary conduit will be a 22-foot inside diameter, circular cross-section structure extending from the junction structure 9,100 feet to the Connecticut River.

From the junction structure to a point in Pope Park northeast of the intersection of Park Terrace and Park Street, a length of 300 feet, construction will be in open cut. Thence it will be by tunneling in earth and rock, a length of 6,200 feet, following Park Street and private property to a point on Wyllys Street near Lisbon Street. From this point, construction will be in open cut again in Wyllys Street and Charter Oaks Avenue to a point near Sheldon Street, a length of 1,700 feet. For 800 feet, under a

portion of Van Dyke Avenue, Highway I-91, and the Corps of Engineers Connecticut River floodwall, the conduit will be constructed by tunneling in earth. The remaining 100 feet to an outlet structure at the Connecticut River will be constructed in open cut.

f. Junction structure. The junction structure will be a reinforced concrete structure resting entirely on earth and will require bearing pile foundation. Flows from the North Branch and South Branch will be combined at the junction structure and discharged to the Park River conduit extension and to the auxiliary conduit.

g. Pumping station. A pumping station will be located on the right bank of the Park River downstream of the junction structure to pump low-level drainage to the conduit extension during flood periods. It will be equipped with 3 vertical volute pumps driven by diesel engines to discharge 250 c.f.s. against a 30-foot head.

h. North Branch headwall. The section of North Branch conduit extension now under construction by the Connecticut Highway Department (section b) will include a headwall and grading to high ground at 54.5 feet, m.s.l. At the entrance to the North Branch (conduit section 8), the contract calls for low steel sheet piling walls tying in to the Farmington Avenue Bridge, in anticipation of further extension of the conduit as a part of this project. It has been found that further extension cannot be justified. Therefore, a reinforced concrete headwall will be constructed at the entrance to the North Branch conduit extension with a top elevation of 54.5 feet, m.s.l., similar to the South Branch headwall. The design headpools at 52 feet, m.s.l. will be contained with a 2.5-foot freeboard.

6. SITE GEOLOGY AND FOUNDATION CONDITIONS

The overburden throughout the area consists of glacial lake deposits composed mainly of varved and stratified silt, clay and sand which are underlain by till. Locally the lake deposits thin out or are missing and the till, consisting of variable, silty, gravelly sand and sandy, silty gravel with numerous cobbles and boulders, occurs at the ground surface. In some areas the river flows on a cobble and boulder pavement and elsewhere on recent alluvium composed of sands, gravels, muck and, locally, peat. Artificial fills consisting of silt, sand, gravel, boulders, cinders, and trash occur in several areas. Bedrock outcrops locally along the conduit extension, particularly in section 2, but is buried to

various depths in the ridge through which the tunnel for the auxiliary conduit is proposed. The bedrock consists of conglomerate, sandstone, shale, and "trap" rock. A more detailed discussion of the geology of the area is presented in Appendix F.

7. AVAILABILITY OF CONSTRUCTION MATERIALS

Random fill, pervious fill, and gravel are available from commercial sources within five miles of the site. Trap rock quarries in Newington and sand deposits in Glastonbury are sources of concrete aggregate for conduit sections now under construction and will be acceptable for future construction.

8. LANDS AND DAMAGES

The sections of conduit extension being proposed in the report which are required to complete the conduit extension will, to a large extent, fall within the banks of the Park River and the North Branch of the Park River. No value has been placed on river areas. The auxiliary conduit will be constructed principally within street rights-of-way. Where the conduit passes under private property, permanent easements will be secured. Local interests will be required to provide spoil areas. No cost is included for such areas because, in areas directly inside the existing dikes and in a number of other areas, development requires fill. It is anticipated that, at the time of construction, fill will be in demand and surplus material from project construction may be sold.

A detailed breakdown of lands and damages is given in Table E-1.

9. RELOCATIONS

Construction of conduit to "fill in the gaps" will require removal of three highway bridges. Upon completion of the conduit, the highway pavement, sidewalks, drains, and other appurtenances will be replaced by local interests at their expense. At a number of locations, the drains, sewers, and utilities will require relocation outside the area required for construction of the conduits.

10. PLAN OF CONSTRUCTION

It is anticipated that the recommended plan will require about three years to complete. The physical limitation of the site and the urban nature of the general area are important factors bearing on the progress that may be expected.

The handling of river flows and the maintenance of traffic and

services at all times will govern the scheduling of the major items of construction and the methods of construction.

The proposed sections of conduit extension will be constructed one barrel at a time to allow for river diversion. Only one of the four highway bridges to be removed should be out of service at a time. The lower open cut section of the auxiliary conduit will be constructed in such a manner as to minimize the interference with highway traffic crossing the construction site and access to adjacent properties.

BASIS FOR FIRST AND ANNUAL COSTS

11. BASIS OF COST ESTIMATES

Topographic maps of the U. S. Geological Survey to a scale of 1:31,600 and 1:24,000, with 10-foot contours; and photogrammetric maps of the Commission on Regional Planning, the Metropolitan District, Hartford County, Connecticut, to a scale of 1" = 200' with 2-foot contours were supplemented by available field survey information previously obtained by other interests. Foundation conditions for the conduit extension were determined by field reconnaissance and by an examination of the logs of borings which have been made in the vicinity of the proposed structures by the state Highway Department and the Greater Hartford Flood Commission in connection with highway and conduit construction in the area. Principal construction items were estimated on the basis of a preliminary design, the plans, sections, and details of which are shown on Plates E-1 through E-5.

12. UNIT PRICES

Unit prices at a 1966 price level, are based on averages for the construction of comparable conduit projects in the Greater Hartford area.

13. CONTINGENCIES, ENGINEERING AND OVERHEAD

The construction and relocation cost estimates have been increased 20 percent to cover contingencies. Costs of engineering and design, supervision and administration, are estimated lump sums based on experience, evaluation of the site and project, and comparison with similar projects in the area.

FIRST COSTS AND ANNUAL COSTS

14. FIRST COSTS

The total estimated cost of the project is \$31,100,000. Local interests will provide all lands, easements, and rights-of-way and accomplish relocations made necessary by the construction. Detailed estimates by principal project feature are given in Table E-1.

15. ANNUAL COSTS

The estimated annual cost of the proposed improvement is \$1,130,000. The determination of annual costs is shown in Table E-2.

TABLE E-1

ESTIMATED FIRST COST
PARK RIVER FLOOD CONTROL
Hartford, Conn.

SUMMARY

Non-Federal
Lands & Damages
Relocations

\$ 630,000
170,000
800,000

Federal
Conduit Extension
Auxiliary Conduit
Pumping Station
Engineering & Design
Supervision & Administration
Total Federal First Costs

\$ 9,400,000
16,360,000
480,000
2,090,000
1,970,000
30,300,000

TOTAL FIRST COST

31,100,000

TABLE E-1 (cont'd)

LANDS AND DAMAGES

<u>Item</u>	<u>Estimated Quantity</u>	<u>Unit</u>	<u>Unit Price</u>	<u>Amount</u>
Land - Fee				
Commerical	2,000	s.f.	3.00	\$ 6,000
Industrial	28,000	s.f.	1.00	28,000
Parkland	40,000	s.f.	.50	20,000
Residential	36,000	s.f.	.50	18,000
Land - Permanent Easement				
Industrial	26,000	s.f.	1.00	26,000
Park Land	40,000	s.f.	.50	20,000
Residential	36,000	s.f.	.50	18,000
Residential	80,000	s.f.	.25	20,000
Land - Temporary Easement				
Residential	80,000	s.f.	.15	12,000
Improvements				
Commercial	1	job	L.S.	40,000
Industrial	1	job	L.S.	90,000
Residential	2	job	L.S.	30,000
Severence damage				160,000
Administrative cost				5,000
				<u>493,000</u>
Contingencies				57,000
				<u>550,000</u>
Acquisition costs				80,000
				<u>80,000</u>
TOTAL COST - LANDS AND DAMAGES				\$630,000

TABLE E-1 (cont'd)

RELOCATIONS

<u>Item</u>	<u>Estimated Quantity</u>	<u>Unit</u>	<u>Unit Price</u>	<u>Amount</u>
Replacement of				
a. Broad Street	1	job	L.S.	\$ 25,000
b. Flowers Street	1	job	L.S.	25,000
c. Laurel Street	1	job	L.S.	20,000
Relocation of sewers, drains and utilities	1	job	L.S.	50,000
				<u>120,000</u>
Contingencies				25,000
				<u>145,000</u>
Engineering & Design				13,000
Supervision & Administration				<u>12,000</u>
TOTAL - RELOCATIONS				\$170,000

CONDUIT EXTENSION

(Sect. 2, 4, 5, 7 Junction Structure and No. Branch H'wall)

<u>Description</u>	<u>Estimated Quantity</u>	<u>Unit</u>	<u>Unit Price</u>	<u>Estimated Amount</u>
Preparation of site	1	job	L.S.	\$ 10,000
Clearing and Grubbing	1	job	L.S.	3,000
Control of River	1	job	L.S.	300,000
Underpinning & protec. of existing structures	1	job	L.S.	75,000
Maintenance & control of traffic	1	job	L.S.	35,000
Removal of buildings	1	job	L.S.	20,000
Removal of bridges	1	job	L.S.	17,000
Excavation				
Earth, structure	148,000	c.y.	\$2.00	296,000
Rock, structure	43,000	c.y.	5.00	215,000
Rock, trench	1,800	c.y.	10.00	18,000
Borrow				
Random	27,000	c.y.	1.00	27,000
Pervious	120,000	c.y.	1.75	210,000
Gravel	12,000	c.y.	2.00	24,000
Broken Stone	8,000	c.y.	3.00	24,000

TABLE E-1 (cont'd)

CONDUIT EXTENSION (cont'd)

<u>Description</u>	<u>Estimated Quantity</u>	<u>Unit</u>	<u>Unit Price</u>	<u>Estimated Amount</u>
Placing				
Random fill	60,000	c.y.	.50	30,000
Broken Stone	8,000	c.y.	1.00	8,000
Gravel	10,000	c.y.	.50	5,000
Pervious backfill	98,000	c.y.	1.00	98,000
Conduit				
Reinforced concrete	63,000	c.y.	80.00	5,040,000
Access manholes	6	ea.	1,500.00	9,000
Furnishing & driving piles	56,000	l.f.	11.50	644,000
Side drains	8,000	l.f.	6.00	48,000
Drain chambers	14	ea.	4,500.00	63,000
Reinforced concrete pipe				
12"	1,000	l.f.	4.00	4,000
15"	1,200	l.f.	5.00	6,000
18"	450	l.f.	6.00	2,700
21"	400	l.f.	7.50	3,000
24"	500	l.f.	8.00	4,000
27"	40	l.f.	10.00	400
30"	400	l.f.	15.00	6,000
36"	1,400	l.f.	18.00	25,200
42"	400	l.f.	20.00	8,000
48"	450	l.f.	24.00	10,800
72"	1,300	l.f.	65.00	84,500
84"	1,000	l.f.	70.00	70,000
Reinforced concrete pipe (Lock Joint)				
36"	500	l.f.	20.00	10,000
42"	150	l.f.	22.00	3,300
48"	800	l.f.	24.00	19,200
Manholes, pressure	16	ea.	1,800	28,800
Manholes, concrete	12	ea.	1,000	12,000
Manholes, brick	14	ea.	400	5,600
Catch basins	22	ea.	400	8,800
Storm, siphon - Willow St.	1	job	L.S.	50,000
Storm, siphon - Pump Sta.	1	job	L.S.	75,000

TABLE E-1 (cont'd)

CONDUIT EXTENSION (cont'd)

<u>Description</u>	<u>Estimated Quantity</u>	<u>Unit</u>	<u>Unit Price</u>	<u>Estimated Amount</u>
Storm, siphon -				
W. of Flower St.	1	job	L.S.	\$ 6,000
Sanitary siphon,				
So. Woodbine St.	1	job	L.S.	10,000
Sanitary siphon, Armory	1	job	L.S.	30,000
Reinforced concrete				
North Branch Headwall	1,000	c.y.	80.00	80,000
Seeded topsoil	25,000	s.y.	1.00	25,000
Removal and replacement of utilities	1	job	L.S.	25,000
				<u>7,832,300</u>
Contingencies				<u>1,567,700</u>
				<u>9,400,000</u>
Engineering & Design				750,000
Supervision & Administration				<u>700,000</u>
				<u>\$10,850,000</u>

AUXILIARY CONDUIT

Preparation of site	1	job	L.S.	\$ 10,000
Maint. & control of traffic	1	job	L.S.	50,000
Control of water	1	job	L.S.	100,000
Underpinning & prot. of bldgs.	1	job	L.S.	50,000
Removal of bldgs.	1	job	L.S.	5,000
Earth excavation, common	5,000	c.y.	1.00	5,000
Earth excavation, structure	63,000	c.y.	2.00	126,000
Earth excavation, tunnel	28,000	c.y.	20.00	560,000
Rock excavation, struc.	26,000	c.y.	5.00	130,000
Rock, tunnel	145,000	c.y.	23.00	3,335,000
Borrow				
a. Pervious	28,000	c.y.	1.75	49,000
b. Gravel	1,000	c.y.	2.00	2,000
Placing				
a. Random backfill	24,000	c.y.	.50	12,000
b. Pervious backfill	26,000	c.y.	1.00	26,000
c. Gravel	2,000	c.y.	.50	1,000

TABLE E-1 (cont'd)

AUXILIARY CONDUIT (cont'd)

<u>Description</u>	<u>Estimated Quantity</u>	<u>Unit</u>	<u>Unit Price</u>	<u>Estimated Amount</u>
Furnishing and driving steel sheet piling	100,000	s.f.	3.50	350,000
Tunnel support steel				
a. Tunnel in rock	4,500,000	lbs.	.35	1,575,000
b. Tunnel in earth	1,500,000	lbs.	.35	525,000
Rock bolts	25,000	l.f.	5.00	125,000
Steel lagging	40,000	l.f.	2.50	100,000
Liner plate - tunnel in earth	1,100,000	lbs.	.35	385,000
Concrete mass	3,000	c.y.	50.00	150,000
Concrete, reinforced				
a. Tunnel in earth	9,600	c.y.	70.00	672,000
b. Conduit in open cut	20,000	c.y.	70.00	1,400,000
Concrete, tunnel lining	60,000	c.y.	50.00	3,000,000
Grout, tunnel in rock	1	job	L.S.	125,000
Removal and replacement Water lines, Sewer lines, Drainage facilities & Utilities	1	job	L.S.	600,000
Access, manhole	2	ea.	1,500	3,000
Replacement of highway Pavement and sidewalks	1	job	L.S.	40,000
Seeded topsoil	5,000	s.y.	1.00	5,000
Cofferdam	1	job	L.S.	50,000
Contingencies				13,566,000
				<u>2,794,000</u>
				16,360,000
Engineering & Design				1,300,000
Supervision & Administration				<u>1,240,000</u>
TOTAL				\$18,900,000

TABLE E-1 (cont'd)

PUMPING STATION

<u>Item</u>	<u>Quantity</u>	<u>Unit Price</u>	<u>Unit</u>	<u>Amount</u>
Structure	1	job	L.S.	\$240,000
Mechanical and Electrical Equipment	1	job	L.S.	160,000
				<u>400,000</u>
Contingencies				80,000
				<u>480,000</u>
Engineering & Design				40,000
Supervision & Administration				<u>30,000</u>
TOTAL - PUMPING STATION				\$550,000

TABLE E-2

ESTIMATED ANNUAL COSTS
PARK RIVER FLOOD CONTROL
Hartford, Conn.

Federal Investment

First Cost	\$30,300,000
Interest during construction	<u>1,400,000</u>
Total Federal Investment	31,700,000

Federal Annual Costs

Interest on Investment	989,000
Amortization	<u>48,000</u>
Federal Annual Costs	1,037,000

Non-Federal Investment

First Cost	800,000
Interest during construction	<u>38,000</u>
Total Non-Federal Investment	838,000

Non-Federal Annual Costs

Interest on Investment	27,000
Amortization	1,000
Major replacements	15,000
Maintenance and operation	<u>50,000</u>
Non-Federal Annual Costs	93,000

TOTAL ANNUAL COST

\$ 1,130,000

\$ 12,740,000 Conduit Extensions
Annual Cost (No Int During Const)
100 I & A 417,000
Major Repl. 3,000
O & M 25,000
447 447,000
1130
1577

E-16

$$\frac{1,420,000}{1,577,000} = .90 \text{ to } 1.0$$

OTHER PLANS CONSIDERED

16. GENERAL

Consideration was given to upstream reservoir storage and diversion in lieu of auxiliary conduit capacity. Further extension of the North Branch conduit as requested by local interests was also considered.

The presence of recent housing, highway, and commercial developments in the basin, as well as established communities along the main streams, makes the construction of large impoundments economically infeasible. Impoundments throughout the basin in the future will be less favorable due to continued growth and development. The eight reservoirs in the Soil Conservation Service plans were derived as the maximum reservoir development on the basis of studies inclusive of review of previous studies by others.

The Greater Hartford Flood Commission, after the 1955 record flood, engaged engineering firms to study the problem and propose solutions. Many alternative reservoirs and reservoir systems in the headwaters and channel improvements throughout the basin were considered as supplemental to plans of downstream conduit and auxiliary conduit extension. The Commission also considered the diversion of North and South Branch flows.

The Soil Conservation Service engaged an engineering firm to develop plans for the North and South Branches. The existing channel program of that agency will be beneficial to low areas along the main stream. The more rapid concentration of flow combined with future development will increase flows at Hartford in a major flood.

Although, in general, few possibilities for additional storage exist in the basin, studies for this report considered all additional potential improvements for flood control in both branches of the Park River.

17. STORAGE RESERVOIRS

Three Soil Conservation Service detention reservoirs in the North Branch watershed have been completed and one, under contract, is scheduled for completion in 1966. The four reservoirs have a combined storage capacity of 4,400 acre-feet and will cost a total of about \$1,070,000. Over 80 percent of the cost is for land acquisition. In selecting these four reservoirs, ten other sites were studied and eliminated. The most favorable of the sites

studied and eliminated was a dam and reservoir on Tumbledown Brook. The reservoir would store 1,700 acre-feet from a 3.8 square mile drainage area and would cost an estimated \$3,000,000. The site was eliminated principally because of strong local opposition to land acquisition involved. It is anticipated that the local objection to development of this site would be encountered in the future also. Development of other, smaller sites would be less favorable. Larger sites on the South Branch would involve thickly settled areas.

Two Soil Conservation Service detention reservoirs in the South Branch watershed have been completed; a third, under contract, is scheduled for completion in 1966; a fourth, soon to be placed under contract, is scheduled for completion in 1967. The combined capacity of the reservoirs will be 2,470 acre-feet and the cost will total just under \$2,000,000 with about 74 percent of the cost for land acquisition. The maintenance of Deadwood Swamp in its present state has cost \$64,000 for flowage rights.

A total of thirteen sites in the South Branch watershed were studied by the Soil Conservation Service. Eight of the thirteen sites were found to be not economically justified because of recent development of high value properties and the alignment of existing and proposed interstate highways and access roads in reservoir or structure areas. One site, Deadwood Swamp, was not developed due to its effectiveness under natural conditions.

A field and office review of previously considered sites was made. One reservoir plan, considered in early studies by the Greater Hartford Flood Commission and later studied and eliminated by the Soil Conservation Service, appeared to be the most favorable of the plans not developed. It would consist of two reservoirs in the Piper Brook watershed and overflow to Wood Pond in the Trout Brook watershed. At the time of the original study, the plan would have provided 3,300 acre-feet of storage from a drainage area of 9.7 square miles. However, an interstate highway, now under design, will pass through the storage area reducing the storage to about 2,300 acre-feet. The plan would cost an estimated \$10,000,000.

The most favorable North and South Branch reservoirs, with a combined storage capacity of 4,000 acre-feet, would not eliminate the need for an auxiliary conduit. In a standard project flood, without an auxiliary conduit, the headpools at the North and South Branch conduit extension entrances would rise to elevation 55 feet m.s.l., or three feet above the design elevation of 52.0 feet, m.s.l. It is estimated that provision of the total storage required would

exceed the cost of the auxiliary conduit. Therefore, no further consideration was given to reservoir storage.

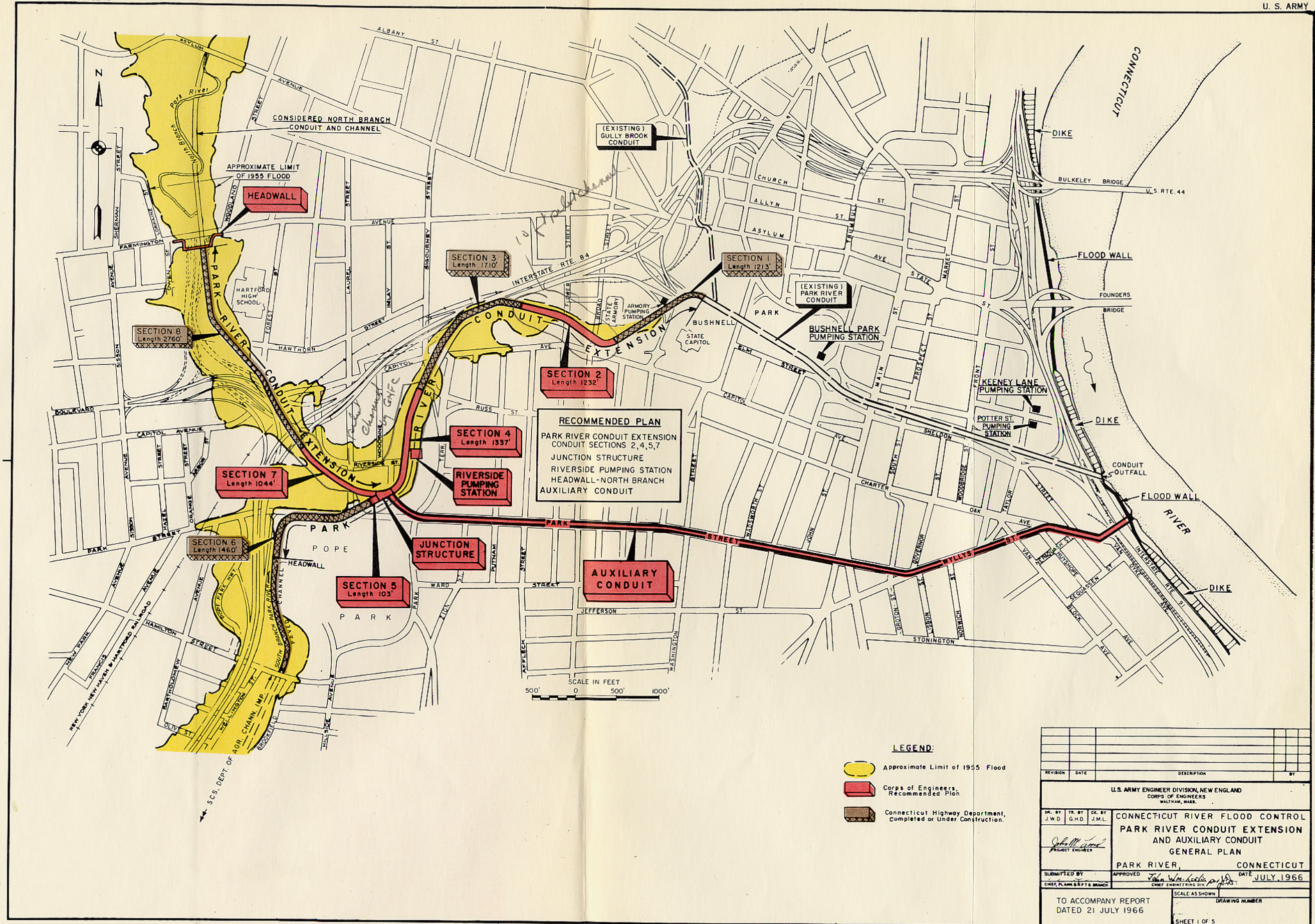
18. DIVERSION

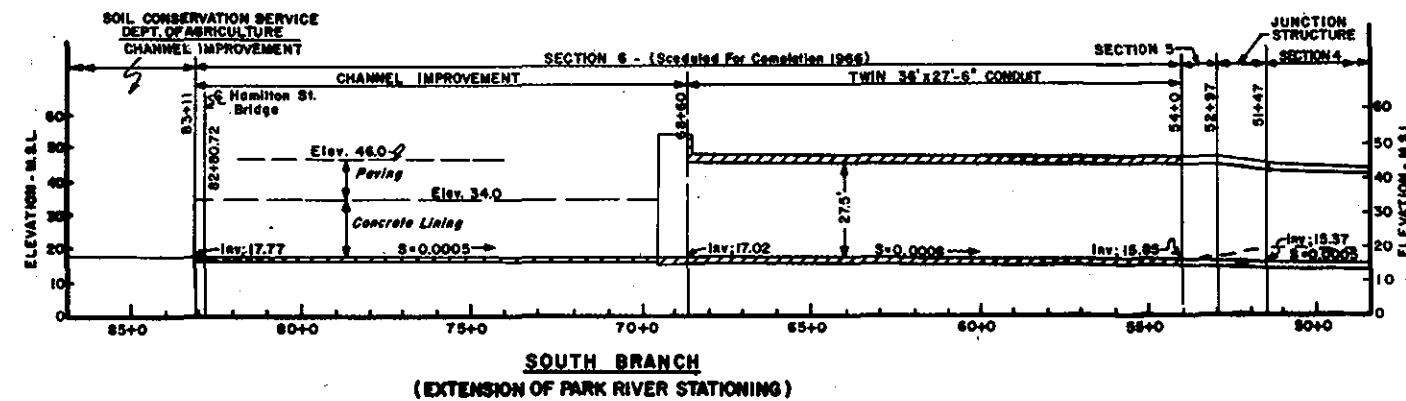
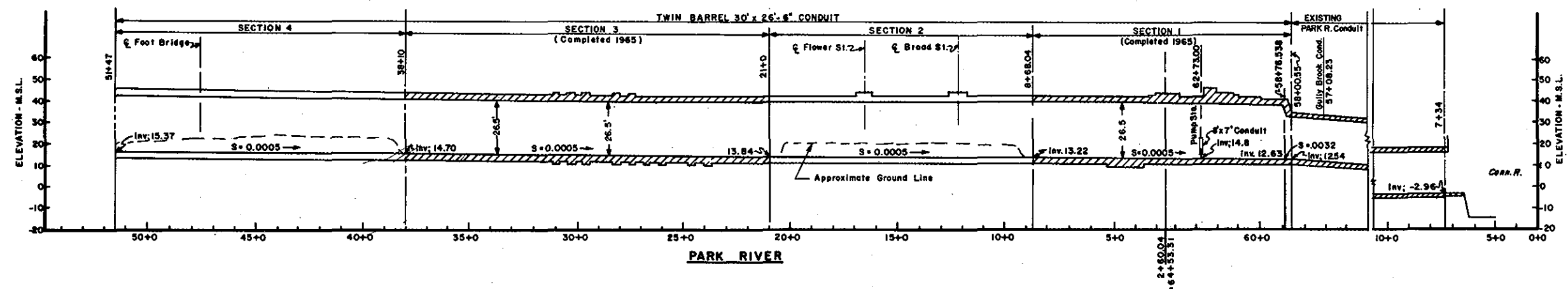
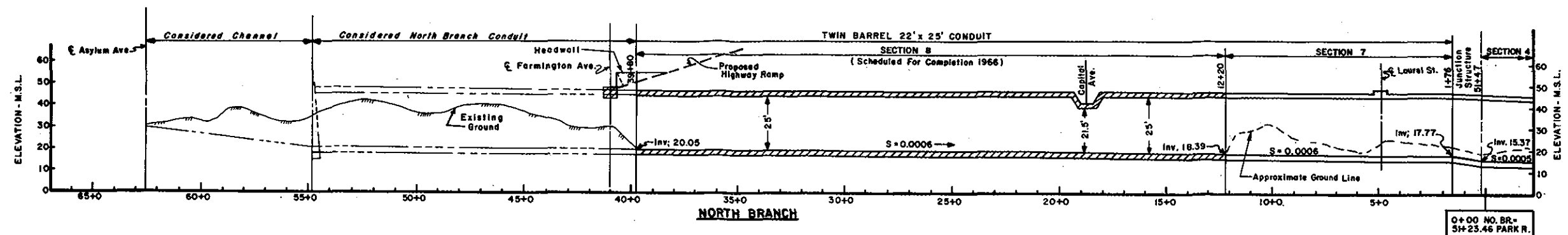
Diversion of North Branch flood flows to the Connecticut River either through Windsor or Hartford would require construction through an urban area. The total length of the diversion and the cost would be greater than for an auxiliary conduit downstream.

The Greater Hartford Flood Commission in an early study considered diversion of Piper Brook flood runoff to the Mattabesset River by way of Webster Brook. A field and office review of the plan indicated a cost of over \$10,000,000. About 22,000 feet of channel improvement, rebuilding of four bridges on Webster Brook, and three on the Mattabesset River, and construction of a diversion structure and dikes and walls at several locations would be the major items of cost. During a major storm, the Mattabesset River would be at flood stage and diversion of Park River runoff would be a liability. The plan would be less effective than increasing downstream conduit capacity by construction of an auxiliary conduit in the Park River basin. Consideration was also given to diversion of South Branch flood runoff to Wethersfield Cove from the confluence of Mill and Piper Brook. The three miles of conduit and diversion structure required would be more costly than the downstream auxiliary conduit. Diversion of flood flows therefore was found not to merit further study.

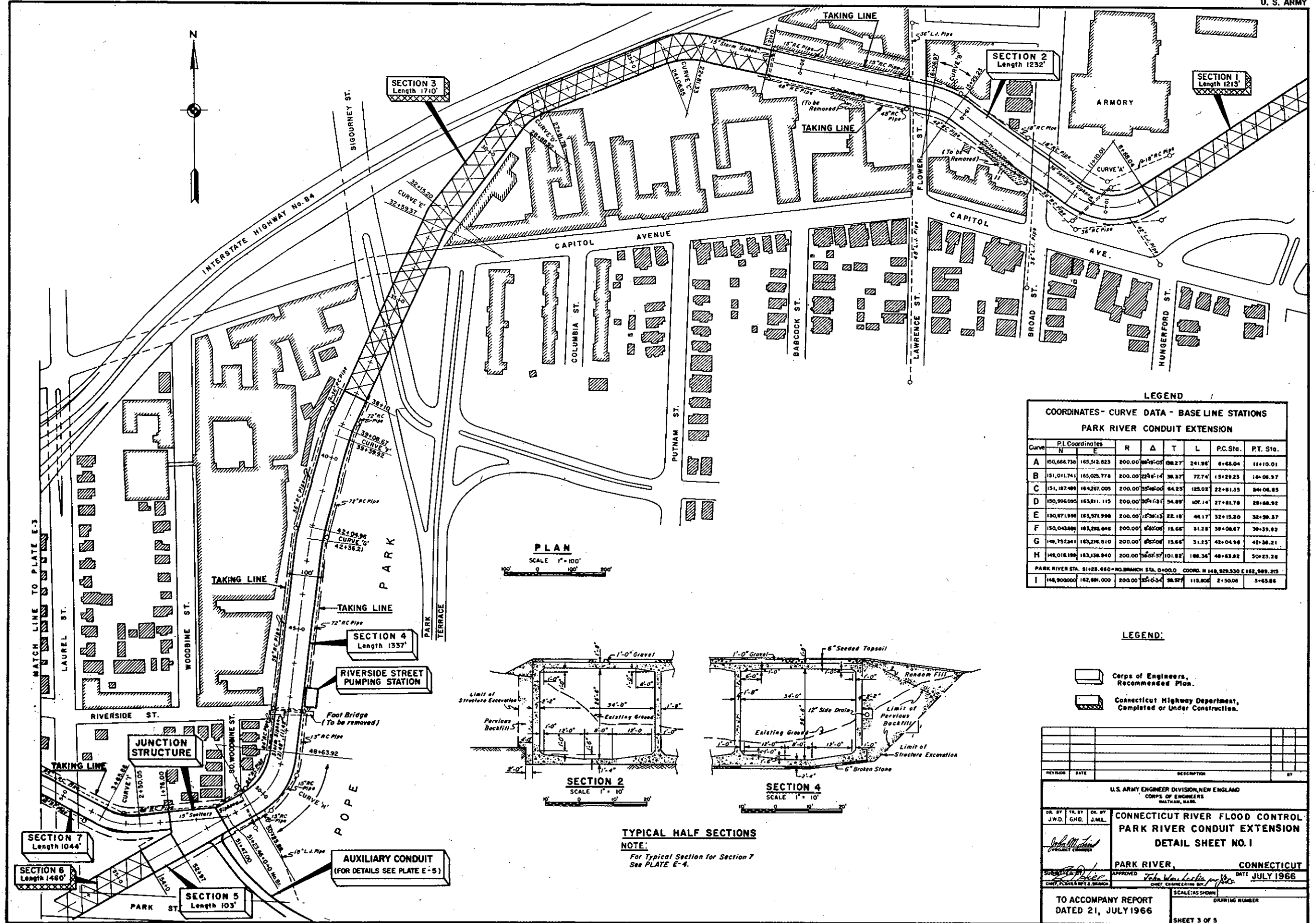
19. NORTH BRANCH CONDUIT EXTENSION

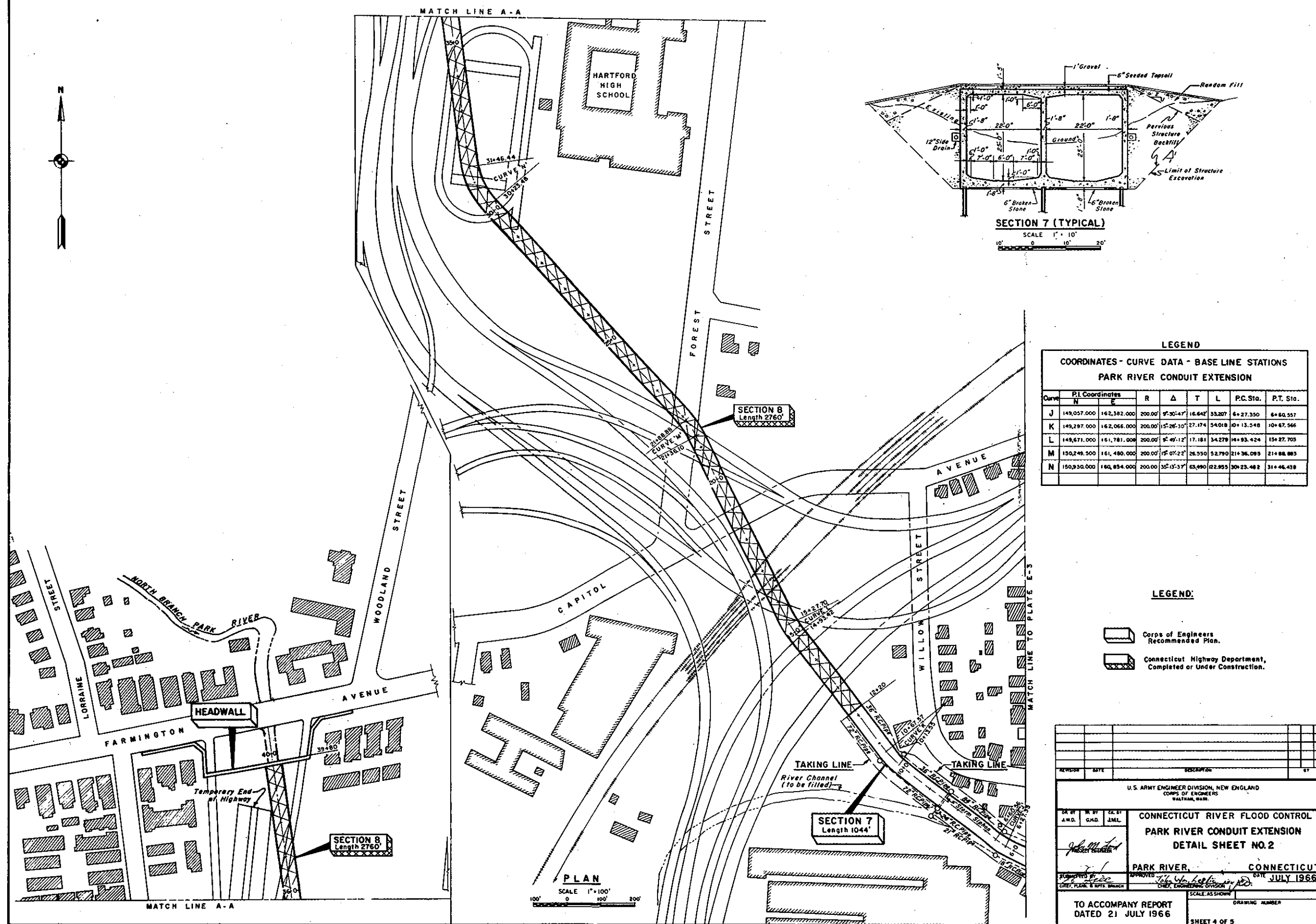
Consideration was given to further extension of the North Branch conduit 1,000 feet upstream as requested by local interests. It would involve costly relocations and conduit construction at a total estimated cost of about \$5,000,000, which would not be justified by the benefits to be realized.





DIVISION		DATE		DESCRIPTION		BY	
U.S. ARMY ENGINEER DIVISION, NEW ENGLAND CORPS OF ENGINEERS WATERWAYS DIVISION							
CONNECTICUT RIVER FLOOD CONTROL PARK RIVER CONDUIT EXTENSION PROFILES							
PARK RIVER, CONNECTICUT				DATE: JULY 1966			
TO ACCOMPANY REPORT DATED 21. JULY 1966				SHEET 2 OF 5			







APPENDIX F

GEOLOGY

APPENDIX F

GEOLOGY

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	LOG OF BORINGS (Following Text)	

PLATES

<u>Number</u>	
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F-2	Profiles
F-3	Record of Explorations
F-4	Surficial Geology

APPENDIX F

GEOLOGY

1. GENERAL GEOLOGY

The Park River is located in the Connecticut Valley, a broad lowland underlain by Triassic bedrock consisting of conglomerate, sandstone and shale with included sheets of basalt, a volcanic rock commonly called "trap." Although relief in the lowland is generally low and subdued, faulting and differential weathering have left prominent ridges of the resistant "trap" rock projecting above the softer sediments. The region is blanketed by glacial till which occurs at the surface in the higher parts of the lowland. In the low, flat, or gently undulating plains which form the surface throughout most of the region, however, the till is overlain by wide-spread, glacial lake deposits of stratified sand and varved silt and clay. The lake beds also are buried locally but occasionally in extensive areas under glacial outwash, terraces, and delta deposits of sand, silt, and gravel. Thick deposits of recent alluvium consisting of fine sand and silt have accumulated on the broad flood plains of the Connecticut River, and locally, thinner alluvial deposits occur along the flood plains of most of the tributary streams. The banks of the Park River, locally, and the Connecticut River, generally, are blanketed by thick and occasionally extensive artificial fills.

2. SUBSURFACE INVESTIGATIONS

a. Conduit Extension. The Greater Hartford Flood Commission has had numerous foundation borings made in the vicinity of Park River and both North and South Branches, Park River, in connection with studies for conduit extensions and the design of the conduit sections being built in conjunction with construction of Interstate Route 84. Logs of these borings pertinent to the recommended project are included in this appendix. The locations of these explorations are shown on "Plan of Explorations" Plate F-1 and "Profiles" Plate F-2.

b. Auxiliary conduit (Tunnel). Subsurface investigations have not been made for the auxiliary conduit. All available data from previous borings and wells in the area have been reviewed. Borings for the existing Jefferson Street tunnel, approximately 700 to 1,200 feet south of the proposed tunnel alignment, were made for the Hartford Bureau of Public Works in 1934. Borings in the vicinity of outlet

area along the Connecticut River were made in connection with flood control dikes and walls constructed by the Providence District, Corps of Engineers, in 1940. Locations and data from wells in the area were obtained from a report, Records of Logs of Selected Wells and Test Borings and Chemical Analyses of Water in North Central Connecticut, prepared by the U. S. Geological Survey, in cooperation with the Connecticut Water Resources Commission. The locations of these borings and wells are shown on Plate F-1. Descriptions and classification of materials encountered in the borings are presented on "Record of Explorations," Plate F-3. Surficial geology of the area is shown on "Surficial Geology" Plate F-4.

3. FOUNDATION CONDITIONS

a. Conduit extension. Overburden in the several sections of the conduit extensions consists mainly of glacial lake bottom deposits which rest on till or bedrock. Locally, as at Sections 2 and 4 of the conduit, the lake deposits are thin or missing and till occurs at the ground surface. Throughout most of the area, however, the lake deposits consisting of stratified and varved clay, silt and fine sand, are very thick and extend to depths far below conduit grades. In Sections 2 and 4 the till which constitutes the main overburden, is variable ranging from silty, gravelly sand to sandy, silty gravel with cobbles and boulders scattered throughout. In many reaches the existing stream flows on a cobble and boulder pavement; in other reaches generally thin deposits of muck and peat occur. Overlying the natural materials in scattered but numerous areas are artificial fills composed of sand, silt, gravel, boulders, cinders and trash.

Bedrock is generally deeply buried in the area of the conduit extensions except in some reaches of Sections 2 and 4 where it occurs close to or above conduit grade. As shown on "Surficial Geology," Plate F-4, bedrock outcrops in several areas in Section 2. The bedrock consists of thin-bedded sandstones and shales which trend generally north-south and dip eastward at 15° to 20° . In the vicinity of the fault which crosses the Park River at Section 2 both the trend and dip of the strata vary widely within short distances.

b. Auxiliary conduit (Tunnel). The alignment of the proposed auxiliary conduit and an assumed bedrock profile are shown on "Auxiliary Conduit, Plan, Profile and Sections", Plate E-5. As shown on the profile, open cut excavation and tunnelling in overburden will be required at the intake end of the auxiliary conduit from the Junction Structure to the assumed steep rock face located where the fault shown on Surficial Geology, Plate F-4 crosses the conduit alignment.

The overburden at, and near the Junction Structure consists of lake deposits, mainly sands, silt and clay, underlain by till composed of silty to clayey, gravelly sand with numerous cobbles and boulders. The lake deposits become thin against the rising till surface approaching the steep bedrock face near Park Terrace, and overburden tunnelling in this area will be entirely in till. A deep till-filled valley occurs in the rock surface in the vicinity of Hungerford Street so that the rock surface in this area is expected to be close to or below the roof of the tunnel. Where the tunnel leaves the rock near Lisbon Street, the overburden is composed of lake deposits underlain by till. Further eastward in the vicinity of Van Block Street where the excavation will be in open cut, the overburden at the surface is flood plain alluvium consisting of stratified sand and silt. Underlying the alluvium are the lake bottom varved silt and clay deposits which rest on till or, where till is missing, on the bedrock. Adjacent to the Connecticut River the conduit will go under the existing flood wall and dike in a tunnel which will be excavated in alluvial and lake bottom sands and silts and artificial fills.

The bedrock along the tunnel alignment is a series of interbedded sandstones, shales and basalt. The sandstones and shales are generally thin-bedded, soft to moderately hard and variable in color. The basalt which was emplaced as a series of volcanic flows or sills, is dark gray to black, hard, fine grained and close-jointed. Bedding of the series trends approximately normal to the tunnel alignment and dips eastward at 15° to 20° . The steep rock face near the upstream end of the tunnel is probably a fault scarp and, as indicated by borings for the Jefferson Street Tunnel, other smaller faults probably cross the alignment. The tunnelling history for the Jefferson Street Tunnel is not known but the bore diameter was 8 feet, about one-third the diameter proposed for this tunnel. For estimating purposes it is assumed that close support designed for very blocky and seamy rock will be required.

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.		CLIENT: <u>Greater Hartford Flood Comm.</u>		SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>8</u>						
CONTRACTOR		PROJECT NO		LINE						
FOREMAN -DRILLER <u>Higgins</u>		PROJECT NAME <u>Park River Conduit</u>		STATION						
INSPECTOR <u>Batterson</u>		LOCATION <u>Capitol Ave., Hartford, Conn.</u>		OFFSET						
GROUND WATER OBSERVATIONS AT <u>9'</u> FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS		CASING TYPE SIZE I.D. <u>2"</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>		SAMPLER <u>S.S.</u> <u>1 3/8</u> <u>140</u> <u>30</u>						
		CORE BAR. BIT.		Date Start <u>10/17</u> Date Fin. <u>10/18</u> SURFACE ELEV. <u>37.5</u> GROUND WATER ELEV. _____						
DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE) 0-6 6-12 12-18	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.					
4										
7										
8						10	12	12		loam
8										2'0" rubble
12										4'0" fine sand and silt
14					6'6"	4	8	10		dry medium to fine sand, little silt
18										
25										
28										
31										9'0"
10					11'6"	14	21	24		wet fine sand and silt, some medium to coarse gravel (hardpan)
15										15'0"
20										21'6" rock
25										
30										bottom of boring
35										
40										
GROUND SURFACE TO _____ FT. USED _____ CASING THEN _____ CASING TO _____ FT.										HOLE NO. 8
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST										
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%										

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.										CLIENT: Greater Hartford Flood Comm.										SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>9</u>									
CONTRACTOR										PROJECT NO. 1960-3										LINE									
FOREMAN - DRILLER Bessette										PROJECT NAME Park River Conduit Ext.										STATION									
INSPECTOR Batterson										LOCATION Hartford, Conn.										OFFSET									
GROUND WATER OBSERVATIONS										CASING TYPE <u>W.I.</u> SAMPLER <u>S.S.</u> CORE BAR _____										Date Start <u>12/27</u> Date Fin. <u>12/27/60</u>									
AT ____ FT. AFTER ____ HOURS										SIZE I.D. <u>2 1/2</u> <u>1 3/8</u>										SURFACE ELEV. <u>25.1</u>									
AT ____ FT. AFTER ____ HOURS										HAMMER WT. <u>300</u> <u>140</u> BIT _____										GROUND WATER ELEV. <u>24.6</u>									
										TYPE <u>W.I.</u> SAMPLER <u>S.S.</u> CORE BAR _____																			
										SIZE I.D. <u>2 1/2</u> <u>1 3/8</u>																			
										HAMMER WT. <u>300</u> <u>140</u> BIT _____																			
										HAMMER FALL <u>24"</u> <u>30"</u>																			
DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.																
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18		MOIST			ELEV.															
	19																												
	28																												
	146	Casing Refused																											
		c								3		1'6"	GR.COARSE TO FINE SAND & GRAVEL																
		c								3	MEDIUM DENSE	3'0"	BR.SAND, SIST, GRAVEL, PIECES OF ROCK																
		c								4			BR.FINE SANDSTONE																
		c								4			RUN 1 3'to 8'																
		c								6		8'0"	RECOVERY 14"																
10													END OF HOLE 8'0"																
15																													
20																													
25																													
30																													
35																													
40																													

GROUND SURFACE TO ____ FT., USED ____ " CASING THEN ____ " CASING TO ____ FT.

D : DRY W = WASHED C : CORED P : PIT A : AUGER UP : UNDISTURBED PISTON

UB : UNDISTURBED BALL CHECK T : THIN WALL V : VANE TEST

PROPORTIONS USED TRACE : 0-10%, LITTLE : 10-20%, SOME : 20-35%, AND : 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.										CLIENT: <u>Greater Hartford Flood Com.</u>										SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>10</u>									
CONTRACTOR										PROJECT NO. 1960-3										LINE									
FOREMAN - DRILLER Bessette										PROJECT NAME Park River Conduit Ext.										STATION									
INSPECTOR Batterson										LOCATION Hartford, Conn.										OFFSET									
GROUND WATER OBSERVATIONS										CASING SAMPLER CORE BAR.										Date Start <u>12/23</u> Date Fin. <u>12/23/60</u>									
AT _____ FT. AFTER _____ HOURS										TYPE <u>W.I.</u> SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>										SURFACE ELEV. <u>25.6</u>									
AT _____ FT. AFTER _____ HOURS										SAMPLER <u>M.S.</u> <u>1 3/8</u> <u>140</u> BIT. <u>30"</u>										GROUND WATER ELEV. <u>-24.9</u>									

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18		MOIST	ELEV.	
7													DARK GRAY SAND & SILT, SOME GRAVEL; CEMENTED TILL & SOFT ROCK
8													
29													
186		Casing Refused											
5		C								4			RUN 1 4'0" to 9'0" REC 13" BROWN FINE SANDSTONE
		C								4			
		C								6			
		C								6			
		C								5			
10											9'0"		END HOLE AT 9'0"
40													

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.										HOLE NO. 10									
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST																			
PROPORTIONS USED: TRACE : 0-10%, LITTLE : 10-20%, SOME : 20-35%, AND : 35-50%																			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>11</u>			
CONTRACTOR				PROJECT NO. 1960-3				LINE			
FOREMAN - DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION			
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET			
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE <u>W.1</u> SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>				SAMPLER <u>W.1</u> SIZE I.D. <u>1 3/8</u> BIT. <u>140</u> CORE BAR. <u>30"</u>			
								Date Start <u>12/23</u> Date Fin. <u>12/23/60</u> SURFACE ELEV. <u>25.3</u> GROUND WATER ELEV. <u>24.6</u>			

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT	0-6	6-12				
7												
14												
131		Casing Refused										
		c							4	LOOSE		DARK GRAY FINE SAND & SILT, TRACE GRAVEL SOFT BROWN SANDSTONE
5		c							6	FROZEN	2'0"	
		c							6	DENSE	3'0"	
		c							4			
		c							8	MEDIUM HARD	8'0"	BR. FINE SANDSTONE RUN #1 3' to 8' REC. 16"
10												
15												
20												
25												END HOLE AT 8'0"
30												
35												
40												

GROUND SURFACE TO _____ FT. USED _____" CASING THEN _____" CASING TO _____ FT.										HOLE NO. 11
O: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST										
PROPORTIONS USED: TRACE: 0-10%, LITTLE: 10-20%, SOME: 20-35%, AND: 35-50%										

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.										CLIENT: Greater Hartford Flood Comm.										SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>12</u>									
CONTRACTOR										PROJECT NO. 1960-3										LINE									
FOREMAN - DRILLER Bessette										PROJECT NAME Park River Conduit Ext.										STATION									
INSPECTOR Batterson										LOCATION Hartford, Conn.										OFFSET									
GROUND WATER OBSERVATIONS										Casing W.I. Sampler S.S. Core Bar.										Date Start 12/22 Date Fin. 12/22									
AT _____ FT. AFTER _____ HOURS										TYPE SIZE I.D. 2 1/2 1 3/8										SURFACE ELEV. 25.9									
AT _____ FT. AFTER _____ HOURS										HAMMER WT. 300 BIT.										GROUND WATER ELEV. -2' 25.6									
										Casing W.I. Sampler S.S. Core Bar.										Date Start 12/22 Date Fin. 12/22									
										TYPE SIZE I.D. 2 1/2 1 3/8										SURFACE ELEV. 25.9									
										HAMMER WT. 300 BIT.										GROUND WATER ELEV. -2' 25.6									
										Casing W.I. Sampler S.S. Core Bar.										Date Start 12/22 Date Fin. 12/22									
										TYPE SIZE I.D. 2 1/2 1 3/8										SURFACE ELEV. 25.9									
										HAMMER WT. 300 BIT.										GROUND WATER ELEV. -2' 25.6									

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18		MOIST.			ELEV.
5	18										FROZEN		GRAY FINE SAND & SILT TRACE GRAVEL & ROOTS	
	12										WET	3'0"		
	10												BR. SAND, SILT, GRAVEL	
	41										DENSE			
	186 Casing Refused										MOIST	5'0"		
10		C								3	MEDIUM HARD		BR.FINE SANBSTONE RUN #1 5'TO 10" REC. 20"	
		C								3				
		C								4				
		C								4				
		C								5		10'0"		
END HOLE AT 10'0"														

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.	HOLE NO. 12
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D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON

UB = UNDISTURBED BALL CHECK T = THIN WALL V = VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>13</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Besette				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				TYPE <u>CASING</u> W.1 <u>SAMPLER</u> S.S. <u>CORE BAR.</u> SIZE I.D. 2 1/2 <u>1 3/8</u> HAMMER WT. 300 <u>140</u> <u>BIT.</u> HAMMER FALL 24" <u>30"</u>				Date Start <u>12/21</u> Date Fin. <u>12/21/60</u> SURFACE ELEV. _____ GROUND WATER ELEV. _____	

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18					
	27												LOOSE WET 2'0" DENSE MOIST 5'0"	DARK GR. SILT & SAND BOULDERS & RIP RAP BR. SAND, SILT AND GRAVEL PIECES OF ROCK
	46													
	82													
	111													
5	127	casing refused												
													REFUSAL - ROCK END OF HOLE @ 5'0" (REMOVED MACHINE DUE TO RISING WATERS)	
40														

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. **13**
 D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON
 UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.								CLIENT: Greater Hartford Flood Comm.								SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>15</u>							
CONTRACTOR								PROJECT NO. 1980-3								LINE							
FOREMAN - DRILLER Bennette								PROJECT NAME Park River Conduit Ext.								STATION							
INSPECTOR Batterson								LOCATION Hartford, Conn.								OFFSET							
GROUND WATER OBSERVATIONS								CASING V.I								SAMPLER S.S				CORE BAR.			
AT _____ FT. AFTER _____ HOURS								TYPE 2 1/2								SIZE I.D. 1 3/8							
AT _____ FT. AFTER _____ HOURS								HAMMER WT. 300								BIT.							
								HAMMER FALL 24"								30"							
																Date Start 12/19 Date Fin. 12/19/60							
																SURFACE ELEV. 26.6 (WATER)							
																GROUND WATER ELEV. _____							

DEPTH	CASING BLOWS PER FOOT	SAMPLE							BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18	MOIST	ELEV.				
														1'6"	RIVER WATER (PARK RIVER)
													LOOSE	3'0"	COBBLES AND BOULDERS
5													BENSE MOIST		RED BROWN SILT, SOME MEDIUM TO FINE GRAVEL (HARDPAN)
														7'0"	
													MEDIUM HARD		BROWN FINE SANDSTONE RUN 1 7' to 12' RECOVERY 25"
10														12'0"	
															END HOLE AT 12'0"
15															
20															
25															
30															
35															
40															

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.

D=DRY W=WASHED C=CORED P=PIT A=AUGER UP=UNDISTURBED PISTON
UB=UNDISTURBED BALL CHECK T=THINWALL V=VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

HOLE NO. 15

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.										CLIENT: <u>Greater Hartford Flood Comm</u>										SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>16</u>																			
CONTRACTOR										PROJECT NO. <u>1960-3</u>										LINE																			
FOREMAN -DRILLER <u>Bessette</u>										PROJECT NAME <u>Park River Conduit Ext.</u>										STATION																			
INSPECTOR <u>Batterson</u>										LOCATION <u>Hartford, Conn.</u>										OFFSET																			
GROUND WATER OBSERVATIONS										CASING TYPE <u>W.I</u> SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>										SAMPLER <u>S.S</u> <u>1 3/8</u> <u>140</u> <u>30"</u>										CORE BAR. BIT. 									
AT _____ FT. AFTER _____ HOURS										Date Start <u>12/17</u> Date Fin. <u>12/17/60</u>										SURFACE ELEV. <u>26.6</u> (<u>Water</u>)																			
AT _____ FT. AFTER _____ HOURS										GROUND WATER ELEV. _____																													

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18		MOIST.			ELEV.
													RIVER WATER (PARK RIVER)	
	12											2'0"		
	22											3'0"	COBBLES & BOULDERS	
5	48													
	40	1	D	18"	16"	6'6"	12	20	17		DENSE MOIST		RED BROWN SILT, LITTLE MEDIUM TO FINE GRAVEL (HARDPAN)	
	64													
	99													
	124													
10	238	Casing Refused										10'0"		
	C									4				
	C									4	MEDIUM HARD		BROWN FINE SANDSTONE RUN 1 10' to 15' RECOVERY 24"	
	C									4				
	C									6				
15	C									6		15'0"		
20													END HOLE AT 15'0"	
25														
30														
35														
40														

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.

D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON

UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

HOLE NO. 16

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>17</u>			
CONTRACTOR				PROJECT NO.				LINE			
FOREMAN -DRILLER Miller				PROJECT NAME				STATION			
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET			
GROUND WATER OBSERVATIONS AT <u>6</u> FT. AFTER <u>24</u> HOURS AT <u>6</u> FT. AFTER <u>48</u> HOURS				CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u> "				SAMPLER CORE BAR. <u>1 3/8</u> <u>1 3/8</u> BIT.			
				Date Start <u>10/20/60</u> Date Fin <u>10/21/60</u> SURFACE ELEV. <u>38.20</u> GROUND WATER ELEV. _____							

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
8													
12													
15													
12													
5						5'to	4	4	4				fine to medium sand, some silt, gravel, cobbles, and cinders
14						6'6"							
10													
8													
8													
10													
8						9'6"	6	12	6				
10						to 11'						12'0"	
10													
20						12'to							fine to coarse sand, silt, gravel, and cobbles
29						13'6"	12	14	25				
15						14'6"						15'7"	
39						to 15'6"	21	32					
36													
25													
34													gravel, sand, and silt hardpan
33													
20						20'to	19	25	29				
68						21'6"							
						21'6"							
						to 23'	17	31	48				
25												26'0"	
30												31'0"	rock, laminated red shale 2'1" recovery from 5'run
35													bottom of boring 1st foot - 10 min. 2nd " - 12 " 3rd " - 12 " 4th " - 9 " 5th " - 8 "
40													

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO.
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2646 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Com.</u>				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>18</u>			
CONTRACTOR				PROJECT NO. 1960-3				LINE			
FOREMAN -DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION			
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET			
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>				SAMPLER <u>S.S</u> <u>1 3/8</u> <u>140</u> <u>30"</u>			
								CORE BAR. BIT.			
								Date Start <u>12/14/60</u> Date Fin. <u>12/15/60</u> SURFACE ELEV. <u>23.7 (Bottom)</u> GROUND WATER ELEV. <u>25.7 (N/L)</u>			

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18				
	10											2'0"	ROVER WATER (PARK RIVER)
	27											LOOSE 3'0"	COBBLES & BOULDERS
5	45												
	53	1	D	18"	16'6"6"	24	32	31		VERY DENSE MOIST			RED BR. SILT, TRACE FINE GRAVEL (HARDPAN)
	94												
	148												
	247	Casing Refused										9'0"	
10			C										
			C										
			C						4				
			C						6				
			C						6				
15			C						8				
			C						8				
			-C-									16'6"	
20													
25													
30													
35													
40													

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT.										HOLE NO. <u>16</u>
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST										
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%										

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.										CLIENT: Greater Hartford Flood Comm.										SHEET 1 OF 1 HOLE NO. 19									
CONTRACTOR										PROJECT NO. 1960-3										LINE									
FOREMAN —DRILLER Benette										PROJECT NAME Park River Conduit Ext.										STATION									
INSPECTOR Batterson										LOCATION Hartford, Conn.										OFFSET									
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS										CASING V.I. TYPE SS SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24" SAMPLER SS NO. 13/8 BIT. 140 CORE BAR. 30"										Date Start 12/8 Date Fin. 12/8/60 SURFACE ELEV. 26.9 GROUND WATER ELEV.									
DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.																
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18		MOIST	ELEV																	
4																													
4																													
14																													
29																													
5	104	1	D	18"	16"	5'0"	7	12	24		MEDIUM COMPACT MOIST	5'0"	DARK GRAY SAND & SILT LITTLE MUCK, PIECES OF WOOD																
			c							2																			
			c							2																			
			c							3																			
			c							8																			
10			c									10'0"	RED SHALE ROCK RUN #1 5'to 10' REC. 30"																
													END HOLE AT 10'0"																
15																													
20																													
25																													
30																													
35																													
40																													

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.

D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON
 UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>20</u>	
CONTRACTOR				PROJECT NO.				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Capitol Ave., Hartford				OFFSET	
GROUND WATER OBSERVATIONS AT <u>13'</u> FT. AFTER <u>1</u> HOURS AT <u>13'</u> FT. AFTER <u>24</u> HOURS				CASING TYPE SIZE I.D. <u>2 1/2"</u> HAMMER WT. <u>350</u> HAMMER FALL <u>24"</u>		SAMPLER <u>1 3/8"</u> <u>140</u> <u>30"</u>		CORE BAR. <u>1 7/8"</u> BIT.	
				Date Start <u>10/10</u> Date Fin. <u>10/19/60</u> SURFACE ELEV. <u>38.55</u> GROUND WATER ELEV. _____					

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6"	6-12"	12-18"				
51											1'-0"	M A C A D A M	
20													
25													
22													
15													
10					4' 6"	12	10	9					
10					to 6"								
8													
					9' 8"								
10					to 10"	4	3	3			11' 0"		
											13' 0"	fine to medium sand, silt, and gravel	
15												red shale 13' to 16' = 26" rec. 16' to 21' = 36" rec.	
20											21' 0"		
												bottom of boring	
												drill time: 1st foot = 10 min. 2nd foot = 9 min. 3rd foot = 9 min. 4th foot = 12 min. 5th foot = 11 min. 6th foot = 8 min. 7th foot = 9 min.	
25													
30													
35													
40													

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.										HOLE NO.
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST										
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%										

[illegible]

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.										CLIENT: Greater Hartford Flood Comm.										SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>32</u>																			
CONTRACTOR										PROJECT NO. 1960-3										LINE																			
FOREMAN —DRILLER Bessette										PROJECT NAME										STATION																			
INSPECTOR Battersen										LOCATION Hartford, Conn.										OFFSET																			
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS										CASING TYPE SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24"										SAMPLER CORE BAR. 133/8 140 30"										Date Start <u>11/22</u> , Date Fin <u>11/12/60</u> SURFACE ELEV. _____ WATER ELEV. 31.8									
DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.																										
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18		MOIST.	ELEV.																											
													Park River																										
												3'0"																											
5	1										soft wet		Black soft muck																										
	1					6'6"	1	0	0			7'0"																											
	1										spft		gray soft silt, pieces of rotted wood																										
10	1										wet																												
	2					11'6"	1	3	2			13'0"																											
	2																																						
	67										dense moist	15'0"	red clay & silt, little																										
15	300					14'6"	12	27	39																														
	390	casing refused									medium hard rock		gray medium hard shale, chopped and drove from 15'6" to 19'6" using 300 lb. wt. and fishtail bit																										
		no penetration with sampler										19'6"																											
20													end hole @ 19'6"																										
													note: moved boring 32 twice (5' each move) refused at 12' & at 13'0"																										
25																																							
30																																							
35																																							
40																																							

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.

D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON

UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-60%

ENGINEERING SERVICES INC. 2040 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>33</u>	
CONTRACTOR				PROJECT NO. 1900-3				LINE	
FOREMAN --DRILLER Bessette				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>		SAMPLER <u>1 3/8</u> <u>140</u> <u>30"</u>		CORE BAR. _____ BIT. _____	
						Date Start <u>11/12</u> Date Fin. <u>11/14/60</u>		SURFACE ELEV. _____ GROUND WATER ELEV. <u>31.8</u>	

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18				
													Park River
												3'0"	
5	1												soft
	2		d			6'6"	1	1	3				wet
	3												
	4												
	5												
10	12												soft
	12		d			11'6"	7	14	20				wet
	17												hard
	46												comp
	107		d			13'0"	12	13	50				wet
15			c							6			med
			c							6			hard
			c							8			rock
			c							11			
			c							11			
20													18'0"
25													
30													
35													
40													

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.										HOLE NO. 33	
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST											
*PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%											

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>34</u>	
CONTRACTOR				PROJECT NO.				LINE	
FOREMAN —DRILLER Bessette				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. 2 1/2" HAMMER WT. 300 HAMMER FALL 24"		SAMPLER 1 3/8" 140 30"		CORE BAR BIT. Date Start <u>11/1/60</u> Date Fin. <u>11/1/60</u> SURFACE ELEV. _____ GROUND WATER ELEV. 31.8	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.					
5										Park River
10	4							soft	10'0"	dark gray coarse to fine sand, some gravel, mixed with black muck
	4							wet	13'0"	
	8									
	3									
15	2									red clay, trace fine sand & gravel
	3	1	d			15'6"	1	2	3	
	22									
	43									
20	87							compact		red clay & silt, some coarse gravel, little fine sand
	128	2	d			20'6"	22	31	20	
	209									
	301							dense		
		3	d			24'0"	40	65	24'0"	very dense dry
25			c							
			c							
			c							
			c			sampler refused @ 28'			28'0"	cored for penetration, using fish tail bit 24' to 28' very dense till & pieces of rock
30										
35										end hole @ 28'
40										

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.

D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

HOLE NO. **34**

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>35</u>			
CONTRACTOR				PROJECT NO. 1960-3				LINE			
FOREMAN —DRILLER B Bessette				PROJECT NAME				STATION			
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET			
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE _____ SIZE I.D. <u>2 1/2"</u> SAMPLER <u>1 3/8"</u> CORE BAR. _____ HAMMER WT. <u>300</u> BIT. _____ HAMMER FALL <u>24"</u> <u>30"</u>				Date Start <u>11/9</u> Date Fin. <u>11/11/60</u> SURFACE ELEV. _____ GROUND WATER ELEV. <u>31.5</u>			

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
											2'0"	Park River	
5	1					6'6"	1	0	1		soft wet		dark gray muck, traces of peat
	1												
	2												
	2												
10	1					11'6"	1	1	1		soft wet	11'0"	red clay
	2											13'0"	
	3												
	16												
15	21					15'6"	10	16	20		hard moist		red clay & some silt, trace of fine sand, little coarse to fine gravel
	18												
	24												
	22												
	28												
20	30					21'6"	12	18	24				
	20												
	26												
	31												
	28												
25	44					26'6"	10	16	22				
	36												
	48												
	55												
	72											29'0"	
30	187					30'6"	37	46	72		very dense moist		red clay & silt, little fine sand & gravel (cemented)
	146											33'0"	
	281												
	382												
35											med hard	36'0"	run #1 33'6" 36' rec.6" red shale rock
											hard		run #2 36'to 40' red shale rock
40												40'0"	end of hole 40'

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO. 35
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2546 MAIN STREET GLASTONBURY, CONN.		CLIENT: Greater Hartford Flood Comm		SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>36</u>	
CONTRACTOR		PROJECT NO.		LINE	
FOREMAN - DRILLER Bessette		1960-3		STATION	
INSPECTOR Batterson		PROJECT NAME		OFFSET	
LOCATION Hartford, Conn.		CASING		SAMPLER	
GROUND WATER OBSERVATIONS		CORE BAR.		Date Start <u>11/11</u> Date Fin. <u>11/11/60</u>	
AT _____ FT. AFTER _____ HOURS		TYPE		SURFACE ELEV. _____	
AT _____ FT. AFTER _____ HOURS		SIZE I.D. <u>2 1/2</u> <u>1 3/8</u>		GROUND WATER ELEV. <u>31.8</u>	
		HAMMER WT. <u>300</u> <u>140</u>			
		HAMMER FALL <u>24"</u> <u>30"</u>			

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
													Park River
	2											3'0"	
5	3												soft
	4					6'6"	2	2	2				wet
	7												dark grey muck & clayey silt
	6												
	4												
10	4												grey clay & silt
	2					11'6"	1	2	2				
	3												
	2											13'0"	
	6												red clay, trace of fine sand
15	7												
	4					15'6"	2	3	7				
	18											17'0"	
	29												red clay; some silt; little
20	37												fine sand and coarse to fine
	74												gravel
	40					21'6"	20	27	41				
	63												
	78												
	197												
25	208												
	264					26'6"	22	29	33				
	418											27'0"	
													very dense till & red shale
													rock fragments
30													end hole @ 30'0"
													note: cored from 27' to 30'
													using fish tail bit
35													
40													

GROUND SURFACE TO _____ FT.		USED _____" CASING		THEN _____" CASING TO _____ FT.		HOLE NO. 36
D = DRY	W = WASHED	C = CORED	P = PIT	A = AUGER	UP = UNDISTURBED PISTON	
UB = UNDISTURBED BALL CHECK		T = THINWALL		V = VANE TEST		
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%						

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>37</u>			
CONTRACTOR				PROJECT NO. 1960-3				LINE			
FOREMAN —DRILLER Bennette				PROJECT NAME Park River Conduit Ext.				STATION			
INSPECTOR Battersen				LOCATION Hartford, Conn.				OFFSET			
GROUND WATER OBSERVATIONS				CASING SAMPLER CORE BAR.				Date Start <u>11/9/60</u> Date Fin. <u>11/9/60</u>			
AT _____ FT. AFTER _____ HOURS				TYPE SIZE I.D. <u>2 1/2</u> <u>1 3/8</u>				SURFACE ELEV. _____			
AT _____ FT. AFTER _____ HOURS				HAMMER WT. <u>300</u> <u>140</u> BIT.				GROUND WATER ELEV. <u>31.5</u>			
				HAMMER FALL <u>24"</u> <u>30"</u>							

DEPTH	CASING BLOWS PER FOOT	SAMPLE				NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.
		O-6	6-12	12-18	MOIST.						ELEV.						
																Park River	
5																	dark gray silt
10	1									13'6"	1	1	1	soft	11'0"		red clay & silt, some fine sand & gravel, cemented
	1																
	1	1	d														
	2																
	27	2	d							15'6"	16	28	37	dense moist			red shale (decomposed rock) end hole @ 23'0"
	44																
	40																
	190																
	265	3	d							19'6"	29	47	75		19'6"		note: chopped & drove using 300 lb.wt. for penetration from 20' to 23'
		4	d							20'0"	155	refused					
20														hard			end hole @ 23'0"
										sampler refused					23'0"	</	

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>38</u>			
CONTRACTOR				PROJECT NO. 1960 - 3				LINE			
FOREMAN -DRILLER Giggey				PROJECT NAME				STATION			
INSPECTOR				LOCATION Hartford, Conn.				OFFSET			
GROUND WATER OBSERVATIONS AT <u>7'6"</u> FT. AFTER <u>24</u> HOURS AT <u>7'6"</u> FT. AFTER <u>48</u> HOURS				TYPE SIZE I.D. <u>2 1/2</u> <u>1 3/8</u> HAMMER WT. <u>300</u> <u>140</u> BIT. HAMMER FALL <u>24</u> <u>30</u>				Date Start <u>10/25</u> Date Fin. <u>11/26/60</u> SURFACE ELEV. <u>37.8</u> GROUND WATER ELEV. _____			

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
6													sandy silt, cinders, misc. fill
5													
5													
5													
8						5'to							
12						6'6"	3	2	2				
5													
7													
8													
12						10'to						9'0"	
8						11'6"	1	1	1				loose silt and clay, traces organic material; unable to recover sample at 10'to 11'6" and at 15' to 16'6"
9													
7													
10													
11						15'to							
15						16'6"	1	1	1				
12													
10													
9													
10						20'to						19'0"	
19						21'6"	7	7	4				silt, clay, fine gravel, & organic material.
12													
14													
12													
25						25'to						24'0"	silt, clay, and fine gravel "hardpan"
						26'6"	22	28	30			26'6"	
													bottom of boring
30													
35													
40													

GROUND SURFACE TO _____ FT, USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. 38
 D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.			CLIENT: Greater Hartford Flood Comm.			SHEET <u>1</u> OF <u>1</u> HOLE NO. 39		
CONTRACTOR			PROJECT NO.			LINE		
FOREMAN -DRILLER Bessette			PROJECT NAME Park River Conduit Extensions			STATION		
INSPECTOR Batterson			LOCATION Hartford, Conn.			OFFSET		
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS			CASING TYPE W.I. SAMPLER 5.5 CORE BAR. SIZE I.D. 2 1/2 1 3/8 HAMMER WT. 300 140 BIT. HAMMER FALL 24" 30"			Date Start 11/8 Date Fin. 11/9/60 SURFACE ELEV. _____ River WATER ELEV. 31.5		

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST. ELEV.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS. INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18				
5	1												
	4	1	D	18"14"	6'6"	2	1	2		loose wet	8'0"	Gray coarse to fine sand & gravel; mixed with river muck, boulders	
	11												
	13												
	4												
10	2									soft wet		red clay	
	2	2	D	18"13"	11'6"	1	1	1					
	2												
	3												
	6												
15	27									hard moist	14'0"	red clay & silt, little fine sand, some gravel	
	33	3	D	18"16"	15'8"	12	16	18		very dense dry		same as #4 (cemented)	
	48												
	164												
	260												
20	299	4	D	18"17"	19'6"	28	47	51			20'0"		
										hard		red shale decomposed rock	
											23'6"		
		5	D	3" 3"	23'6"	150						end hole @ 23'6"	
25													
30												note: chopped & drove using 300 lb. wt. for penetration from 20'to 23'6"	
35													
40													

GROUND SURFACE TO _____ FT., USED _____" CASING THEN _____" CASING TO _____ FT.										HOLE NO. 39
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST										
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%										

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.		CLIENT: <u>GREATER WFD FLOOD COMM</u>		SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>40</u>	
CONTRACTOR		PROJECT NO. <u>1960-3</u>		LINE	
FOREMAN -DRILLER <u>BIGGETT</u>		PROJECT NAME		STATION	
INSPECTOR <u>BATTERSON</u>		LOCATION <u>HARTFORD, CONN</u>		OFFSET	
GROUND WATER OBSERVATIONS AT <u>8'-6"</u> FT. AFTER <u>24</u> HOURS AT <u>8'-6"</u> FT. AFTER <u>48</u> HOURS		TYPE <u>CASING</u> SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>		SAMPLER <u>1 1/2</u> CORE BAR. <u>140</u> BIT. <u>30</u>	
				Date Start <u>10-26-60</u> Date Fin. <u>10-26-60</u> SURFACE ELEV. <u>37.5</u> GROUND WATER ELZV. _____	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6 6-12 12-18						
5	6										SILT AND FINE SAND WITH CINDER FILL		
	6												
	8												
	5												
	6			18	6.5	6	4	3					
	15												
	20												
	12												
	7									9.0			
10	6			18	11.5	2	2	2	SLIPPED	SAMPLE	SILT, CLAY, SAND AND FINE GRAVEL		
	6												
	8												
	5												
	8												
15	9			18	16.5	4	3	3					
	9												
	8									18.0			
	8												
20	8			18	21.5	3	3	3			SILTY SAND AND ORGANIC MATERIAL		
	15												
	17												
	14												
	12												
25	12			18	26.5	6	24	28		25.0			
	28												
	58										SILT, CLAY, SOME SAND AND GRAVEL "HARDPAN"		
	64												
	110												
30				18	31.5	50	50	50		31.5			
											BOTTOM OF BORE		
40													

GROUND SURFACE TO _____ FT., USED _____" CASING THEN _____" CASING TO _____ FT.

D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON
 UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

HOLE NO. 40

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>41</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Bessette				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24"		SAMPLER 1 3/8 140 30"		CORE BAR. 1 3/8 BIT. 31.7	
								Date Start 11/6 Date Fin. 11/8/60 SURFACE ELEV. _____ GROUND WATER ELEV. _____	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12					12-18
5												Park River	
1													
10	1	D	18"	18"	10'6"	w	o	h					soft wet
1													
1													
6													
15	7	2	D	18"	17"	15'6"	w	o	h				same as #1
7													
13													
146													
20	160	3	D	6"	4"	19'			125				med comp red hard
294													
		c							9				
		c							10				
		c							20			hard	
		c							22				
25		c	60"	36"	25'				20				
30												end hole @ 25'0"	
35												rock: 5'run, 3' recovery	
40													

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.								HOLE NO. 41	
D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST									
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%									

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>42</u>							
CONTRACTOR				PROJECT NO.				LINE							
FOREMAN - DRILLER				PROJECT NAME				STATION							
INSPECTOR				LOCATION				OFFSET							
Giggey Batterson				1960-3 Hartford											
GROUND WATER OBSERVATIONS AT <u>4'6"</u> FT. AFTER <u>24</u> HOURS AT <u>4'6"</u> FT. AFTER <u>48</u> HOURS				CASING TYPE SIZE I.D. <u>2 1/2"</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>				SAMPLER <u>1 3/8"</u> <u>140</u> <u>30</u>				CORE BAR <u>1 3/8"</u> BIT.			
				Date Start <u>10/24</u> Date Fin <u>10/25/60</u> SURFACE ELEV. <u>38.6</u> GROUND WATER ELEV. _____											

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
1						6	7	10					
2													
3													
4													
5					5' to								
6					6'6"	6	6	5				fine sand and silt, misc. fill	
7													
8													
9													
10					10' to								
11					11'6"	1	2	2					
12													
13													
14													
15					15' to								
16					16'6"	1	2	2					
17													
18													
19													
20					20' to	3	3	2					
21					21'6"								
22													
23													
24					23' to								
25					24'	50	150					hardpan red silt, clay, and gravel	
26													
27													
28													
29													
30					30' to								
31					31'	145	lost sample						
32													
33													
34													
35													
36													
37													
38													
39													
40													

GROUND SURFACE TO _____ FT.	USED _____ CASING	THEN _____ CASING TO _____ FT.
O = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST		
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%		

HOLE NO. **42**

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.										CLIENT: <u>Greater Hartford Flood Comm</u>										SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>43</u>									
CONTRACTOR										PROJECT NO. 1960-3										LINE									
FOREMAN --DRILLER Bessette										PROJECT NAME										STATION									
INSPECTOR Batterson										LOCATION Hartford, Conn.										OFFSET									
GROUND WATER OBSERVATIONS										CASING SAMPLER CORE BAR.										Date Start <u>11/14</u> Date Fin <u>11/15/60</u>									
AT _____ FT. AFTER _____ HOURS										TYPE SIZE I.D. <u>2 1/2</u> <u>1 3/8</u>										SURFACE ELEV. _____									
AT _____ FT. AFTER _____ HOURS										HAMMER WT. <u>300</u> <u>140</u> BIT.										WATER WATER ELEV. <u>31.5</u>									
DEPTH		CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.																
			NO.	TYPE	PEN.	REC.	DEPTH @ BOT.																						
								0-6	6-12					12-18															
		1										2'0"	Park River																
5		1									soft wet		black-gray muck & silt																
		2				5'0"	1	2	1			6'0"																	
		3																											
		2																											
		3																											
		2									soft wet		brown red coarse to fine sand, some gravel & muck (tree roots)																
10		8				10'6"	3	7	4			13'0"																	
		4																											
		4																											
		4																											
		5									firm wet																		
15		7				15'6"	4	4	5			17'0"	red clay & silt, little fine sand and gravel																
		19																											
		213																											
		264	c										boulders, 17'to 20' rec.19"																
		187	c										sandstone																
20		124	c								boulder	20'0"																	
		128	d			21'6"	17	18	125																				
		274	casing refused										red clay & silt, little fine sand & gravel impregnated with cobbles & boulders																
			c								dense moist																		
			c																										
			c																										
25		5	d			26'6"	sampler refused					26'0"																	
													end hole @ 26'0"																
													note: cored for penetration 22'to 26' with fishtail bit																
30																													
35																													
40																													

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT.

D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST

HOLE NO. 43

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2046 MAIN STREET GLASTONBURY, CONN.						CLIENT: Greater Hartford Flood Comm.							SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>44</u>									
CONTRACTOR						PROJECT NO. 1960-3									LINE							
FOREMAN — DRILLER Bessette						PROJECT NAME									STATION							
INSPECTOR						LOCATION Hartford, Conn.									OFFSET							
GROUND WATER OBSERVATIONS						CASING SAMPLER CORE BAR.									Date Start <u>11/15</u> Date Fin <u>11/15/60</u>							
AT _____ FT. AFTER _____ HOURS						TYPE SIZE I.D. 2 1/2" 1 3/8"									SURFACE ELEV. _____							
AT _____ FT. AFTER _____ HOURS						HAMMER WT. 300 140 BIT. _____ HAMMER FALL 24" 30"									G.W. WATER ELEV. 31.5							
DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.									
		NO.	TYPE	PEN.	REC.			0-6	6-12		12-18	MOIST		ELEV.								
													Park River									
	2										2'0"											
	3																					
5	2									soft wet			black muck, some gray clayey silt									
	2				5'6"	1	2	1														
	1										8'0"											
	2																					
10	5									soft wet			red clay									
	5				11'6"	2	2	2														
	7																					
	3										14'0"											
	11																					
15	22									med hard wet			red clay & silt, little fine sand, some coarse to fine gravel									
	40				16'6"	6	8	15														
	29																					
	41																					
	49																					
20	53									hard moist												
	40				21'6"	12	15	15														
	63																					
	89																					
	160																					
25	243									dense moist												
	197	d			26'6"	20	32	31														
	184	c																				
		c																				
		c																				
30		c																				
		d			31'6"	23	34	89			31'6"											
													refusal at 31'6"									
35													note: cored for penetration 26'6" to 30' using fishtail bit.									
40																						

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.

O = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON

UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST

PROPORTIONS USED: TRACE = 0 - 10%, LITTLE = 10 - 20%, SOME = 20 - 35%, AND = 35 - 50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.		CLIENT: Greater Hartford Flood Comm.		SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>45</u>	
CONTRACTOR		PROJECT NO. 1960-3		LINE	
FOREMAN —DRILLER Bessette		PROJECT NAME		STATION	
INSPECTOR Batterson		LOCATION Hartford, Conn.		OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS		CASING SAMPLER CORE BAR. TYPE SIZE I.D. 2 1/2 1 3/8 HAMMER WT. 300 140 BIT. HAMMER FALL 24" 30"		Date Start 11/15 Date Fin 11/16/60 SURFACE ELEV. _____ WATER ELEV. 31.5	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18					
												2'0"	Park River	
5											soft wet	6'6"	black coarse to fine sand mixed with muck, some gravel	
			d			6'6"	1	1	2					
											soft wet		black gray silt, pieces of rotted wood	
10						11'6"	1	3	2					
												15'0"		
15						16'6"	1	2	1				18'0"	red gray clay
											firm wet	20'0"	red clay, silt, trace fine sand	
20			c								boulder	22'0"	red sandstone boulder rock	
			c											
						26'6"					dense moist		red clay & silt, little fine sand, some gravel, cemented	
25			d			21'6"	18	23	30			27'0"		
			casing refused											
			c						8		med hard		run 1 27' to 32' rec. 24" red shale	
30			c						8					
			c						6					
			c						4					
			c						6			32'0"		
													end hole @ 32'0"	
35													Note: xxx lost water while coring @ 31'0" drove ole. at 32' refused	
40														

GROUND SURFACE TO _____ FT.		USED _____ " CASING		THEN _____ " CASING TO _____ FT.		HOLE NO. 45
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST						
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%						

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>2</u> HOLE NO. <u>46</u>	
CONTRACTOR				PROJECT NO.				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT <u>20</u> FT. AFTER <u>24</u> HOURS AT <u>20</u> FT. AFTER <u>48</u> HOURS				CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>		SAMPLER <u>SS</u> <u>1 3/8</u> <u>140</u> <u>30"</u>		CORE BAR. Date Start <u>10/25</u> Date Fin. <u>10/26/60</u> SURFACE ELEV. <u>50.8</u> GROUND WATER ELEV. _____	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
27											1'-0"	TRAP ROCK & Cobbles	
20													
15													
17													
16					5' to								
27					6' 6"	17	15	15					
21													
29													
24													
26					9' 6"								
18					to 11'	19	14	17					
17													
15													
24													
22					15' to						15' 0"	fine sand, silt, gravel, & cobbles	
18					16' 6"	3	3	3					
13													
12													
13													
12													
26													
25					20' to	2	2	2					
13					21' 6"								
14													
13					24' 6"	2	1	2					
13					to 26'								
12													
13													
12													
13					28' 6"	1	2	2					
12					to 30'						31' 0"	silt, clay, some fine sand	
24					32' 6"	3	4	5					
15					to 34'								
13													
14													
16					36' 6"								
18					to 37' 6"	6	8	8					
17													
19													
24					40' to	8	9	9			38' 6"		silt, fine sand, & gravel
40													
24					41' 6"							fine sand & silt	

GROUND SURFACE TO _____ FT. 41' 6" USED _____ " CASING THEN _____ " CASING TO _____ FT.

D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON
 UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST

PROPORTIONS USED: TRACE: 0-10%, LITTLE: 10-20%, SOME: 20-35%, AND: 35-50%

HOLE NO. 46

ENGINEERING SERVICES INC. 2546 MAIN STREET GLASTONBURY, CONN.										CLIENT: <u>Greater Hartford Flood Comm.</u>										SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>46</u>																			
CONTRACTOR										PROJECT NO. <u>1960-3</u>										LINE																			
FOREMAN --DRILLER <u>Miller</u>										PROJECT NAME										STATION																			
INSPECTOR <u>Batterson</u>										LOCATION <u>Hartford, Conn.</u>										OFFSET																			
GROUND WATER OBSERVATIONS AT <u>20</u> FT. AFTER <u>24</u> HOURS AT <u>20</u> FT. AFTER <u>48</u> HOURS										CASING TYPE SIZE I.D. <u>2 1/2"</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>										SAMPLER <u>SS</u> <u>1 3/8"</u> <u>140</u> <u>30"</u>										CORE BAR. BIT. Date Start <u>10/25</u> Date Fin <u>10/26/60</u> SURFACE ELEV. <u>50.8</u> GROUND WATER ELEV.									
DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.		STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.																									
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18		MOIST.	ELEV.																											
28																																							
24														42'0" fine sand & silt																									
45						45'to								silt, fine sand, gravel																									
						46'6"	21	28	31																														
50						50'to	54	65	80																														
						51'6"																																	
														51'6"																									
														bottom of boring																									
55																																							
60																																							
65																																							
70																																							
75																																							
80																																							

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.
 D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON
 UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

HOLE NO. 46

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.		CLIENT: <u>Greater Hartford Flood Comm.</u>		SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>56</u>	
CONTRACTOR		PROJECT NO. 1960-3		LINE	
FOREMAN --DRILLER Bessette		PROJECT NAME		STATION	
INSPECTOR Batterson		LOCATION Hartford, Conn.		OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS		CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>		SAMPLER CORE BAR. <u>1 3/8</u> <u>140</u> <u>30"</u>	
				Date Start <u>11/16</u> Date Fin. <u>11/16/60</u> SURFACE ELEV. _____ GROUND WATER ELEV. <u>31.5</u>	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.						DEPTH @ BOT.
									2'0"	Park River	
5	1										
	1										
	1										
	1		d		6'6"	1	0	0			
	1										
	2								8'0"	Black Gray Muck & Silt	
10	2										
	2				11'6"	1	1	1			
	2										
	4								13'6"	Gray Silt & Clay	
15	4										
	4				16'6"	1	1	1			
	5										
	4										
	3									Red Clay	
20	5										
	4				21'6"	2	2	1			
	4					sample slipped			22'6"		
	12										
	25										
25	36									Red Clay & Silt, little Fine Sand & Some Coarse to Fine Gravel	
	47				26'6"	14	24	50			
	147										
	208								28'0"		
									29'0"	Red Soft Shale Boulder	
30											
					34'6"	45	70	42			
35					Note: cored for penetration from 28' to 33' and 33' to 38'						
					39'6"	47	54	79			
40									39'6"	end hole @ 39'6"	

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT.				HOLE NO. 56	
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST					
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%					

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.		CLIENT: <u>Greater Hartford Flood Commission</u>		SHEET <u>1</u> OF <u>2</u> HOLE NO. <u>57</u>	
CONTRACTOR		PROJECT NO.		LINE	
FOREMAN —DRILLER Bennette		PROJECT NAME		STATION	
INSPECTOR		LOCATION Hartford, Conn.		OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS		CASING TYPE _____ SAMPLER _____ CORE BAR _____ SIZE I.D. <u>2 1/2</u> <u>1 3/8</u> HAMMER WT. <u>300</u> <u>140</u> BIT _____ HAMMER FALL <u>24"</u> <u>30"</u>		Date Start <u>11/16/60</u> Date Fin. <u>11/17/60</u> SURFACE ELEV. _____ GROUND WATER ELEV. <u>31.5</u>	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS: INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.						DEPTH @ BOT.
									2'0"	Park River	
5	2										
	2										
	4										
	6										
	7	1	d		8'6"	1	5	2		soft wet	
	2										
	2										
10	3										
	2										
	2										
	3										
	2	2	d						14'0"		
	2	2	d		15'6"	1	1	2		soft wet	
15	3										
	3										
	7										
	7										
20	7	3	d		21'6"	1	2	2			
	4										
	7										
	7										
	6										
25	6										
	4										
	9										
	9										
	8										
30	6										
	10										
	13								32'0"		
	87	5	d		33'6"	28	23	22		hard moist	
35	118									red clay & silt, some gravel trace of sand	
	111										
	89										
	93										
	176	6	d		38'6"	22	28	41	38'0"	cemented till	
40										very hard dry	

GROUND SURFACE TO _____ FT.		USED _____ " CASING		TO _____ " CASING TO _____ FT.		HOLE NO. <u>57</u>
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST						
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%						

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>57</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN —DRILLER Bessette				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING SAMPLER CORE BAR. TYPE _____ SIZE I.D. 2 1/2 1 3/8 HAMMER WT. 300 140 BIT. HAMMER FALL 24" 30"				Date Start 11/16/60 Date Fin. 11/17/60 SURFACE ELEV. _____ GROUND WATER ELEV. 31.5	

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18				
			C								very dense	41'6"	red cemented till
			C						8		medium		run 1 41'6" to 46'6" rec. 12"
			C						8		hard		red sandstone
45			C						10			46'6"	note: shale did not recover
			C						6				
			C						8				add hole @ 46'6"
50													
10													
15													
20													
25													
30													
35													
40													

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO. 57
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>2</u> HOLE NO. <u>58</u>	
CONTRACTOR				PROJECT NO.				LINE	
FOREMAN —DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Batterson				LOCATION				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>		SAMPLER <u>1 3/8</u> <u>140</u> <u>30"</u>		CORE BAR. <u>1 3/8</u> BIT. <u>31.7</u>	
						Date Start <u>11/21/69</u> Date Fin. <u>11/22/69</u> SURFACE ELEV. _____ WATER WATER ELEV. <u>31.7</u>			

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18				
											2'0"	Park River	
5	1										soft	black muck, rubbish, tree roots, silt	
	4												
	4												
	3										wet		
	1										7'0"		
	2												
10	2										soft	gray silt and clay	
	2												
	2												
	3										wet		
	4												
15	2											gray red silt & clay	
	2	1	D		16'6"	1	1	1					
	3												
	4												
20	5											red clay	
	7	2	D		21'6"	1	2	1					
	10												
	10												
25	10												
	10												
	11												
	14												
30	17											red clay and silt, some coarse to fine sand & gravel	
	27												
	57	3	D		32'6"	17	22	28					
	43												
35	55												
	62												
	113	4	D		36'6"	18	27	23					
	144												
	194												
	207												
40	218	5									39'0"	red fine sand, little silt & gravel	

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO. <u>58</u>
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Htfd.Flood Comm.				SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>58</u>			
CONTRACTOR				PROJECT NO. 1960-3				LINE			
FOREMAN —DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION			
INSPECTOR Batterson				LOCATION				OFFSET			
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING SAMPLER CORE BAR. TYPE SIZE I.D. 2 1/2 1 3/8 1 3/8 HAMMER WT. 300 140 BIT. HAMMER FALL 24" 30"				Date Start 11/21/60 Date Fin. 11/22/60 SURFACE ELEV. _____ WATER RIVER WATER ELEV. 31.7			

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
	74												red fine sand, little silt, some gravel
	83												
	97												
45	193											45'0"	red sand, silt & gravel, little clay - cemented occasional cbbble cored with diamond bit for penetration from 45'6" to 53'0"
5	287	6	D			45'6"	32	75	100				
			c										
			c										
			c										
			c										
50			c										run 1, 53'to 58'rec. 32" red shale
10			c										
			c										
			c										
			c										
55			c						7				end hole @ 58'0"
15			c						8				
			c						12				
			c						12				
			c						19			58'0"	
60													
20													
25													
30													
35													
40													

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. 58
 D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

DISTRICT NO. _____ COUNTY _____ B.S.M. PROJ. NO. _____	GILES DRILLING CORP. 2 PARK AVENUE NEW YORK 16, N. Y. SUBSURFACE INFORMATION Sheet No. 81 196	HOLE NO. <u>F.C. 6</u> LINE & STA. _____ OFFSET _____						
Greater Hartford Flood Commission								
NAME _____ NO. _____ QUAD. LOCATION <u>Hartford, Conn.</u> DATE, START <u>2/8/60</u> GND. ELEV. <u>40.8 M.S.L.</u> PED. CLASS. _____ DATE, FINISH <u>2/8/60</u> G. W. DEPTH <u>24 hrs 10' 3"</u>								
CASING O.D. <u>4"</u> I.D. <u>3 1/2"</u> WEIGHT OF HAMMER <u>300 & 140 lbs.</u> SAMPLER O.D. <u>2"</u> I.D. <u>1-3/8"</u> INSIDE LENGTH OF SAMPLER <u>20"</u>		HAMMER FALL <u>24"</u> CASING <u>24"</u> SAMPLER <u>30"</u>						
DEPTH BELOW GND. SURF	BLOWS ON CASING	SAMPLE NO.	BLOWS ON SAMPLER	CROSS SECTION	MOISTURE	COLOR	MECH. ANALYSIS % PASSING SIEVE NO. 4 10 40 200	FIELD IDENTIFICATION OF SOIL & REMARKS
0	24	1	4 2 1	18" D				Misc. Fill-Cinders, Ashes, Nails Wood, concrete, Some Red Clay & Gravel 0' - 19'
	18							
	11							
	10							
	10							
	3	2	3 2	18" D				
	10							
	11							
	13							
	12							
10	5	3	2 1	10" M				
	5							
	4							
	10							
	23							
	8	4	3 2	12" W				
	8							
	6							
	7							
	12							
20	11	5	2 3	13" W				
	16							
	10							
	12							
	12							
	11	6	M.W.M.W.	18"				
	12							
	13							
	13							
	14							
30	13	T. 1 Pushed		24"				
	13		31' - 33'					
	12							
	15							
	14							
	16	T. 2 Pushed		24"				
	17		36' - 38'					
	15							
	20							
	31							
40	36							
	94							
	262							
	270							
	278							
	110	7	32 68	18" M				
	163							
	177							
	282							
50	216							

DRILLING INSPECTOR H. D. Stubing ASS'T SOILS ENGINEER _____
 *SAMPLES SHOULD BE TAKEN AT APPROXIMATELY 5 FT. INTERVALS AND WHEREVER THERE IS AN INDICATION OF POSSIBLE CHANGE OF STRATA. CLEAN TO END OF CASING AND TAKE ALL SAMPLES "DRY" WITH SAMPLER BELOW END OF CASING. DO NOT DRIVE THE SAMPLER FARTHER THAN ITS INSIDE LENGTH WITHOUT CLEANING. LOCATION OF LAYER BOUNDARIES MUST BE SHOWN IN "CROSS SECTION" COLUMN. SAMPLES SHOULD BE VISUALLY IDENTIFIED. MOISTURE CONTENT SHOULD BE INDICATED IN "MOISTURE" COLUMN AS W-WET, M-MOIST, OR D-DRY. ANY LOSS OF WASH WATER OR UPWARD FLOW OF WATER AND MATERIAL INTO CASING SHOULD BE EMPHASIZED UNDER "REMARKS".

HOLE NO. F.C. 6

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>59</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN --DRILLER Besette				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE _____ SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24"		SAMPLER 1 3/8 140 30"		CORE BAR. _____ BIT. _____	
								Date Start 11/21 Date Fin 11/21/60 SURFACE ELEV. _____ GROUND WATER ELEV. 3.7	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
	2											2'0"	Park River
	1												
5	3												
	1		d			6'6"	1	0	2			7'0"	gray fine sand & silt mixed with black muck and rotted leaves-wood roots
	1												
	1												
10	3												
	1		d			11'6"	2	1	1			11'6"	gray red clay & silt
	2												
	3												
15	4												
	2		d			16'6"	1	1	1				red clay
	2												
	2												
	5												
20	5												
	4		d			21'6"	1	1	1				
	6												
	7												
	7												
25	7												
	12		d			26'6"	5	6	7			26'0"	
	18												
	24												
	27												
30	31												
	45		d			31'6"	4	5	5				red clay some coarse to fine gravel
	58												
	67												
	110												
35	164												
	90		d			36'6"	28	42	29				red clayey silt, some coarse to fine sand & gravel, few cobbles, cemented
	186												
	204												
	321												
40	280		d			41'6"	33	58	67				end of hole @ 41'6"

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.										HOLE NO. 59	
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST											
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%											

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>1</u> HOLE NO. <u>60</u>	
CONTRACTOR				PROJECT NO. <u>1960-3</u>				LINE	
FOREMAN -DRILLER <u>Bossette</u>				PROJECT NAME <u>Park River Conduit Ext.</u>				STATION	
INSPECTOR <u>Batterson</u>				LOCATION <u>Hartford, Conn.</u>				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE <u>2 1/2</u> SIZE I.D. <u>300</u> HAMMER WT. <u>24"</u>		SAMPLER <u>1 3/8</u> <u>140</u> <u>30"</u>		CORE BAR. Date Start <u>11/19</u> Date Fin. <u>11/21</u> SURFACE ELEV. _____ G.W. WATER ELEV. <u>31.7</u>	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
													Park River
	4											2'0"	
	2											loose	
5	2											wet	5'0"
	2		d			6'6"	2	1	2				
	1											soft	
	2											wet	
	1												
10	1		d			11'6"	1	0	0				
	2												
	3												
15	3		d			16'6"	1	1	1				
	3												
	4												
	5											20'0"	
20	5		d			21'6"	1	2	2				
	7												
	9												
	11												
25	10												red clay, little coarse to fine gravel, trace coarse to fine sand
	6		d			26'6"	2	3	3				
	8												
	13												
	11												
30	9												
	8		d			31'6"	3	4	6			firm	
	14											wet	
	27												
	33												
35	64												red clay & silt, some coarse to fine gravel, trace fine sand
	84		d			35'6"	27	36	46				
	137												
	249												
	274												
40	301		d			41'6"	32	47	53			very dense moist	same (cemented) <i>Bottom of Boring at 41'6"</i>

GROUND SURFACE TO _____ FT.				USED _____ " CASING				THEN _____ " CASING TO _____ FT.				HOLE NO. 60	
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST													
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%													

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>2</u> HOLE NO. <u>61</u>				
CONTRACTOR				PROJECT NO. 1960-3				LINE				
FOREMAN -DRILLER Bennette				PROJECT NAME Park River Conduit Ext.				STATION				
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET				
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>		SAMPLER <u>1 3/8</u> <u>140</u> <u>30</u>		CORE BAR. Date Start <u>11/25</u> Date Fin. <u>11/25/60</u> SURFACE ELEV. _____ river WATER ELEV. <u>31.7</u>				
DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6"	6-12"				
5	4										2'0"	Park River gray coarse to fine sand & gravel, boulders, debris on river bottom gray red silt, some clay
	13										loose wet 4'0"	
	14										firm wet 7'0"	
	3	1	D		6'6"	3	3	4				
	3											
10	5										soft wet	red gray clay red clay sample #4 slipped twice recovered 3rd try Samples #3 thru 7 same
	6											
	3	2	D		11'6"	2	2	1				
	5											
	4											
15	6											
	2	3	D		16'6"	1	1	1				
	2											
	4											
	7											
20	7											
	4	4	D		21'6"	w	o	h				
	3											
	3											
	3											
25	4											
	2	5	D		26'6"	w	o	h				
	4											
	7											
	7											
30	4											
	3	6	D		31'6"	1	0	0				
	7											
	4											
	4											
35	6											
	3	7	D		36'6"	2	2	2				
	8											
	10											
	10											
40	11											

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. 61
 D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>61</u>			
CONTRACTOR				PROJECT NO. 1960-3				LINE			
FOREMAN - DRILLER Bennette				PROJECT NAME Park River Conduit Ext.				STATION			
INSPECTOR Battersen				LOCATION				OFFSET			
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24		SAMPLER 1 3/8 140 30		CORE BAR. BIT. Date Start 11/25 Date Fin. 11/25/60 SURFACE ELEV. _____ WATER ELEV. 31.7 river			
DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE) 0-6 8-12 12-18	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.						DEPTH @ BOT.
12								soft wet	44'0"	red clay, little fine to coarse gravel	
13											
14											
46											
45	228	A	D		45'6"	22	23	28	very dense moist	50'0"	red sand, silt, & gravel cemented with little clay (till)
5											
50											
10											
55											
15											
20											
25											
30											
35											
40											

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. **61**
 D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON
 UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

FC 7

DISTRICT NO. _____ COUNTY _____ B.S.M. PROJ. NO. _____		GILES DRILLING CORP. 2 PARK AVENUE NEW YORK 16, N. Y. SUBSURFACE INFORMATION Sheet 1 of 2		HOLE NO. <u>7</u> LINE & STA. _____ OFFSET _____							
NAME <u>Greater Hartford Flood Commission</u>		NO. _____		QUAD. LOCATION <u>Hartford, Conn.</u> DATE, START <u>1-29-60</u> GND. ELEV. <u>47.5 M.S.L.</u>							
PED. CLASS. _____		DATE, FINISH <u>2-3-60</u>		G. W. DEPTH <u>131' 7"</u>							
CASING O.D. <u>3"</u> I.D. <u>2 1/4"</u>		WEIGHT OF HAMMER <u>300 & 140 lbs.</u>		HAMMER FALL							
SAMPLER O.D. <u>2"</u> I.D. <u>1 3/8"</u>		INSIDE LENGTH OF SAMPLER <u>20"</u>		CASING <u>24"</u> SAMPLER <u>30"</u>							
DEPTH BELOW GND. SURF	BLOWS ON CASING	SAMPLE NO.	BLOWS ON SAMPLER	CROSS SECTION	MOISTURE	COLOR	MECH. ANALYSIS				FIELD IDENTIFICATION OF SOIL & REMARKS
							% PASSING SIEVE NO.				
			0 6 12 18 24				4	10	40	200	
0	38										0' to 11' Misc. Fill Red Clay, Shale Frag. Some Cinders
	24										
	27										
	40										
	21										
	11	1	4	8	18"						
	13			9							
	8										
	10										
	17										
10	8	2	11	6	18"						11' to 23' Brown Clay
	21			4							
	28										
	23										
	27										
	21	3	8	8	13"						
	21			10							
	25										
	27										
	24										
20	14	4	2	2	18"						23' to 58' Varved Clay
	11			3							
	9										
	9										
	10										
	8	5	1	2	18"						
	10			1							
	10										
	11										
	12										
30	9	6	1	1	18"						
	9			2							
	11										
	11										
	13										
	11	7	1	2	18"						
	14			1							
	14										
	19										
	27										
40	19	8	2	1	18"						
	17			2							
	16										
	13										
	19										
	14	9	2	2	18"						
	16			2							
	18										
	21										
	23										
50											

DRILLING INSPECTOR H. D. Stalling

ASS'T SOILS ENGINEER _____

SAMPLES SHOULD BE TAKEN AT APPROXIMATELY 5 FT. INTERVALS AND WHEREVER THERE IS AN INDICATION OF POSSIBLE CHANGE OF STRATA. CLEAN TO END OF CASING AND TAKE ALL SAMPLES "DRY" WITH SAMPLER BELOW END OF CASING. DO NOT DRIVE THE SAMPLER FARTHER THAN ITS INSIDE LENGTH WITHOUT CLEANING. LOCATION OF LAYER BOUNDARIES MUST BE SHOWN IN "CROSS SECTION" COLUMN. SAMPLES SHOULD BE VISUALLY IDENTIFIED. MOISTURE CONTENT SHOULD BE INDICATED IN "MOISTURE" COLUMN AS W-WET, M-MOIST, OR D-DRY. ANY LOSS OF WASH WATER OR UPWARD FLOW OF WATER AND MATERIAL INTO CASING SHOULD BE EMPHASIZED UNDER "REMARKS".

HOLE NO. 7

DISTRICT NO. _____ COUNTY _____ B.S.M. PROJ. NO. _____		GILES DRILLING CORP. 2 PARK AVENUE NEW YORK 16, N. Y. SUBSURFACE INFORMATION Sheet 2		HOLE NO. <u>7</u> LINE & STA. _____ OFFSET _____	
NAME <u>Greater Hartford Flood Commission</u>		NO. _____		QUAD. LOCATION <u>Hartford, Conn.</u>	
PED. CLASS. _____		DATE, START _____		GND. ELEV. _____	
		DATE, FINISH _____		G. W. DEPTH _____	
CASING O.D. _____ I.D. _____		WEIGHT OF HAMMER _____		HAMMER FALL _____	
SAMPLER O.D. _____ I.D. _____		INSIDE LENGTH OF SAMPLER _____		CASING _____ SAMPLER _____	

DEPTH BELOW GND. SURF	BLOWS ON CASING	SAMPLE NO.	BLOWS ON SAMPLER						CROSS SECTION	MOISTURE	COLOR	MECH. ANALYSIS				FIELD IDENTIFICATION OF SOIL & REMARKS
												% PASSING SIEVE NO.				
			0	6	12	18	24					4	10	40	200	
0	18	10	1	2				18"								
	24				2											
	23															
	25															
	27															
	24	11	2	2				18"								
	27				2											
	53	(53	to	59	6"										
	186	(12	23	46				18"								
10	212				71											58' to 70' 6"
	312															Glacier Till
	216															
	221															
	220															
	221															
	186	13	18	22				18"								
	209				30											
	243															
	245															
20	526															
	124	14	4	19	4"			4"								
	175	(15	70	6"	to	73)										
	186	(Washed Samp.						M Br			70' 4" to 70' 6"				70' 6" to 73'	
	211										Boulder				Br. Fine to Med. Sand	
Drilled and Sirs	236															
	93	16	26	36				18"			74' 3" to 74' 5"				73' to 87' 7"	
	186				42						Boulder					
	212															
From 70'	321															Glacier Till
	386															
30	174	17	31	39				18"			79' 7" to 79' 11"					
to	268										Boulder					
87' 7"	317															

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>GREATER HFD FLOOD COMM</u>				SHEET <u>1</u> OF <u>2</u> HOLE NO. <u>62</u>	
CONTRACTOR				PROJECT NO. <u>1960-3</u>				LINE	
FOREMAN -DRILLER <u>MILLER</u>				PROJECT NAME				STATION	
INSPECTOR <u>BATTERSON</u>				LOCATION <u>HARTFORD, CONN</u>				OFFSET	
GROUND WATER OBSERVATIONS AT <u>5</u> FT. AFTER <u>24</u> HOURS AT <u>5</u> FT. AFTER <u>48</u> HOURS				CASING SAMPLER CORE BAR. TYPE SIZE I.D. <u>2 1/2</u> <u>1 1/2</u> HAMMER WT. <u>300</u> <u>140</u> BIT. HAMMER FALL <u>24</u> <u>30</u>				Date Start <u>10-27</u> Date Fin. <u>10-31</u> SURFACE ELEV. <u>40.5</u> GROUND WATER ELEV.	

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6 6-12 12-18						
1													SILT, CLAY, SAND AND CINDERS - FILL
1													
1													
1													
5													
5						18		6.5	2	2	2		
6													
8													
13													
22								11.5	9	7	6		(LOST SAMPLE AT 10.0)
10													
24													
24												12.0	
19													
15						18		16.5	3	2	2		SILT, CLAY AND FINE SAND
18													
8												17.0	
7						18		18.5	2	2	2		FINE SAND, SILT AND ORGANIC MATERIAL
7												19.0	
20						18		21.5	1	1	1		SILT AND CLAY (VARVED)
11													
6													
4													
5													
25						18		26.5	1	1	1		
9													
9													
10													
10													
30						18		31.5	1	1	1		
12													
10													
11													
11													
35						18		36.5	1	1	1		
12													
13													
14													
40													

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO.
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>GREATER MFD. FLOOD COMM</u>				SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>62</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN -DRILLER MILLER				PROJECT NAME				STATION	
INSPECTOR BATTERSON				LOCATION HARTFORD, CONN.				OFFSET	
GROUND WATER OBSERVATIONS AT <u>5</u> FT. AFTER <u>24</u> HOURS AT <u>5</u> FT. AFTER <u>48</u> HOURS				CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>		SAMPLER <u>1 1/2</u> <u>140</u> <u>30</u>		CORE BAR. BIT. Date Start <u>10-27</u> Date Fin. <u>10-31</u> SURFACE ELEV. <u>40.5</u> GROUND WATER ELEV.	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
				18		41.5	1	1	1				SILT AND CLAY (VARVED)
45				18		46.5	1	1	1				
50				18		51.5	1	2	2				
55				18		56.5	2	2	2				
60				18		61.5	2	2	2				
65				18		66.5	2	2	2				
70				18		70.5	45	52	80		69.0		
												SILT, CLAY AND GRAVEL HARDPAN	
75				0.5		75.5	200				75.5		
80													

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO.
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>3</u> HOLE NO. <u>80</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN --DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>		CASING W.1 SAMPLER SS 1 3/8 140 30		CORE BAR. BIT.	
								Date Start <u>12/2</u> Date Fin. <u>12/3/60</u> SURFACE ELEV. _____ RIVER GROUND WATER ELEV. <u>36.0</u>	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
	6												NORTH BRANCH PARK RIVER
	14												
	8												
5	4	1	D	18"	14"	6'6"	7	4	4			6'0"	DARK GRAY COARSE TO FINE SAND AND GRAVEL, ROOTS, MUCK, BOULDERS
	3												
	6												
	4												GRAY SILT & TRACE FINE SAND, SOME CLAY
	5												
10	4											10'0"	
	3												GRAY-BROWN VARVED CLAY
	3												
	4												
	3												
15	2	2	D	18"	16"	16'6"	1	2	1				
	6												
	4												
	4												
	4												
	6												
20	4												
	4												
	4												
	3												
25	3	3	D	18"	18"	26'6"	1	1	1				
	3												
	4												
	4												
30	4												
	4												
	3												
	6												
	6												
35	4	4	D	18"	16"	36'6"	1	1	2				
	7												
	7												
	7												
40	4												

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO. 80
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>2</u> OF <u>3</u> HOLE NO. <u>80</u>	
CONTRACTOR				PROJECT NO. 1980-3				LINE	
FOREMAN —DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				TYPE <u>W.I.</u> SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>				CASING <u>W.I.</u> SAMPLER <u>SS</u> CORE BAR. _____ SURFACE ELEV. _____ RIVER <u>36.0</u> GROUND WATER ELEV. _____	
DATE START <u>12/2</u> DATE FIN. <u>12/3/60</u>									

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12					12-18
45 3		5	D	18"	16"	46'6"	1	2	2	SOFT WET		BROWN GRAY VARVED CLAY	
50 10													
55 18		6	D	18"	16"	56'6"	1	2	2				
60 20													
65 28		7	D	18"	18"	66'6"	2	2	2				
70 30													
75 38		8	D	18"	18"	76'6"	2	2	3				
80 40													

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO. 80
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Com.</u>				SHEET <u>2</u> OF <u>3</u> HOLE NO. <u>80</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				TYPE SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24"		CASING W.1 SAMPLER SS 1 3/8 140 30"		CORE BAR. BIT. Date Start 12/2 Date Fin 12/3/66 SURFACE ELEV. _____ RIVER WATER ELEV. 36.0	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.	
		NO.	TYPE	PEN	REC	DEPTH @ BOT.	0-6	6-12					12-18
85'-0"										SOFT WET	92'0"	BROWN VARVED CLAY	
		9	D	18"	14"	86'6"	2	2	3				
90'-0"													
		10	D	18"	13"	95'6"	28	22	20		HARD MOIST	95'0"	BROWN SILT
95'-0"										COMPACT WET	100'0"	BROWN FINE SAND, LITTLE SILT	
		11	D	18"	15"	96'6"	7	15	21				
100'-0"													
		12	D	18"	14"	102'6"	18	16	20		HENSE MOIST	109'0"	BROWN FINE SAND, SILT, & MEDIUM TO FINE GRAVEL CEMENTED TILL
105'-0"													
		13	D	18"	13"	107'6"	23	31	37				
110'-0"		sampler refused at 109'0"										END OF HOLE AT 109'0"	
115'-0"													
120'-0"													

GROUND SURFACE TO _____ FT.	USED _____" CASING	THEN _____" CASING TO _____ FT.	HOLE NO. 80
D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.			CLIENT: <u>Greater Hartford Flood Comm.</u>			SHEET <u>1</u> OF <u>3</u> HOLE NO. <u>81</u>		
CONTRACTOR 			PROJECT NO. <u>1960-3</u>			LINE		
FOREMAN —DRILLER <u>Besette</u>			PROJECT NAME <u>Park River Conduit Ext.</u>			STATION		
INSPECTOR <u>Batterson</u>			LOCATION <u>Hartford, Conn.</u>			OFFSET		
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS			CASING TYPE <u>W.1</u> SAMPLER <u>SS</u> CORE BAR. _____ SIZE I.D. <u>2 1/2</u> <u>1 3/8</u> HAMMER WT. <u>300</u> <u>140</u> BIT. _____ HAMMER FALL <u>24"</u> <u>30"</u>			Date Start <u>12/1</u> Date Fin. <u>12/60</u> SURFACE ELEV. _____ WATER ELEV. <u>36.0</u>		

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
	12												
5	7												
	8												
	6												
	6												
10	5												
	4	1	D	18"	16"	10'0"	2	3	2				
	2												
	2												
15	2												
	1												
	2	2	D	18"	18"	16'6"	1	2	2				
	3												
20	3												
	4												
	2												
	2	3	D	18"	18"	21'6"	2	3	2				
25	4												
	6												
	9												
	8												
30	4	4	D	18"	16"	26'6"	2	3	2				
	6												
	7												
	7												
35	8												
	8												
	7												
	8												
40	8												
	6	5	D	18"	16"	36'6"	2	2	2				
	10												
	11												
	10												

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO. <u>81</u>
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST			
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%			

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.										CLIENT: Greater Hartford Flood Comm.										SHEET <u>2</u> OF <u>3</u> HOLE NO. <u>81</u>																																																	
CONTRACTOR										PROJECT NO. 1980-3										LINE																																																	
FOREMAN - DRILLER Bessette										PROJECT NAME Park River Conduit Ext.										STATION																																																	
INSPECTOR Batterson										LOCATION Hartford, Conn.										OFFSET																																																	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS										TYPE SIZE I.D. HAMMER WT. HAMMER FALL										CASING W.1 2 1/2 300 24"										SAMPLER SS 1 3/8 140 30"										CORE BAR. BIT. Date Start <u>12/1</u> Date Fin. <u>12/2/60</u> SURFACE ELEV. RIVER GROUND WATER ELEV. <u>36.0</u>																													
DEPTH CASING BLOWS PER FOOT										SAMPLE NO. TYPE PEN. REC. DEPTH @ BOT.										BLOWS PER 6" ON SAMPLER (FORCE ON TUBE) 0-6 6-12 12-18										CORING TIME PER FT. (MIN.)										DENSITY OR CONSIST.										STRATA CHANGE DEPTH										FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.									
45 50 55 60 65 70 75 80										6 D 18"16"46'6"										2 2 2										SOFT WET										BROWN GRAY VARVED CLAY																													
7 D 18"12"56'6"										2 1 2																																																											
8 D 18"16"66'6"										2 2 3																																																											
9 D 18"16"76'6"										2 3 2																																																											
GROUND SURFACE TO _____ FT.										USED _____ " CASING										THEN _____ " CASING TO _____ FT.										HOLE NO. 81																																							
D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON										UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST										PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%																																																	

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Com.				SHEET <u>3</u> OF <u>3</u> HOLE NO. <u>81</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Bessette				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Battersen				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				TYPE SIZE I.D. W.1 2 1/2" HAMMER WT. 300 HAMMER FALL 24"		SAMPLER SS 1 3/8" 140 30"		CORE BAR. Date Start 12/1 Date Fin. 12/3/60 SURFACE ELEV. _____ GROUND WATER ELEV. 36.0	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12				
108'										SOFT WET	93'0"	BROWN VARVED CLAY
		10	D	18"	16	86'6"	2	3	3			
110'												
115'										MEDIUM HARD WET	99'0"	BR. SILT, TRACE FINE SAND
		11	D	18"	14"	95'0"	7	12	18			
120'										COMPACT WET	105'0"	BR. FINE SAND, LITTLE SILT
		12	D	18"	12"	101'6"	8	14	19			
125'												
130'										VERY DENSE MOIST	114'0"	BR. FINE SAND, SILT, AND MEDIUM TO FINE GRAVEL (cemented) TILL
		13	D	18"	13"	106'6"	22	20	28			
135'												
140'										MEDIUM HARD	119'0"	RUN 1 114' to 119' RECOVERED GRAY SHALE 10" END OF HOLE 119'0"

GROUND SURFACE TO _____ FT. USED _____" CASING THEN _____" CASING TO _____ FT. HOLE NO. 81
 D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON
 UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Com.				SHEET <u>1</u> OF <u>3</u> HOLE NO. <u>82</u>			
CONTRACTOR				PROJECT NO. 1960-3				LINE			
FOREMAN - DRILLER Miller				PROJECT NAME Park River Conduit Ext.				STATION			
INSPECTOR Battersen				LOCATION Hartford, Conn.				OFFSET			
GROUND WATER OBSERVATIONS AT <u>7</u> FT. AFTER <u>24</u> HOURS AT <u>7</u> FT. AFTER <u>48</u> HOURS				TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>				CASING SAMPLER <u>1 3/8</u> CORE BAR. <u>140</u> BIT. <u>30"</u>			
				Date Start <u>11/15</u> Date End <u>11/17/60</u>				SURFACE ELEV. <u>39.3</u> GROUND WATER ELEV. _____			

DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.					
	8									
	10									
	15									
	10									
5	12					4' to 5' 6"	2 2 2			cinders, sand
	14									
	12									
	10									
	10									
10	15								9' 0"	
	12									fine to medium sand, silt, some decayed material
	10									
	8									
	9									
	6									
15	5					15' to 16' 6"	1 1 1		14' 0"	
	6									silt, clay, little fine sand.
	5									
	6									
	6									
20	8									
	7									
	8									
	10									
	10									
25	12									
	10									
	12									
	13									
	18									
30	20					30' to 31' 6"	1 1 1			
	18									
	14									
	16									
	19									
35	19									
	22									
	19									
	22									
	19									
40	22									

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT.				HOLE NO. 82
D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST				
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%				

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Com.				SHEET <u>2</u> OF <u>3</u> HOLE NO. <u>82</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME Park River Conduit Ext.				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING SAMPLER CORE BAR. TYPE SIZE I.D. 2 1/2 1 3/8 HAMMER WT. 300 140 BIT. HAMMER FALL 24" 30"				Date Start _____ Date Fin. _____ SURFACE ELEV. 39.3 GROUND WATER ELEV. _____	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, STRAINS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
17													
14													
13													
14													
12						45' to							
14		SS				46' 6"	1	1	1				
12													
14													
13													
14													
15													
14													
13													
13													
15													
15													
14													
14													
16													
18						60' to							
19		SS				65' 6"	1	1	1				
19													
20													
22													
22													
22													
21													
20						70' to							
27						71' 6"	6	4	6				fine sand, silt
28													
31													
29													
32						74' to	28	33	36				
54						75' 6"							medium to coarse sand, some silt, gravel, cobbles
58													
51													
36													
34						80' to	24	39	32				
81' 6"													

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. 82
 D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.		CLIENT: Greater Hartford Flood Comm.		SHEET 3 OF 3 HOLE NO. 82						
CONTRACTOR		PROJECT NO. 1960-3		LINE						
FOREMAN —DRILLER Miller		PROJECT NAME Park River Conduit Ext.		STATION						
INSPECTOR Batterson		LOCATION Hartford, Conn.		OFFSET						
GROUND WATER OBSERVATIONS AT 7' FT. AFTER 24 HOURS AT 7' FT. AFTER 48 HOURS		CASING TYPE SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24"		SAMPLER CORE BAR. 1 3/8 140 30"						
				Date Start 11/15 Date Fin. 11/17/60 SURFACE ELEV. 39.3 GROUND WATER ELEV. _____						
DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.					
85	47									
	49									
	56									
	71									
	72					85' to				
90	68		SS			86' 6"	49	54	56	87' 0"
	52									
	51					87' to				
	53					88' 6"	31	38		
	57					90' to				medium to fine sand and silt
95	48					91' 6"	12	28	39	
	47									
	61									
	58									
	73		V			95' to 96' 6"				94' 6"
100										medium sand, some silt, gravel, cobbles
110										110' 0"
115										15
										20
										20
										18
										20
120										20
GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT.										HOLE NO. 82
D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%										

DISTRICT NO. _____
COUNTY _____
B.S.M. PROJ. NO. _____

OKLES DRILLING CORP.
2 PARK AVENUE
NEW YORK 16, N. Y.
SUBSURFACE INFORMATION
Sheet One of Three

HOLE NO. 2.0.9
LINE & STA. _____
OFFSET _____

NAME Greater Hartford Flood Commission NO. _____
QUAD. LOCATION Hartford, Conn. DATE, START 2/2/60 GND. ELEV. 33.0 M.S.L.
PED. CLASS. _____ DATE, FINISH 2/4/60 G. W. DEPTH 110'

CASING O.D. 3" I.D. 2 1/2" WEIGHT OF HAMMER 300 & 140 lbs. HAMMER FALL _____
SAMPLER O.D. 2" I.D. 1-3/8" INSIDE LENGTH OF SAMPLER 20" CASING 24" SAMPLER 30"

DEPTH BELOW GND. SURF	BLOWS ON CASING	SAMPLE NO.	BLOWS ON SAMPLER					CROSS SECTION	MOISTURE	COLOR	MECH. ANALYSIS				FIELD IDENTIFICATION OF SOIL & REMARKS
			0	4	12	18	24				% PASSING SIEVE NO.				
											4	10	40	200	
0	3	1	10	2	16										Brown fine sand, some silt 0'0" - 5'0"
	3	1	1	2											
	9				3	14	Rec.								
	8						M		BROWN						
	7		5'0"	6'6"											
	3	2	1	2											Brown Silt, some clay, with fine sand layers 5' - 24'0"
	4				2	12	Rec.								
	4														
	4														
-10	5		10'0"	11'6"											
	4	3	1	1											
	4				1	18	Rec.								
	4														
	4														
	4		15'0"	16'6"											
	3	4	1	1											Reddish Brown Silt, Some Clay 24'0" - 59'0"
	4				1	18	Rec.								
	5						M		BROWN						
	6		20'0"	21'6"											
-20	4	5	1	1											
	5				1	18	Rec.								
	5														
	6														
	6		25'0"	26'6"											
	6	6	1	1											
	6				1	18	Rec.								
	7														
	8														
-30	9		30'0"	31'6"											
	6	7	1	1											
	7				1	18	Rec.								
	8														
	8						M		REDDISH BROWN						
	9		35'0"	36'6"											
	7	8	1	1											
	8				1	18	Rec.								
	9														
	9														
-40	10		40'0"	41'6"											
	8	9	1	1											
	10				1	18	Rec.								
	10														
	11														
	12		45'	46'6"											
	11	10	1	1											
	12				2	18	Rec.								
	13														
	13														
50	14														

DRILLING INSPECTOR H. D. STUBING ASS'T SOILS ENGINEER _____

SAMPLES SHOULD BE TAKEN AT APPROXIMATELY 5 FT. INTERVALS AND WHEREVER THERE IS AN INDICATION OF POSSIBLE CHANGE OF STRATA. CLEAN TO END OF CASING AND TAKE ALL SAMPLES "DRY" WITH SAMPLER BELOW END OF CASING. DO NOT DRIVE THE SAMPLER FARTHER THAN ITS INSIDE LENGTH WITHOUT CLEANING. LOCATION OF LAYER BOUNDARIES MUST BE SHOWN IN "CROSS SECTION" COLUMN. SAMPLES SHOULD BE VISUALLY IDENTIFIED. MOISTURE CONTENT SHOULD BE INDICATED IN "MOISTURE" COLUMN AS W-WET, M-MOIST, OR D-DRY. ANY LOSS OF WASH WATER OR UPWARD FLOW OF WATER AND MATERIAL INTO CASING SHOULD BE EMPHASIZED UNDER "REMARKS".

HOLE NO. 2.0.9

DISTRICT NO. _____ COUNTY _____ B.S.M. PROJ. NO. _____	GILES DRILLING CORP. 2 PARK AVENUE NEW YORK 16, N. Y. SUBSURFACE INFORMATION Sheet Two of Three	HOLE NO. <u>F.C. 9</u> LINE & STA. _____ OFFSET _____
NAME <u>Greater Hartford Flood Commission</u> NO. _____ QUAD. LOCATION <u>Hartford, Conn.</u> START _____ GND. ELEV. _____ PED. CLASS. _____ DATE, FINISH _____ G. W. DEPTH _____		
CASING O.D. _____ I.D. _____ SAMPLER O.D. _____ I.D. _____		WEIGHT OF HAMMER _____ INSIDE LENGTH OF SAMPLER _____
HAMMER FALL _____ CASING _____ SAMPLER _____		

DEPTH BELOW GND. SURF.	BLOWS ON CASING	SAMPLE NO.	BLOWS ON SAMPLER					CROSS SECTION	MOISTURE	COLOR	MECH. ANALYSIS				FIELD IDENTIFICATION OF SOIL & REMARKS
											% PASSING SIEVE NO.				
			0	6	12	18	24				4	10	40	200	
0	10	11	1	2											Reddish Brown Silt, Some Clay 55'0" - 56'6"
	13				2	18"	Rec.								
	14														
	15														
	16	55'0"			56'6"		M	REDDISH BROWN							
	16	12	1	2											
	18				2	18"	Rec.								
	21														
	23														
-10	26	60'0"			61'6"										Reddish Brown Silt, Trace of Very Fine Sand 59'0" - 68'0"
	27	13	2	3											
	39				4	18"	Rec.								
	41														
	27						M	REDDISH BROWN							
	36	65'0"			66'6"										
	29	14	3	4											
	36														
	37														
	42														
-20	43	70'0"			71'6"										Reddish Brown c/f sand, Some Silt, Trace of Gravel 68'0" - 95'0"
	36	15	6	8											
	34				11	12"	Rec.								
	41														
	38														
	42	75'0"			76'6"										
	37	16	6	10											
	39				14	13"	Rec.								
	41														
	42														
-30	48	80'0"			81'6"										Notes: Over-flow of water at 85'. Ran for 1/2 hour while out to lunch. Stopped when drove next pipe
	47	17	11	13											
	49				13	12"	Rec.								
	50														
	55						M	REDDISH BROWN							
	59	85'0"			86'6"										
	49	18	11	12											
	58				14	12"	Rec.								
	71														
	78														
-40	96	90'0"			91'6"										REDDISH Brown Fine Sand, A Little Silt
	54	19	33	24											
	86				36	14"	Rec.								
	197														
	201														
	254	95'0"			96'6"										
	69	20	17	21											
	75				29	15"	Rec.								
	92														
	95						M	REDDISH BROWN							
50	124														

DRILLING INSPECTOR _____	ASS'T SOILS ENGINEER _____
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SAMPLES SHOULD BE TAKEN AT APPROXIMATELY 5 FT. INTERVALS AND WHEREVER THERE IS AN INDICATION OF POSSIBLE CHANGE OF STRATA. CLEAN TO END OF CASING AND TAKE ALL SAMPLES "DRY" WITH SAMPLER BELOW END OF CASING. DO NOT DRIVE THE SAMPLER FARTHER THAN ITS INSIDE LENGTH WITHOUT CLEANING. LOCATION OF LAYER BOUNDARIES MUST BE SHOWN IN "CROSS SECTION" COLUMN. SAMPLES SHOULD BE VISUALLY IDENTIFIED. MOISTURE CONTENT SHOULD BE INDICATED IN "MOISTURE" COLUMN AS W-WET, M-MOIST, OR D-DRY. ANY LOSS OF WASH WATER OR UPWARD FLOW OF WATER AND MATERIAL INTO CASING SHOULD BE EMPHASIZED UNDER "REMARKS".

HOLE NO. <u>F.C. 9</u>

Form No. 15

[illegible]

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hartford Flood Comm.				SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>83</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING SAMPLER CORE BAR. TYPE _____ SIZE I.D. _____ HAMMER WT. _____ BIT. HAMMER FALL _____				Date Start <u>11/14</u> Date Fin <u>11/15/60</u> SURFACE ELEV. <u>40.7</u> GROUND WATER ELEV. _____	

DEPTH DOWN	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT	0-6	6-12				
45						45' to 46' 6"	2	2	2			silt and clay
50												
55												
60						60' to 60' 6"	3				60' 0"	
						60' 6" to 61' 6"	4	8				fine sand, silt
65						64' to 65' 6"	37	39	28		64' 0"	
70						70' to 71' 6"	41	38	58			medium to coarse sand, silt, gravel, cobbles
75						75' to 76' 6"	48	52	49			
80						80' to 81' 6"	51	72	56		81' 6"	

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT.

D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON
 US = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

HOLE NO. **83**

ENGINEERING SERVICES INC. 2848 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>1</u> OF <u>3</u> HOLE NO. <u>84</u>				
CONTRACTOR				PROJECT NO. 1960-3				LINE				
FOREMAN -DRILLER Miller				PROJECT NAME				STATION				
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET				
GROUND WATER OBSERVATIONS AT <u>25</u> FT. AFTER <u>24</u> HOURS AT _____ FT. AFTER _____ HOURS				CASING SAMPLER CORE BAR. TYPE SIZE I.D. <u>2 1/2</u> <u>1 3/8</u> HAMMER WT. <u>300</u> <u>140</u> HAMMER FALL <u>24"</u> <u>30"</u> BIT.				Date Start <u>11/11</u> Date Fin. <u>11/14/80</u> SURFACE ELEV. <u>44.6</u> GROUND WATER ELEV. <u>41.6</u>				
DEPTH	CASING BLOWS PER FOOT	SAMPLE				BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18	MOIST.	ELEV.	
	16											
	25											
	22											
	24											
5	21					4'to						
	22					5'6"	8	12	15			
	24											
	24											
	23											
10	22					10'to						
						11'6"	3	3	3			
15						15'to						
						16'6"	2	2	2			
20						20'to						
						21'6"	1	1	2			
25												
30												
35						35'to						
						36'6"	1	2	1			
40												

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. **84**
 D= DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST
 PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>2</u> OF <u>3</u> HOLE NO. <u>84</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT <u>25</u> FT. AFTER <u>24</u> HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. <u>2 1/2</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24"</u>		SAMPLER <u>1 3/8</u> <u>140</u> <u>30"</u>		CORE BAR. _____ BIT. _____	
				Date Start <u>11/11</u> Date Fin <u>11/14/60</u>		SURFACE ELEV. <u>44.6</u>		GROUND WATER ELEV. <u>44.6</u>	

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 8" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-8	8-12	12-16				
45													
50					50' to 51'6"	1	1	1					
55													
60													
63					63' to 64'6"	4	8	9			63'0"		
65					64'6" to 66'	12	16	18			64'6"		fine sand, silt
67					67' to 68'6"	18	32	36					medium to coarse sand, silt, and gravel
70													
75					75' to 76'6"	38	36	53					
80					80' to 81'6"	37	54	39					

GROUND SURFACE TO _____ FT.	USED _____ CASING	THEN _____ CASING	TO _____ FT.	HOLE NO. 84
D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST				
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%				

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.										CLIENT: Greater Hartford Flood Com.										SHEET <u>3</u> OF <u>3</u> HOLE NO. <u>84</u>																			
CONTRACTOR										PROJECT NO. 1960-3										LINE																			
FOREMAN —DRILLER Miller										PROJECT NAME										STATION																			
INSPECTOR Batterson										LOCATION Hartford, Conn.										OFFSET																			
GROUND WATER OBSERVATIONS AT <u>25</u> FT. AFTER <u>24</u> HOURS AT _____ FT. AFTER _____ HOURS										CASING TYPE SIZE I.D. 2 1/2 HAMMER WT. 300 HAMMER FALL 24"										SAMPLER 1 3/8 140 30"										CORE BAR. BIT. Date Start <u>11/11</u> Date Fin. <u>11/14/60</u> SURFACE ELEV. <u>44.6</u> GROUND WATER ELEV. <u>44.6</u>									
DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.																										
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18																														
85													medium to coarse sand, silt, and gravel 88'6"																										
90													bottom of boring																										
100																																							
105																																							
110																																							
115																																							
120																																							

GROUND SURFACE TO _____ FT. USED _____ " CASING THEN _____ " CASING TO _____ FT.

HOLE NO. **84**

D=DRY W= WASHED C= CORED P= PIT A= AUGER UP= UNDISTURBED PISTON
 UB= UNDISTURBED BALL CHECK T= THINWALL V= VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

DISTRICT NO. _____
COUNTY _____
B.S.M. PROJ. NO. _____

GILES DRILLING CORP.
2 PARK AVENUE
NEW YORK 16, N. Y.
SUBSURFACE INFORMATION
Sheet One of Two

HOLE NO. F. C. 10
LINE & STA. _____
OFFSET _____

NAME Greater Hartford Flood Commission

NO. _____

QUAD. LOCATION Hartford, Conn.

DATE, START 2/2/60

GND. ELEV. 38.2 M.S.L.

PED. CLASS. _____

DATE, FINISH 2/4/60

G. W. DEPTH 10.4

CASING O.D. 3" I.D. 2 1/2"
SAMPLER O.D. 2 1/2" I.D. 1 3/4"

WEIGHT OF HAMMER 300 & 140 lbs.
INSIDE LENGTH OF SAMPLER 20"

HAMMER FALL _____
CASING _____ SAMPLER _____

DEPTH BELOW GND. SURF	BLOWS ON CASING	SAMPLE NO.	BLOWS ON SAMPLER					CROSS SECTION	MOISTURE	COLOR	MECH. ANALYSIS				FIELD IDENTIFICATION OF SOIL & REMARKS
											% PASSING SIEVE NO.				
			0	6	12	18	24				4	10	40	200	
0	1														Gray Silty Clay 1'0" - 10' 0"
	4	1	1	2											
	3				6	17	Rec.								
	4														
	3	2	2	3											
	9				3	18	Rec.								Gray Clay 10'0" - 30'0"
	7														
10	10														
	12	3	1	1		18	Rec.								
	14				1										
	18									GRAY					
	18														
	12	4	1	2											
	13				1	18	Rec.								
	12														
20	10														Red Gray Clay 30'0" - 50'0"
	10	5	1	1											
	11				1	18	Rec.								
	16														
	13														
	13														
	16	6	0	1											
	17				1	18	Rec.								
	16														
	15														
30	17														RED & GRAY
	14	7	0	1											
	17				1	18	Rec.								
	16														
	14														
	15														
	18	8	1	1											
	22				1	18	Rec.								
	19														
	17														
40	19														
	18	9	1	2											
	20				1	14	Rec.								
	21														
	23														
	23														
	20	10	1	2											
	23				2	16	Rec.								
	21														
	23														
50	25														

DRILLING INSPECTOR H. D. TUBING ASS'T SOILS ENGINEER _____

SAMPLES SHOULD BE TAKEN AT APPROXIMATELY 5 FT. INTERVALS AND WHEREVER THERE IS AN INDICATION OF POSSIBLE CHANGE OF STRATA. CLEAN TO END OF CASING AND TAKE ALL SAMPLES "DRY" WITH SAMPLER BELOW END OF CASING. DO NOT DRIVE THE SAMPLER FARTHER THAN ITS INSIDE LENGTH WITHOUT CLEANING. LOCATION OF LAYER BOUNDARIES MUST BE SHOWN IN "CROSS SECTION" COLUMN. SAMPLES SHOULD BE VISUALLY IDENTIFIED. MOISTURE CONTENT SHOULD BE INDICATED IN "MOISTURE" COLUMN AS W-WET, M-MOIST, OR D-DRY. ANY LOSS OF WASH WATER OR UPWARD FLOW OF WATER AND MATERIAL INTO CASING SHOULD BE EMPHASIZED UNDER "REMARKS".

HOLE NO. F. C. 10

DISTRICT NO. _____ COUNTY _____ B.S.M. PROJ. NO. _____		GILES DRILLING CORP. 2 PARK AVENUE NEW YORK 14, N. Y. SURFACE INFORMATION Sheet Two of Two		HOLE NO. <u>F. C. 10</u> LINE & STA. _____ OFFSET _____	
NAME <u>Greater Hartford Flood Commission</u>				NO. _____	
QUAD. LOCATION <u>Hartford, Conn.</u>		DATE, START <u>2/2/60</u>		GND. ELEV. _____	
PED. CLASS. _____		DATE, FINISH <u>2/4/60</u>		G. W. DEPTH _____	
CASING O.D. _____ I.D. _____ SAMPLER O.D. _____ I.D. _____		WEIGHT OF HAMMER _____ INSIDE LENGTH OF SAMPLER _____		HAMMER FALL _____ CASING _____ SAMPLER _____	

DEPTH FEET BELOW GND. SURF.	BLOWS ON CASING	SAMPLE NO.	BLOWS ON SAMPLER								CROSS SECTION	MOISTURE	COLOR	MECH. ANALYSIS				FIELD IDENTIFICATION OF SOIL & REMARKS
														% PASSING SIEVE NO.				
			0	6	12	18	24	30	36	42				4	10	40	200	
0	25	11	2	3													Brown Sand, Gravel	
	26							2	18"	Rec.							50'0" - 84'4"	
	28																	
	37																	
	41																	
	47	12	Missed														Missed Sample #12	
	20																	
	18																	
	23																Sample #13 Wash Sample	
	24																	
10	31	13	47	10														
	37							10										
	41									X		RED						
	39																	
	42																	
	38	14	78						16"	Rec.								
	38	14		18	20													
	41																	
	46																	
20	51																	
	44	15	24	18					18"	Rec.								
	47																	
	43																	
	49																	
	50																	
	47	16	41	34					14"	Rec.								
	41																	
	52																	
	53																	
30	44																	
	46	17	31	42					15"	Rec.								
	45																	

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: Greater Hfd. Flood Comm.				SHEET <u>1</u> OF <u>2</u> HOLE NO. <u>85</u>	
CONTRACTOR				PROJECT NO. 1980-3				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT <u>2'</u> FT. AFTER <u>24</u> HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE SIZE I.D. <u>4"</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>		SAMPLER CORE BAR. <u>1 3/8</u> <u>140</u> <u>30</u>		Date Start <u>11/16/80</u> Date Fin. <u>11/22/80</u> SURFACE ELEV. <u>36.0</u> GROUND WATER ELEV. <u>28.00</u>	

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18		MOIST	ELEV.	
	8												
	12												
	10												
	12												
5	10					5'to							
	12		SS			6'6"	1	2	1				fine sand , silt, some organic material
	10												
	12												
	12												
10	10					10'to							
	12					11'6"	3	2	2			12'0"	
	12												
	10					12'to							
	9					13'6"	1	1	1				
15	10					15'to							
	12					16'6"	1	1	1				clay, silt, trace fine sand
	14												
	16												
	16												
20	18					20'to							
	17					21'	1	1	1			21'0"	
	16												SHELBY
	16											23'0"	
	16												
25	18												
30												30'0"	
													SHELBY
												32'0"	
40		SS				38'6"	/	/	/				
						40'0"							

GROUND SURFACE TO _____ FT., USED _____ " CASING THEN _____ " CASING TO _____ FT. HOLE NO. **85**

D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON
UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Htfd. Flood Comm.</u>				SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>85</u>	
CONTRACTOR				PROJECT NO. 1960-3				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME				STATION	
INSPECTOR Batterson				LOCATION Hartford, Conn.				OFFSET	
GROUND WATER OBSERVATIONS AT _____ FT. AFTER _____ HOURS AT _____ FT. AFTER _____ HOURS				CASING TYPE <u>4"</u> SIZE I.D. <u>1 3/8</u> HAMMER WT. <u>300</u> HAMMER FALL <u>24</u>				SAMPLER <u>140</u> CORE BAR. <u>30</u> BIT.	
DATE START <u>11/16</u> DATE FIN <u>11/22/60</u> SURFACE ELEV. <u>32.0</u> GROUND WATER ELEV. _____									

DEPTH	CASING BLOWS PER FOOT	SAMPLE					DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)	CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS (INCL. COLOR, LOSS OF WASH WATER, SEAMS IN ROCK, ETC.)		
		NO.	TYPE	PEN.	REC.	0-6							6-12	12-18
												42'0" S H E L B Y		
45												Clay and Silt		
50														
55														
60														
61							60'to 61'6"	17	18	17			60'0"	
65							65'to 66'6"	28	39	41			Fine to Medium Sand, Silt, and Gravel	
70							70'to 71'6"	21	20	24				
75							74'6" to 75'							75'0"
76										70				n Rock, Shale (red) 5'6" run; recovery 3'2"
77										15				
78										10				
80										10		80'6"		
81										10		Bottom of boring		

GROUND SURFACE TO _____ FT.	USED _____ " CASING	5	THEN _____ " CASING TO _____ FT.	HOLE NO. 85
-----------------------------	---------------------	---	----------------------------------	-------------

D: DRY W: WASHED C: CORED P: PIT A: AUGER UP: UNDISTURBED PISTON
 UB: UNDISTURBED BALL CHECK T: THINWALL V: VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-60%

ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.										CLIENT: Greater Hartford Flood Contr.										SHEET <u>1</u> OF <u>2</u> HOLE NO. <u>86</u>																			
CONTRACTOR										PROJECT NO.										LINE																			
FOREMAN --DRILLER										PROJECT NAME										STATION																			
INSPECTOR										LOCATION										OFFSET																			
GROUND WATER OBSERVATIONS										CASING										SAMPLER										CORE BAR.									
AT _____ FT. AFTER _____ HOURS										TYPE										DATE START <u>11/22</u> DATE FIN. <u>11/25/60</u>																			
AT <u>4'6"</u> FT. AFTER <u>48</u> HOURS										SIZE I.D. <u>2 1/2</u>										SURFACE ELEV. <u>37.00</u>																			
										HAMMER WT. <u>300</u>										GROUND WATER ELEV. <u>32.5</u>																			
										HAMMER FALL <u>24</u>										BIT.																			

DEPTH	CASING BLOWS PER FOOT	SAMPLE				DEPTH @ BOT.	BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST.	STRATA CHANGE DEPTH	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.		0-6	6-12	12-18				
10												loam, organic material, fine to medium sand, silt	
12													
12													
12													
10					5'to								
13		SS			6'6"	2	2	2					
18													
29													
30													
10		SS			10'	1	1						
31					to 11'						11'0"		
28					11'to	1						clay, silt, trace fine sand	
29					11'6"								
31													
30					15'to								
20		SS			16'6"	1	1	1					
19											17'0"		
14													
14											19'0"	shelby	
20													
13													
12													
14													
14													
25		SS			25'to								
12					26'6"	1	1	1					
											27'0"		
											29'0"	shelby	
30													
35													
40													

GROUND SURFACE TO _____ FT.										USED _____ " CASING										THEN _____ " CASING TO _____ FT.										HOLE NO. 86																													
D = DRY										W = WASHED										C = CORED										P = PIT										A = AUGER										UP = UNDISTURBED PISTON									
UB = UNDISTURBED BALL CHECK										T = THINWALL										V = VANE TEST																																							
PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%																																																											

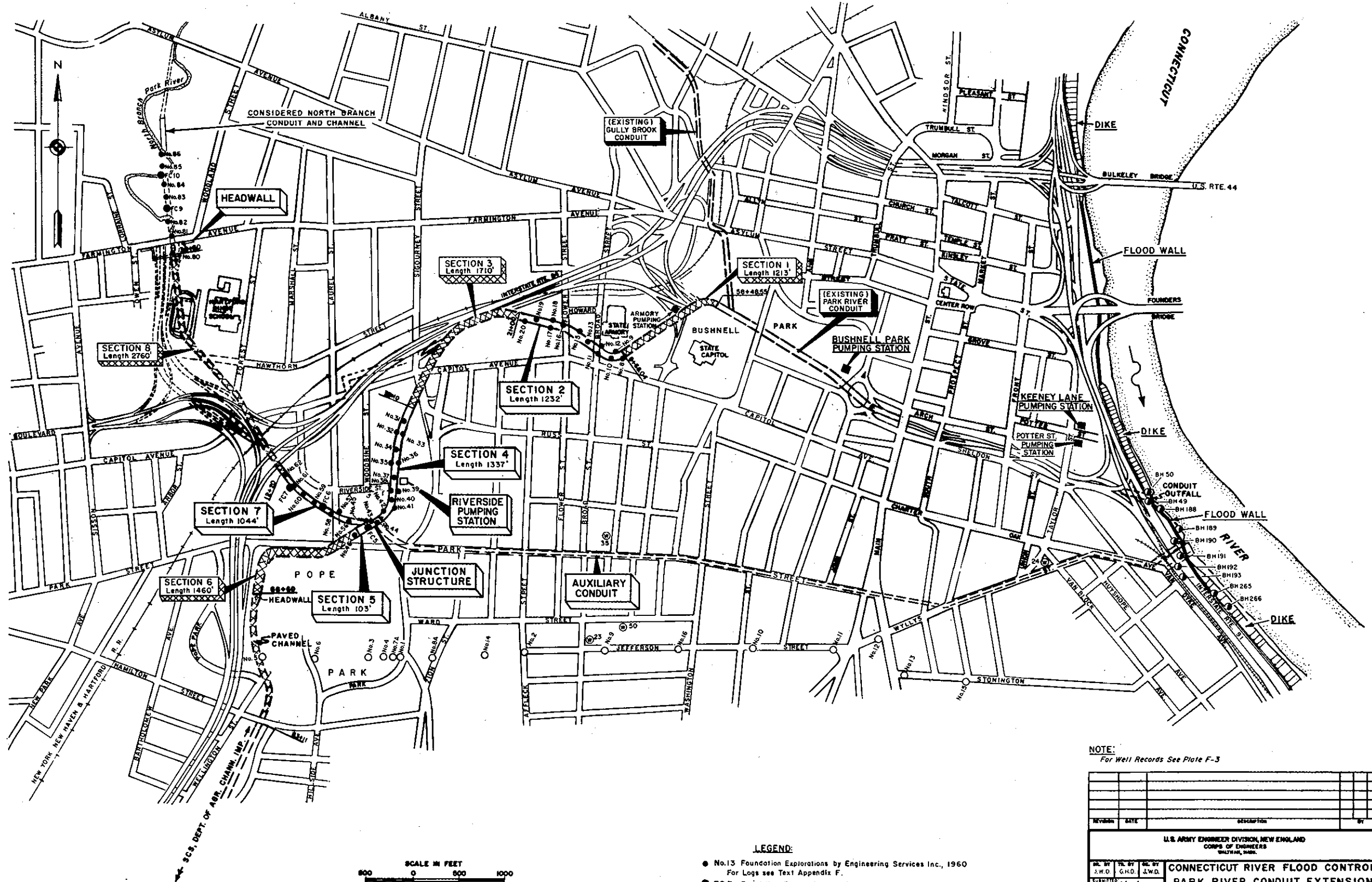
ENGINEERING SERVICES INC. 2846 MAIN STREET GLASTONBURY, CONN.				CLIENT: <u>Greater Hartford Flood Comm.</u>				SHEET <u>2</u> OF <u>2</u> HOLE NO. <u>86</u>	
CONTRACTOR				PROJECT NO.				LINE	
FOREMAN - DRILLER Miller				PROJECT NAME 1960-3				STATION	
INSPECTOR Batterson				LOCATION Park River Conduit Ext.				OFFSET	
GROUND WATER OBSERVATIONS				CASING SAMPLER CORE BAR.				Date Start <u>11/25</u> Date Fin <u>11/25/60</u>	
AT _____ FT. AFTER _____ HOURS				TYPE SIZE I.D. <u>2 1/2</u> <u>13 3/8</u>				SURFACE ELEV. <u>37.0</u>	
AT _____ FT. AFTER _____ HOURS				HAMMER WT. <u>300</u> <u>140</u> BIT.				GROUND WATER ELEV. <u>32.5</u>	
HAMMER FALL <u>24</u> <u>30</u>									

DEPTH	CASING BLOWS PER FOOT	SAMPLE					BLOWS PER 6" ON SAMPLER (FORCE ON TUBE)			CORING TIME PER FT. (MIN.)	DENSITY OR CONSIST. MOIST.	STRATA CHANGE DEPTH ELEV.	FIELD IDENTIFICATION OF SOIL. REMARKS INCL. COLOR, LOSS OF WASH WATER, BEAMS IN ROCK, ETC.
		NO.	TYPE	PEN.	REC.	DEPTH @ BOT.	0-6	6-12	12-18				
45													
50												49'0"	
55													
60													
65													
70													
75													
80												82'0"	

GROUND SURFACE TO _____ FT.	USED _____ " CASING	THEN _____ " CASING TO _____ FT.	HOLE NO. 86
-----------------------------	---------------------	----------------------------------	-------------

D = DRY W = WASHED C = CORED P = PIT A = AUGER UP = UNDISTURBED PISTON
 UB = UNDISTURBED BALL CHECK T = THINWALL V = VANE TEST

PROPORTIONS USED: TRACE = 0-10%, LITTLE = 10-20%, SOME = 20-35%, AND = 35-50%



NOTE:
For Well Records See Plate F-3

- LEGEND:**
- No. 13 Foundation Explorations by Engineering Services Inc., 1960
For Logs see Text Appendix F.
 - FC 7 Foundation Explorations by Giles Drilling Corp., 1960
For Logs see Text Appendix F.
 - No. 16 Foundation Explorations by Philip J. Hedy Inc., 1934
For Logs see Plate F-3.
 - ① 8H189 Foundation Explorations by Providence District,
Army Engineers 1940 For Logs see Plate F-3.
 - ⑤ 50 Wells, Connecticut Water Resources Bulletin No. 4, 1964
"Records and Logs of Selected Wells and Test Borings."

REVISION	DATE	DESCRIPTION	BY

U.S. ARMY ENGINEER DIVISION, NEW ENGLAND
CORPS OF ENGINEERS
WALTHAM, MASS.

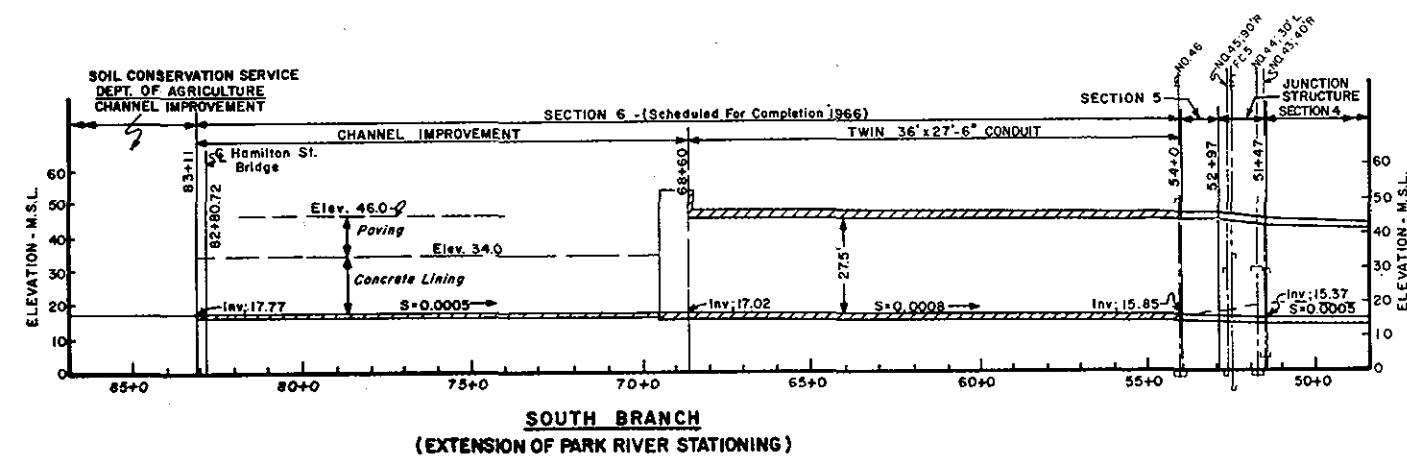
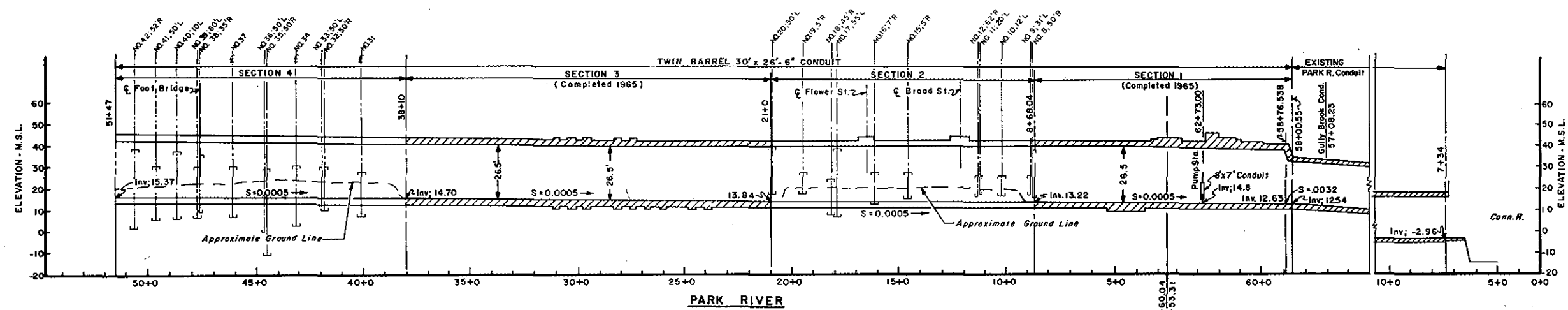
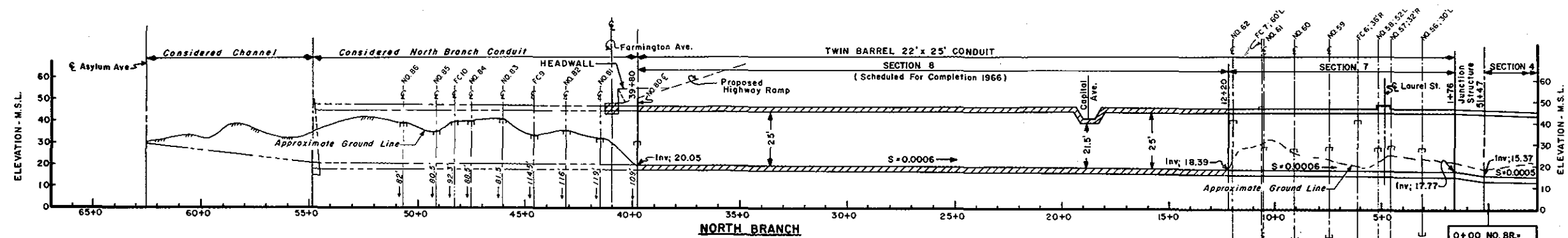
**CONNECTICUT RIVER FLOOD CONTROL
PARK RIVER CONDUIT EXTENSION
AND AUXILIARY CONDUIT
PLAN OF EXPLORATIONS**

PARK RIVER, CONNECTICUT

APPROVED: *John W. Sullivan* DATE: JULY 1966
CHIEF ENGINEER DISTRICT

TO ACCOMPANY REPORT
DATED 21 JULY 1966

SCALE AS SHOWN
DRAWING NUMBER
SHEET 1 OF 4

**LEGEND:**

No. 6. Foundation Exploration by Engineering Services Inc.
FC 7. Foundation Exploration by Giles Drilling Corp.

Top of Boring.
Bottom of Boring.

NOTE:

For Logs of Exploration see attached sheets.
For Location of Profiles see Plan of Exploration, Plate F-1.

REVISION	DATE	DESCRIPTION	BY

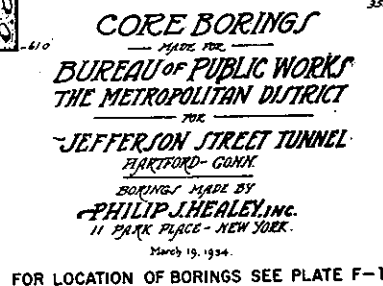
U.S. ARMY ENGINEER DIVISION, NEW ENGLAND
CORPS OF ENGINEERS
WALTHAM, MASS.

**CONNECTICUT RIVER FLOOD CONTROL
PARK RIVER CONDUIT EXTENSION
PROFILES**

PARK RIVER, CONNECTICUT
DATE: JULY 1966

TO ACCOMPANY REPORT
DATED: 21, JULY 1966

SCALE: AS SHOWN
DRAWING NUMBER
SHEET 2 OF 4



- 1 Graded from Gravel to Coarse Sand - Contains little medium sand
- 2 Coarse to Medium Sand - Contains little gravel and fine sand
- 3 Graded from Gravel to Medium Sand - Contains little fine sand
- 4 Medium to Fine Sand - Contains little coarse sand and coarse silt
- 5 Graded from Gravel to Fine Sand - Contains little coarse silt.
- 6 Fine Sand to Coarse Silt - Contains little medium sand and medium silt.
- 7 Graded from Gravel to Coarse Silt - Contains little medium silt.
- 8 Coarse to Medium Silt - Contains little fine sand and fine silt.
- 9 Graded from Gravel to Medium Silt - Contains little fine silt.
- 10 Medium to Fine Silt - Contains little coarse silt and coarse sand. Possesses behavior characteristics of silt.
- 11 Medium Silt to Coarse Clay - Contains little coarse silt and medium clay. Possesses behavior characteristics of clay.
- 12 Graded from Gravel or Coarse Sand to Fine Silt - Contains little coarse clay.
- 13 Fine Silt to Clay - Contains little medium silt and fine clay (colloids). Possesses behavior characteristics of silt.
- 14 Clay - Contains little silt. Possesses behavior characteristics of clay.

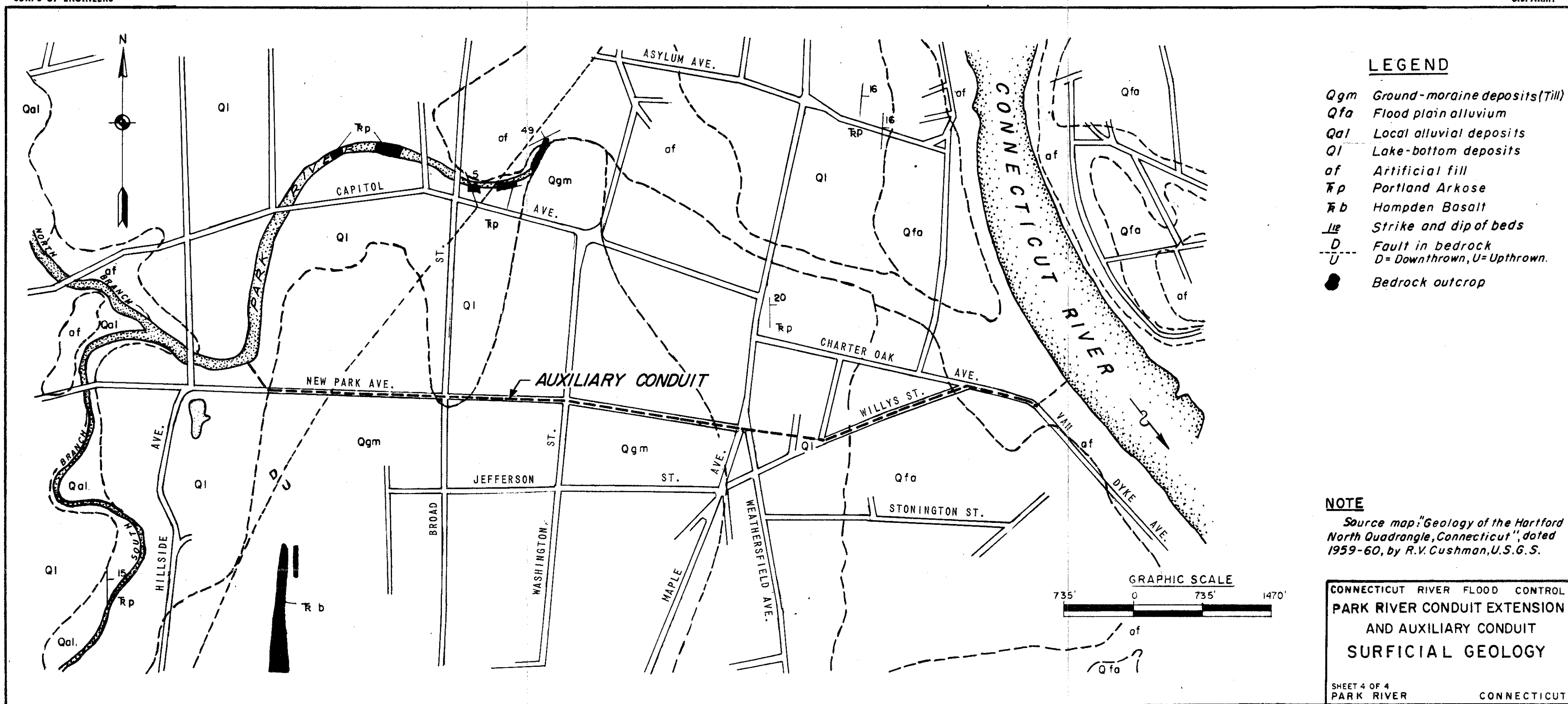
Compactness was determined by the number of blows required to drive 2" O.D. sample spoon one foot with 300 pound hammer dropped 18".

Class 12G indicated in bore hole records, generally occurs in alternating bands, having thin layers of fine clay interbedded with thicker layers of coarse to fine silt.

FOR LOCATION OF WELLS SEE PLATE F-1

Logs for other boring Located on Plate F-1 are included on separate sheets at the end of this appendix.

[illegible]



APPENDIX G

LETTERS OF COMMENT

APPENDIX G
LETTERS OF COMMENT

INDEX

<u>Exhibit No.</u>	<u>Agency</u>	<u>Letter dated</u>
G-1	Soil Conservation Service, U.S.D.A.	21 December 1965
G-2	Department of Health, Education, and Welfare	27 December 1965
G-3	Fish and Wildlife Service, U.S.D.I.	7 December 1964
G-4	Water Resources Commission	10 January 1966
G-5	The Metropolitan District	18 March 1966
G-6	The Metropolitan District	15 December 1964
G-7	Greater Hartford Flood Commission	18 April 1966

UNITED STATES DEPARTMENT OF AGRICULTURE

SOIL CONSERVATION SERVICE

Old Bookstore Building
Storrs, Connecticut 06268

December 21, 1965

Mr. John Wm. Leslie
Chief, Engineering Division
U. S. Army Corps of Engineers
424 Trapelo Road
Waltham, Massachusetts 02154

Dear Mr. Leslie:

Your proposal for flood control work in the Park River basin in Connecticut has been reviewed and we are in complete agreement that this work should be done.

We have pointed out on numerous occasions that the full benefits of work now under construction on this channel will not be realized until gaps in the conduit are completed. As far back as three years ago and several times since, we have suggested that the Greater Hartford Flood Commission consider the construction of a pilot channel in these gaps in order that the level of water would be lower to help construction now under way. This would benefit the Connecticut Highway Department construction as well as the channel work which is under contract and which is subject to backwater from the unimproved gaps south to New Britain Avenue.

We heartily endorse this proposed improvement.

Sincerely yours,

A handwritten signature in dark ink, appearing to read "N. Paul Tedrow", with a stylized flourish at the end.

N. Paul Tedrow
State Conservationist



DEPARTMENT OF HEALTH, EDUCATION, AND WELFARE
REGIONAL OFFICE

PUBLIC HEALTH SERVICE

Region I
120 Boylston Street
Boston, Massachusetts 02116

December 27, 1965

Mr. John Wm. Leslie
Chief, Engineering Division
U. S. Army Engineer Division
New England
Corps of Engineers
424 Trapelo Road
Waltham, Massachusetts

Dear Mr. Leslie:

In accordance with your request of 13 December 1965 we would like to provide the following comments on the Park River Flood Control Project.

We recommend that the design and construction of the project contain adequate provisions for the implementation of present and future combined sewer separation plans. In addition, we recommend that facilities be provided for the collection and treatment of wastewater, which may now be discharged to the Park River.

To facilitate these recommendations we suggest close coordination be maintained in the formulation of the project with the Connecticut Water Resources Commission, the Hartford County Metropolitan District, and this office.

Sincerely yours,

for Alfred P. Anderson
Earl J. Anderson
Acting Regional Program Director
Water Supply and Pollution Control
Public Health Service

EXHIBIT G-2



UNITED STATES
DEPARTMENT OF THE INTERIOR
FISH AND WILDLIFE SERVICE
BUREAU OF SPORT FISHERIES AND WILDLIFE
59 TEMPLE PLACE
BOSTON, MASSACHUSETTS 02111

December 7, 1964

Division Engineer
U. S. Army Engineer Division, New England
Corps of Engineers
424 Trapelo Road
Waltham, Massachusetts 02154

Dear Sir:

Reference is made to your November 20, 1964 notice stating that a public hearing on the review of flood control in the Park River Basin, Hartford, Connecticut will be held in the Capitol Building, Hartford, Connecticut on December 15, 1964.

Based on our knowledge of the area and the limited fish and wildlife resources we believe that any modification of the existing project which is within the Hartford city limits will have no significant effect on the resources; neither would there be any appreciable opportunity for improvement.

In view of the above, we do not plan to report on this project.

Sincerely yours,

Thomas A. Schrader, Chief
Division of Technical Services



STATE OF CONNECTICUT

WATER RESOURCES COMMISSION

STATE OFFICE BUILDING • HARTFORD 15, CONNECTICUT

January 10, 1966

Division Engineer
U. S. Army Corps of Engineers
New England Division
424 Trapelo Road
Waltham 54, Massachusetts

Attention: Mr. John Wm. Leslie, Chief
Engineering Division

Gentlemen:

Reference is made to your letter of December 13, 1965 requesting our comments on the plan developed for flood control on the Park River Basin in accordance with the Senate Committee Resolution approved October 16, 1961.

As you know, the Greater Hartford Flood Control Commission exercises the primary interest in flood control in the Park River Basin. Through our associations and connections with that Commission we are aware of their interest in the project which you describe. It is assumed that you have received their views.

We will attempt to keep abreast of the developments of this project so that at various stages we may offer comments if it appears that they are desirable and appropriate.

Very truly yours,

A handwritten signature in cursive script, appearing to read "William S. Wise".

William S. Wise
Director

WSW:JC:s

THE METROPOLITAN DISTRICT

115 BROAD STREET
HARTFORD 5, CONN.
TELEPHONE 525-0841
5-AWS/smk



OFFICE OF THE
DISTRICT MANAGER

March 18, 1966

John William Leslie, Chief,
U. S. Army Engineer Division
Corps of Engineers
424 Trapelo Road
Waltham 54, Massachusetts

SUBJECT: PARK RIVER BASIN, HARTFORD
REFER TO USA ENGS. FILE NE DED-R

Dear Mr. Leslie:

In your letter of March 10, 1966 you asked for our comment for inclusion in your report on proposed improvements for flood control in the Park River Basin, Hartford County, Connecticut, at an estimated Federal first cost of \$30,800,000 and an estimated local cost for lands, damages and relocations of \$900,000.


Our comment is that we strongly urge and recommend the immediate start and early completion of these improvements. Any delay in making these improvements could conceivably result in serious flooding damage under certain conditions to property in the areas needing flood protection, and interruption to the normal operation of the District's sewerage and drainage system.

We have commented similarly on a general statement transmitted to you by Edward J. McDonough, Chairman of the District Board, under date of December 15, 1964.

We have given more detailed information and suggestions on our drainage and sewerage system involvements, and other comments in letters dated August 10, 1964, December 17, 1964, March 2, 1965, April 2, 1965 and a statement and recommendations submitted by The Metropolitan District Commission on October 1, 1964.

Our Bureau of Public Works (sewerage system functions) and our Water Bureau (water system functions) will be glad to recommend District cooperation in any appropriate way.

Very truly yours,


William A.D. Wurts
District Manager

Enc. 1
cc: GUG
AWS

EXHIBIT G-5

THE METROPOLITAN DISTRICT

115 BROAD STREET
HARTFORD, CONN. 06105
TELEPHONE 525-0841



EDWARD J. MC DONOUGH
CHAIRMAN, THE DISTRICT BOARD

December 15, 1964

Peter J. Hyser, Brigadier General
U.S. Division Engineer
U.S. Army Engineer Division, New England
424 Trapelo Road
Waltham, Massachusetts

**SUBJECT: STATEMENT
PUBLIC HEARING ON REVIEW OF FLOOD CONTROL IN
THE PARK RIVER BASIN, HARTFORD, CONNECTICUT**

Dear Sir:

The Metropolitan District Commission strongly urges further effort to improve flood protection in the Greater Hartford area. The elimination of flooding in the Park River basin is a vital step in improving the sewerage and drainage system in this part of the District.

The proposed deep flood conduit along Park Street, in Hartford, should be helpful to the District and its inhabitants. This flood conduit should provide a less distant and more economical outlet for some of the storm drains to be built as part of the District's comprehensive plan which the District has already undertaken to separate Hartford's old combined sewers.

The District has always worked with the various local, state and federal flood protection agencies to properly plan flood protection work, especially when the District's sanitary sewerage system is involved; substantial District funds have been expended to plan and build sewerage system improvements brought on, or made possible, by flood protection work to date.

We will look forward to working with you on any further flood protection work you undertake.

Very truly yours,


Edward J. McDonough
Chairman

EXHIBIT G-6

GREATER HARTFORD FLOOD COMMISSION

11 ASYLUM STREET
HARTFORD, CONNECTICUT 06103

TELEPHONE 532-9208

April 18, 1966

Commissioners

VINCENT P. CENCI, M.D.
E. WELLES EDDY
WILLIAM E. GLYNN
HAROLD F. KEITH
JOHN C. PARSONS
H. WARD PINNEY
LYONEL H. PUTNAM

HAROLD F. KEITH
Chairman

E. WELLES EDDY
Vice Chairman

H. WARD PINNEY
Secretary

CHARLES W. COOKE
Director

PHILIP C. SMITH
Chief Engineer

ALEXANDER A. GOLDFARB
Counsel

Colonel Remi O. Renier, Acting Division Engineer
New England Division, Corps of Engineers
424 Trapelo Road
Waltham, Massachusetts 02154

Dear Colonel Renier:

This is to acknowledge receipt of your letter of March 24, 1966 with its enclosures. My desire to bring this matter to the attention of the entire Commission necessitated the delay in responding to your letter.

We wish to advise you that we have carefully examined the proposed work as outlined in your letter and as indicated on the maps forwarded therewith. Based upon this examination and the numerous staff conferences referred to in your communication, we wish to advise you that the Greater Hartford Flood Commission is satisfied that the proposed works taken together with the conduit and channel work thus far completed by this Commission will be adequate to accomplish substantial flood control protection in that area which is the subject of our mutual concern. We were disappointed to learn that your recommendations will not include the extension of the conduit to a point north of Farmington Avenue, but we are sure that there are good and adequate reasons for this omission.

The Greater Hartford Flood Commission and the undersigned wish to take this opportunity to assure you that it is willing and able to furnish the required measures of local co-operation as outlined in your letter. You may be interested to know that in hopeful anticipation of a favorable report, steps have already been taken and some moneys already appropriated with a view to acquisition of certain of the easements and rights-of-way necessary for the construction and operation of the project. With regard to Items b, c, and d of the third paragraph of your letter, we wish to assure you that this Commission is willing and able to undertake the responsibilities outlined therein.

EXHIBIT G-7

TO: Colonel Remi O. Renier

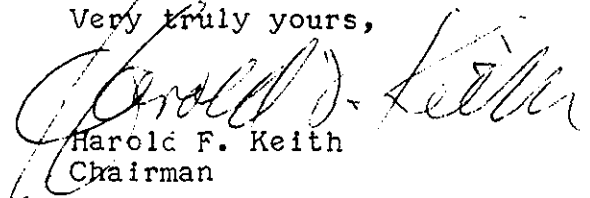
April 18, 1966

We wish to further advise you that numerous conferences between our staff and the City Plan Commission have been held concerning the matter of flood plain zoning. As a result of these conferences, it is expected that provisions with regard to such flood plain zoning will be included in a comprehensive revision of the zoning ordinance about to be presented to the Court of Common Council of the City of Hartford by the City Plan Commission.

On behalf of the people of the City of Hartford and its environs, the City Administration, and this Commission, we would like to take this opportunity to express to you and your staff our sincere appreciation for the interest and concern you have demonstrated in assisting us in accomplishing our goal of providing a maximum in flood control protection.

We shall be anxiously awaiting your full report.

Very truly yours,


Harold F. Keith
Chairman

HFK:m